## 19－0436；Rev 1；3／96

## 500MHz，Low－Power Op Amps

## General Description

The MAX4100／MAX4101 op amps combine ultra－high－ speed performance with low－power operation．The MAX4100 is compensated for unity－gain stability，while the MAX4101 is compensated for stability in applica－ tions with a closed－loop gain（AvcL）of $2 \mathrm{~V} / \mathrm{V}$ or greater．
The MAX4100／MAX4101 require only 5mA of supply current while delivering a 500 MHz unity－gain bandwidth （MAX4100）or a $200 \mathrm{MHz}-3 \mathrm{~dB}$ bandwidth（MAX4101） with a $250 \mathrm{~V} / \mu \mathrm{s}$ slew rate．
These high－speed op amps have a wide output voltage swing of $\pm 3.5 \mathrm{~V}$ and a high current－drive capability of 80 mA ．

Applications
Video Cable Driver
Ultrasound
Gamma Cameras
Portable Instruments
Active Filters
ADC Buffers

Typical Application Circuit

－500MHz Unity－Gain Bandwidth（MAX4100） $200 \mathrm{MHz}-3 \mathrm{~dB}$ Bandwidth（AvCL $=2 \mathrm{~V} / \mathrm{V}$ ，MAX4101）
－65MHz 0．1dB Gain Flatness（MAX4100）
－ $250 \mathrm{~V} / \mathrm{\mu s}$ Slew Rate
－0．06\％／0．04 ${ }^{\circ}$ Differential Gain／Phase
－High Output Drive：80mA
－Low Power：5mA Supply Current
－Fast Settling Time：
18ns to 0．1\％
35ns to 0．01\％
Ordering Information

| PART | TEMP．RANGE | PIN－PACKAGE |
| :--- | :--- | :--- |
| MAX4100ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO |
| MAX4100EUA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $8 \mu \mathrm{MAX}^{*}$ |
| MAX4101ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO |

＊Contact factory for availability of $\mu M A X$ package．

TOP VIEN

＊Contact factory for availability of MAX4100 $\mu$ MAX package．

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## ABSOLUTE MAXIMUM RATINGS

Power-Supply Voltage (VCC, $\mathrm{V}_{\mathrm{EE}}$ )

$\qquad$
Voltage on Any Pin to Ground or Any Other Pin......... $V_{C C}$ to $V_{E E}$ Short-Circuit Duration (VOUT to GND) $\qquad$ .Indefinite
Continuous Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ )
SO (derate $5.88 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ ) $\qquad$ 471 mW
$\mu \mathrm{MAX}$ (derate $4.10 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ ) $\qquad$ 330 mW
Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{MIN}}\right.$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC SPECIFICATIONS |  |  |  |  |  |  |  |
| Input Offset Voltage | VOS | VOUT $=0 \mathrm{~V}$ |  |  | 1 | 8 | mV |
| Input Offset Voltage Drift | TCVos | Vout $=0 \mathrm{~V}$ |  | 15 |  |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | IB | VOUT $=0 \mathrm{~V}, \mathrm{~V}$ IN $=-\mathrm{V}_{\text {OS }}$ |  |  | 3 | 9 | $\mu \mathrm{A}$ |
| Input Offset Current | los | Vout $=0 \mathrm{~V}, \mathrm{~V}$ IN $=-\mathrm{V}$ OS |  |  | 0.05 | 0.5 | $\mu \mathrm{A}$ |
| Common-Mode Input Resistance | RINCM | Either input |  |  | 5 |  | $\mathrm{M} \Omega$ |
| Common-Mode Input Capacitance | CIncm | Either input |  |  | 1 |  | pF |
| Input Voltage Noise | $e_{n}$ | $\mathrm{f}=100 \mathrm{kHz}$ | MAX4100 |  | 8 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
|  |  |  | MAX4101 |  | 6 |  |  |
| Integrated Voltage Noise |  | $\mathrm{f}=1 \mathrm{MHz}$ to 100 MHz | MAX4100 |  | 100 |  | $\mu \mathrm{V}_{\text {RMS }}$ |
|  |  |  | MAX4101 |  | 75 |  |  |
| Input Current Noise | $\mathrm{in}_{n}$ | $\mathrm{f}=100 \mathrm{kHz}$ | MAX4100 |  | 0.8 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
|  |  |  | MAX4101 |  | 0.8 |  |  |
| Integrated Current Noise |  | $\mathrm{f}=1 \mathrm{MHz}$ to 100 MHz | MAX4100 |  | 10 |  | nARMS |
|  |  |  | MAX4101 |  | 10 |  |  |
| Common-Mode Input Voltage | VCM |  |  | -2.5 |  | 2.5 | V |
| Common-Mode Rejection | CMR | $\mathrm{V}_{\mathrm{CM}}= \pm 2.5 \mathrm{~V}$ |  | 75 | 90 |  | dB |
| Power-Supply Rejection | PSR | $\mathrm{V}_{\mathrm{S}}= \pm 4.5 \mathrm{~V}$ to $\pm 5.5 \mathrm{~V}$ |  | 55 | 60 |  | dB |
| Open-Loop Voltage Gain | AOL | $\mathrm{V}_{\text {OUT }}= \pm 2.0 \mathrm{~V}, \mathrm{~V}_{\text {CM }}=0 \mathrm{~V}$ | $\mathrm{R}_{\mathrm{L}}=\infty$ | 53 | 58 |  | dB |
|  |  |  | $\mathrm{R}_{\mathrm{L}}=100 \Omega$ | 51 | 56 |  |  |
| Quiescent Supply Current | ISY | $\mathrm{V}_{\mathrm{IN}}=0 \mathrm{~V}$ |  |  | 5 | 6 | mA |
| Output Voltage Swing | Vout | $\mathrm{R}_{\mathrm{L}}=\infty$ |  | $\pm 3.5$ | $\pm 3.8$ |  | V |
|  |  | $\mathrm{R}_{\mathrm{L}}=100 \Omega$ |  | $\pm 3.1$ | $\pm 3.5$ |  |  |
| Output Current |  | $\mathrm{R}_{\mathrm{L}}=30 \Omega, \mathrm{~T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 65 | 80 |  | mA |
| Short-Circuit Output Current | Isc | Short to ground or either supply voltage |  |  | 90 |  | mA |

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## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{MIN}}\right.$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)


Typical Operating Characteristics
$\left(\mathrm{V}_{C C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted. $)$


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( $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)
Typical Operating Characteristics (continued)


MAX4100
SMALL-SIGNAL PULSE RESPONSE
$($ AVCL $=+5)$


TIME (50ns/div)

MAX4101
LARGE-SIGNAL PULSE RESPONSE
(AvCL $=+10$ )


TIME (20ns/div)
SM ALL-SIGNAL PULSE
$($ (AvCL $=+5)$

ND


MAX4101
SM ALL-SIGNAL PULSE RESPONSE
( $\mathrm{AVCL}=+2$ )


TIME (10ns/div)

MAX4100
SM ALL-SIGNAL PULSE RESPONSE
( A VCL $=+1$ )


MAX4101
LARGE-SIGNAL PULSE RESPONSE
( $_{\text {VCL }}=+2$ )


MAX4101
SM ALL-SIGNAL PULSE RESPONSE
(AvCL $=+10$ )


TIME (50ns/div)

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## Typical Operating Characteristics (continued)

$\left(\mathrm{V} C \mathrm{C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)


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$\left(\overline{\mathrm{V}} \mathrm{CC}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)



MAX4100
HARM ONIC DISTORTION vs. FREQUENCY


MAX4101
HARM ONIC DISTORTION vs. FREQUENCY


MAX4100
HARM ONIC DISTORTION vs. FREQUENCY


MAX4101 HARM ONIC DISTORTION vs. FREQUENCY


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## Typical Operating Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{E E}=-5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)


| PIN | NAME | FUNCTION |
| :---: | :---: | :--- |
| $1,5,8$ | N.C. | No Connection, not internally connected |
| 2 | IN- | Inverting Input |
| 3 | IN+ | Noninverting Input |
| 4 | VEE $^{2}$ | Negative Power Supply, connected to -5 V |
| 6 | OUT | Amplifier Output |
| 7 | VCC | Positive Power Supply, connected to +5 V |

# 500MHz, Low-Power Op Amps 

___Detailed Description
The MAX4100/MAX4101 are low-power, high-bandwidth operational amplifiers optimized for driving back-terminated cables in composite video, RGB, and RF systems. The MAX4100 is unity-gain stable, and the MAX4101 is optimized for closed-loop gains greater than or equal to $2 \mathrm{~V} / \mathrm{V}$ ( $\mathrm{AvCL} \geq 2 \mathrm{~V} / \mathrm{V}$ ). While consuming only 5 mA ( 6 mA max) supply current, both devices can drive $50 \Omega$ backterminated cables to $\pm 3.1 \mathrm{~V}$ minimum.
The MAX4100 features a bandwidth in excess of 500 MHz and a 0.1 dB gain flatness of 65 MHz . It offers differential gain and phase errors of $0.06 \% / 0.04^{\circ}$, respectively. The MAX4101 features a -3dB bandwidth of 200 MHz , a 0.1 dB bandwidth of 50 MHz , and $0.07 \% / 0.04^{\circ}$ differential gain and phase.
Available in small 8-pin SO and $\mu \mathrm{MAX}$ packages, these ICs are ideally suited for use in portable systems (in RGB, broadcast, or consumer video applications) that benefit from low power consumption.

## Applications Information

## Layout and Power-Supply Bypassing

The MAX4100/MAX4101 have an RF bandwidth and, consequently, require careful board layout. Depending on the size of the PC board used and the frequency of operation, it may be desirable to use constant-impedance microstrip or stripline techniques.
To realize the full AC performance of this high-speed amplifier, pay careful attention to power-supply bypassing and board layout. The PC board should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces.


Figure 1a. Inverting Gain Configuration

Regardless of whether a constant-impedance board is used, it is best to observe the following guidelines when designing the board. Wire-wrap boards are much too inductive, and breadboards are much too capacitive; neither should be used. IC sockets increase parasitic capacitance and inductance, and should not be used. In general, surface-mount components give better high-frequency performance than through-hole components. They have shorter leads and lower parasitic reactances. Keep lines as short and as straight as possible. Do not make $90^{\circ}$ turns; round all corners.
High-frequency bypassing techniques must be observed to maintain the amplifier accuracy. The bypass capacitors should include a 1000pF ceramic capacitor between each supply pin and the ground plane, located as close to the package as possible. Next, place a $0.01 \mu \mathrm{~F}$ to $0.1 \mu \mathrm{~F}$ ceramic capacitor in parallel with each 1000 pF capacitor, and as close to each as possible. Then place a $10 \mu \mathrm{~F}$ to $15 \mu \mathrm{~F}$ low-ESR tantalum at the point of entry (to the PC board) of the power-supply pins. The power-supply trace should lead directly from the tantalum capacitor to the $\mathrm{V}_{\mathrm{CC}}$ and $\mathrm{V}_{E E}$ pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.


Figure 1b. Noninverting Gain Configuration


Figure 1c. MAX4100 Unity-Gain Buffer Configuration

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Figure 2. Effect of Feedback Resistor Values and Parasitic Capacitance on Bandwidth

## Setting Gain

The MAX4100/MAX4101 are voltage-feedback op amps that can be configured as an inverting or noninverting gain block, as shown in Figures 1a and 1b. The gain is determined by the ratio of two resistors and does not affect amplifier frequency compensation.
In the unity-gain configuration (as shown in Figure 1c), maximum bandwidth and stability is achieved with the MAX4100 when a small feedback resistor is included. This resistor suppresses the negative effects of parasitic inductance and capacitance. A value of $24 \Omega$ provides the best combination of wide bandwidth, low peaking, and fast settling time. In addition, this resistor reduces the errors from input bias currents.

## Choosing Resistor Values

The values of feedback and input resistors used in the inverting or noninverting gain configurations are not critical (as is the case with current feedback amplifiers). However, take care when selecting because the ohmic values need to be kept small and noninductive for practical reasons.
The input capacitance of the MAX4100/MAX4101 is approximately $2 p F$. In either the inverting or noninverting configuration, the bandwidth limit caused by the package capacitance and resistor time constant is $f 3 d B=1 /(2 \Pi R C)$, where $R$ is the parallel combination of the input and feedback resistors ( $R F$ and $R G$ in Figure 2) and $C$ is the package and board capacitance at the inverting input. Table 1 shows the bandwidth limit for several values of RF and RG, assuming $4 p F$ total capacitance ( $2 p F$ for the MAX4100/MAX4101 and $2 p F$ of PC board parasitics).

Table 1. Resistor and Bandwidth Values for Various Gain Configurations

| GAIN <br> $\mathbf{( V / V )}$ | $\mathbf{R}_{\mathbf{G}}$ <br> $(\Omega)$ | $\mathbf{R F}_{\mathbf{F}}$ <br> $(\Omega)$ | BANDWIDTH <br> LIMIT* $^{*}$ <br> $(\mathbf{M H z})$ |
| :---: | :---: | :---: | :---: |
| +1 | $\infty$ | 24 | 1659 |
| +2 | 200 | 200 | 398 |
| +5 | 50 | 200 | 995 |
| +10 | 30 | 270 | 1474 |
| -1 | 200 | 200 | 398 |
| -2 | 75 | 150 | 796 |
| -5 | 50 | 250 | 955 |
| -10 | 50 | 500 | 875 |

* Assuming an infinite bandwidth amplifier.


## Resistor Types

Surface-mount resistors are the best choice for highfrequency circuits. They are of similar material to the metal film resistors, but are deposited using a thick-film process in a flat, linear manner so that inductance is minimized. Their small size and lack of leads also minimize parasitic inductance and capacitance, thereby yielding more predictable performance.

## DC and Noise Errors

There are several major error sources to be considered in any operational amplifier. These apply equally to the MAX4100/MAX4101. Offset-error terms are given by the equation below. Voltage and current noise errors are root-square summed, so are computed separately. Using the circuit in Figure 3, the total output offset voltage is determined by:
a) The input offset voltage (VOS) times the closed-loop gain ( $1+\mathrm{RF}_{\mathrm{F}} / \mathrm{RG}_{\mathrm{G}}$ )
b) The positive input bias current ( $\mathrm{I}_{+}$) times the source resistor (Rs) minus the negative input bias current (lB-) times the parallel combination of $\mathrm{R}_{\mathrm{G}}$ and RF. Ios (offset current) is the difference between the two bias currents. If $\mathrm{RG}_{\mathrm{G}}| | \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{S}}$, this part of the expression becomes los $\times$ Rs.
The equation for total DC error is:

$$
V_{\mathrm{OUT}}=\left(\mathrm{los}_{\mathrm{S}}+\mathrm{V}_{\mathrm{OS}}\right)\left(1+\frac{\mathrm{R}_{\mathrm{F}}}{\mathrm{R}_{\mathrm{G}}}\right)
$$

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Figure 3. Output Offset Voltage
c) Total output-referred noise voltage is shown by the equation below ( $\mathrm{en}_{\mathrm{n}}(\mathrm{OUT})$ ):

$$
\mathrm{e}_{\mathrm{n}(\mathrm{OUT})}=\left(1+\frac{\mathrm{R}_{\mathrm{F}}}{\mathrm{R}_{\mathrm{G}}}\right) \sqrt{\left(2 \mathrm{i}_{\mathrm{n}} \mathrm{R}_{\mathrm{S}}\right)^{2}+\left(\mathrm{e}_{\mathrm{N}}\right)^{2}}
$$

The MAX4100/MAX4101, with two high-impedance inputs, have low $8 \mathrm{nV} \sqrt{\mathrm{Hz}}$ voltage noise and only $0.8 p \mathrm{~A} \sqrt{\mathrm{~Hz}}$ current noise.
An example of DC error calculations, using the MAX4100/MAX4101 typical data and the typical operating circuit with $R_{F}=R_{G}=200 \Omega\left(R_{S}=100 \Omega\right)$, gives:

$$
\begin{aligned}
& V_{\text {OUT }}=\left(l_{\text {OS }} R_{S}+V_{\text {OS }}\right)\left(1+\frac{R_{F}}{R_{G}}\right) \\
& V_{\text {OUT }}=\left(3 \times 10^{-6} \times 10^{2}+1 \times 10^{-3}\right)(1+1) \\
& V_{\text {OUT }}=2.6 \mathrm{mV}
\end{aligned}
$$

Calculating total output-referred noise in a similar manner yields:
$e_{n(\text { OUT })}=(1+1) \sqrt{\left(2 \times 0.8 \times 10^{-12} \times 100\right)^{2}+\left(8 \times 10^{-9}\right)^{2}}$
$\mathrm{e}_{\mathrm{n}(\mathrm{OUT})}=8 \mathrm{nV} / \sqrt{\mathrm{Hz}}$
With a 200 MHz system bandwidth, this calculates to $133 \mu \mathrm{~V}_{\text {RMS }}$ (approximately $679 \mu \mathrm{~V}_{\text {p-p }}$ ).

In both DC and noise calculations, errors are dominated by offset voltage and noise voltage (rather than by input bias current or noise current).
Metal-film resistors with leads are manufactured using a thin-film process, where resistive material is deposited in a spiral layer around a ceramic rod. Although the materials used are noninductive, the spiral winding presents a small inductance (about 5 nH ) that may have an adverse effect on high-frequency circuits.


Figure 4a. MAX4100 Bandwidth vs. Capacitive Load


Figure 4b. MAX4100 Bandwidth vs. Capacitive Load and Isolation Resistor

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Carbon composition resistors with leads are manufactured by pouring the resistor material into a mold. This process yields a relatively low-inductance resistor that is very useful in high-frequency applications, although they tend to cost more and have more thermal noise than other types. The ability of carbon composition resistors to self-heal after a large current overload makes them useful in high-power RF applications.
For general-purpose use, surface-mount metal-film resistors seem to have the best overall performance for low cost, low inductance, and low noise.

Driving Capacitive Loads
When driving $50 \Omega$ or $75 \Omega$ back-terminated transmission lines, capacitive loading is not an issue; therefore an isolation resistor is not required. For other applications where the ability to drive capacitive loads is required, the MAX4100/MAX4101 can typically drive 5pF and 20pF, respectively. Figure 4a illustrates how a capacitive load influences the amplifier's peaking without an isolation resistor (RS). Figure 4b shows how an isolation resistor decreases the amplifier's peaking.
The MAX4100/MAX4101 can drive capacitive loads up to $5 p F$. By using a small isolation resistor between the amplifier output and the load, large capacitance values may be driven without oscillation (Figure 5a). In most cases, less than $50 \Omega$ is sufficient. Use Figure $5 b$ to determine the value needed in your application. Determine the worst-case maximum capacitive load you may encounter and select the appropriate resistor from the graph.


Figure 5a. Using an Isolation Resistor for High Capacitive Loads (MAX4100)


Figure 5b. Isolation vs. Capacitive Load

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