Low Noise, Precision, High Speed Operational Amplifier (AVCL ≥ 5)

OP37

FEATURES
Low Noise, 80 nV p-p (0.1 Hz to 10 Hz)
3 nV/√Hz @ 1 kHz
Low Drift, 0.2 μV/°C
High Speed, 17 V/µs Slew Rate
63 MHz Gain Bandwidth
Low Input Offset Voltage, 10 μV
Excellent CMRR, 126 dB (Common-Voltage @ 11 V)
High Open-Loop Gain, 1.8 Million
Replaces 725, OP-07, SE5534 In Gains > 5
Available in Die Form

GENERAL DESCRIPTION
The OP37 provides the same high performance as the OP27, but the design is optimized for circuits with gains greater than five. This design change increases slew rate to 17 V/µs and gain-bandwidth product to 63 MHz.

The OP37 provides the low offset and drift of the OP07 plus higher speed and lower noise. Offsets down to 25 µV and drift of 0.6 µV/°C maximum make the OP37 ideal for precision instrumentation applications. Exceptionally low noise (en = 3.5 nV/√Hz), a low 1/f noise corner frequency of 2.7 Hz, and the high gain of 1.8 million, allow accurate high-gain amplification of low-level signals.

The low input bias current of 10 nA and offset current of 7 nA are achieved by using a bias-current cancellation circuit. Over the military temperature range this typically holds IB and IOS to 20 nA and 15 nA respectively.

The output stage has good load driving capability. A guaranteed swing of 10 V into 600 Ω and low output distortion make the OP37 an excellent choice for professional audio applications. PSRR and CMRR exceed 120 dB. These characteristics, coupled with long-term drift of 0.2 µV/month, allow the circuit designer to achieve performance levels previously attained only by discrete designs.

Low-cost, high-volume production of the OP37 is achieved by using on-chip zener-zap trimming. This reliable and stable offset trimming scheme has proved its effectiveness over many years of production history.

The OP37 brings low-noise instrumentation-type performance to such diverse applications as microphone, tapehead, and RIAA phono preamplifiers, high-speed signal conditioning for data acquisition systems, and wide-bandwidth instrumentation.

PIN CONNECTIONS
8-Lead Hermetic DIP
(Z Suffix)
Epoxy Mini-DIP
(P Suffix)
8-Lead SO
(S Suffix)

SIMPLIFIED SCHEMATIC

R1 and R2 are permanently adjusted at wafer test for minimum offset voltage.

*VOS TRIM
IN
OUT
NC
VOS ADJ.
### OP37

#### ABSOLUTE MAXIMUM RATINGS

Supply Voltage ........................................ 22 V  
Internal Voltage (Note 1) ......................... 22 V  
Output Short-Circuit Duration ................. Indefinite  
Differential Input Voltage (Note2) ........... 0.7 V  
Differential Input Current (Note 2) .......... 25 mA  
Storage Temperature Range .................. -65°C to +150°C  
Operating Temperature Range 
   OP37A ........................................... -55°C to +125°C  
   OP37E (Z) ...................................... -25°C to +85°C  
   OP37E, OP-37F (P) .......................... 0°C to 70°C  
   OP37G (P, S, Z) .............................. -40°C to +85°C  
Lead Temperature Range (Soldering, 60 sec) ... 300°C  
Junction Temperature .......................... -45°C to +150°C  

#### ORDERING GUIDE

<table>
<thead>
<tr>
<th>Package Type</th>
<th>( \theta_A )</th>
<th>( \theta_C )</th>
<th>Unit</th>
<th>( V_{OS} ) MAX (( \mu )V)</th>
<th>CerDIP 8-Lead</th>
<th>Plastic 8-Lead</th>
<th>Operating Temperature Range</th>
</tr>
</thead>
<tbody>
<tr>
<td>8-Lead Hermetic DIP (Z)</td>
<td>148</td>
<td>16</td>
<td>°C/W</td>
<td>25</td>
<td>OP37AZ*</td>
<td>OP37EZ</td>
<td>MIL</td>
</tr>
<tr>
<td>8-Lead Plastic DIP (P)</td>
<td>103</td>
<td>43</td>
<td>°C/W</td>
<td>25</td>
<td>OP37EP</td>
<td>OP37FP*</td>
<td>IND/COM</td>
</tr>
<tr>
<td>8-Lead SO (S)</td>
<td>158</td>
<td>43</td>
<td>°C/W</td>
<td>100</td>
<td>OP37GP</td>
<td>OP37GS</td>
<td>XIND</td>
</tr>
</tbody>
</table>

*Not for new design, obsolete, April 2002.

#### CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the OP37 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high-energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.
### SPECIFICATIONS (V_S = \pm 15 V, T_A = 25^\circ C, unless otherwise noted.)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Conditions</th>
<th>OP37A/E</th>
<th>OP37F</th>
<th>OP37G</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Input Offset Voltage</strong></td>
<td>V_{OS}</td>
<td>Note 1</td>
<td>Min</td>
<td>Typ</td>
<td>Max</td>
</tr>
<tr>
<td>Long-Term Stability</td>
<td>V_{OS}/Time</td>
<td>Notes 2, 3</td>
<td>0.2</td>
<td>1.0</td>
<td></td>
</tr>
<tr>
<td><strong>Input Offset Current</strong></td>
<td>I_{OS}</td>
<td></td>
<td>7</td>
<td>35</td>
<td>9</td>
</tr>
<tr>
<td><strong>Input Bias Current</strong></td>
<td>I_{B}</td>
<td>±10</td>
<td>±40</td>
<td>±12</td>
<td>±55</td>
</tr>
<tr>
<td><strong>Input Offset Voltage</strong></td>
<td>e_{OV-p}</td>
<td>1 Hz to 10 Hz(^3)</td>
<td>0.08</td>
<td>0.18</td>
<td></td>
</tr>
<tr>
<td><strong>Input Voltage Noise</strong></td>
<td>e_{n}</td>
<td>f_o = 10 Hz(^4)</td>
<td>3.5</td>
<td>5.5</td>
<td></td>
</tr>
<tr>
<td><strong>Input Voltage Noise Density</strong></td>
<td>i_{N}</td>
<td>f_o = 10 Hz(^4)</td>
<td>1.7</td>
<td>4.0</td>
<td></td>
</tr>
<tr>
<td><strong>Input Resistance Differential Mode</strong></td>
<td>R_{IN}</td>
<td>Note 7</td>
<td>1.3</td>
<td>6</td>
<td>0.9</td>
</tr>
<tr>
<td><strong>Input Resistance Common Mode</strong></td>
<td>R_{INCM}</td>
<td></td>
<td>3</td>
<td></td>
<td>2.5</td>
</tr>
<tr>
<td><strong>Input Voltage Range</strong></td>
<td>IVR</td>
<td></td>
<td>±11</td>
<td>±12.3</td>
<td>±11</td>
</tr>
<tr>
<td><strong>Common Mode Rejection Ratio</strong></td>
<td>CMRR</td>
<td>V_{CM} = \pm 11 V</td>
<td>114</td>
<td>126</td>
<td>106</td>
</tr>
<tr>
<td><strong>Power Supply Rejection Ratio</strong></td>
<td>PSSR</td>
<td>V_S = \pm 4 V to \pm 18 V</td>
<td>1</td>
<td>10</td>
<td>1</td>
</tr>
<tr>
<td><strong>Large Signal Voltage Gain</strong></td>
<td>A_{VO}</td>
<td>R_L ≥ 2 kΩ, V_O = \pm 10 V</td>
<td>1000</td>
<td>1800</td>
<td>1000</td>
</tr>
<tr>
<td><strong>Output Voltage Swing</strong></td>
<td>V_O</td>
<td>R_L ≥ 1 kΩ, V_O = \pm 10 V</td>
<td>800</td>
<td>1500</td>
<td>800</td>
</tr>
<tr>
<td><strong>Slew Rate</strong></td>
<td>SR</td>
<td>R_L ≥ 2 kΩ(^4)</td>
<td>11</td>
<td>17</td>
<td>11</td>
</tr>
<tr>
<td><strong>Gain Bandwidth Product</strong></td>
<td>GBW</td>
<td>f_o = 10 kHz(^4)</td>
<td>45</td>
<td>63</td>
<td>45</td>
</tr>
<tr>
<td><strong>Open-Loop Output Resistance</strong></td>
<td>R_O</td>
<td>V_O = 0, I_O = 0</td>
<td>70</td>
<td></td>
<td></td>
</tr>
<tr>
<td><strong>Power Consumption</strong></td>
<td>P_d</td>
<td>V_O = 0</td>
<td>90</td>
<td>140</td>
<td>90</td>
</tr>
</tbody>
</table>

**NOTES**

1. Input offset voltage measurements are performed by automated test equipment approximately 0.5 seconds after application of power. A/E grades guaranteed fully warmed up.
2. Long-term input offset voltage stability refers to the average trend line of V_{OS} vs. Time over extended periods after the first 30 days of operation. Excluding the initial hour of operation, changes in V_{OS} during the first 30 days are typically 2.5 µV—refer to typical performance curve.
3. Sample tested.
4. Guaranteed by design.
5. See test circuit and frequency response curve for 0.1 Hz to 10 Hz tester.
6. See test circuit for current noise measurement.
7. Guaranteed by input bias current.
## OP37—SPECIFICATIONS

### Electrical Characteristics \( (V_S = \pm 15\, \text{V}, -55^\circ\text{C} \leq T_A \leq +125^\circ\text{C}, \text{unless otherwise noted}) \)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Conditions</th>
<th>OP37A Min</th>
<th>OP37A Typ</th>
<th>OP37A Max</th>
<th>OP37C Min</th>
<th>OP37C Typ</th>
<th>OP37C Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Offset Voltage</td>
<td>( V_{OS} )</td>
<td>Note 1</td>
<td>1025</td>
<td>30</td>
<td>100</td>
<td>55</td>
<td>220</td>
<td></td>
<td>( \mu\text{V} )</td>
</tr>
<tr>
<td>Average Input Offset Drift</td>
<td>( TCV_{OS} )</td>
<td>Note 2</td>
<td>0.2</td>
<td>0.4</td>
<td>1.8</td>
<td></td>
<td></td>
<td></td>
<td>( \mu\text{V/}^\circ\text{C} )</td>
</tr>
<tr>
<td></td>
<td>( TCV_{OSN} )</td>
<td>Note 3</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Input Offset Current</td>
<td>( I_{OS} )</td>
<td></td>
<td>1550</td>
<td>30</td>
<td>135</td>
<td></td>
<td></td>
<td></td>
<td>( \text{nA} )</td>
</tr>
<tr>
<td>Input Bias Current</td>
<td>( I_B )</td>
<td>±20</td>
<td></td>
<td>±35</td>
<td>±150</td>
<td></td>
<td></td>
<td></td>
<td>( \text{nA} )</td>
</tr>
<tr>
<td>Input Voltage Range</td>
<td>( IVR )</td>
<td>±10.3 ±11.5</td>
<td>±10.2 ±11.5</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
<tr>
<td>Common Mode Rejection Ratio</td>
<td>( \text{CMRR} )</td>
<td>( V_{CM} = \pm 10, \text{V} )</td>
<td>108</td>
<td>2</td>
<td>4</td>
<td>4</td>
<td>16</td>
<td></td>
<td>( \text{dB} )</td>
</tr>
<tr>
<td>Power Supply Rejection Ratio</td>
<td>( \text{PSRR} )</td>
<td>( V_S = \pm 4.5, \text{V} ) to ( \pm 18, \text{V} )</td>
<td>2</td>
<td>15</td>
<td>2</td>
<td>4</td>
<td>32</td>
<td></td>
<td>( \mu\text{V/} \text{V} )</td>
</tr>
<tr>
<td>Large-Signal Voltage Gain</td>
<td>( A_{VO} )</td>
<td>( R_L \geq 2, \text{k}\Omega, V_O = \pm 10, \text{V} )</td>
<td>600</td>
<td>1200</td>
<td>300</td>
<td>800</td>
<td></td>
<td></td>
<td>( \text{V/mV} )</td>
</tr>
<tr>
<td>Output Voltage Swing</td>
<td>( V_O )</td>
<td>( R_L \geq 2, \text{k}\Omega )</td>
<td>±11.5</td>
<td>±13.5</td>
<td>±10.5</td>
<td>±13.0</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
</tbody>
</table>

### NOTES

1. Input offset voltage measurements are performed by automated test equipment approximately 0.5 seconds after application of power. A/E grades guaranteed fully warmed up.
2. The \( TCV_{OS} \) performance is within the specifications unnullled or when nulled with \( R_P = 8\, \text{k}\Omega \) to 20\, \text{k}\Omega. \( TCV_{OSN} \) is 100% tested for A/E grades, sample tested for F/G grades.
3. Guaranteed by design.
## Wafer Test Limits

### Parameters

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Conditions</th>
<th>OP37NT Limit</th>
<th>OP37N Limit</th>
<th>OP37GT Limit</th>
<th>OP37G Limit</th>
<th>OP37GR Limit</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Offset Voltage</td>
<td>V&lt;sub&gt;OS&lt;/sub&gt;</td>
<td>Note 1</td>
<td>60</td>
<td>35</td>
<td>200</td>
<td>60</td>
<td>100</td>
<td>µV MAX</td>
</tr>
<tr>
<td>Input Offset Current</td>
<td>I&lt;sub&gt;OS&lt;/sub&gt;</td>
<td>50</td>
<td>35</td>
<td>85</td>
<td>50</td>
<td>75</td>
<td>nA MAX</td>
<td></td>
</tr>
<tr>
<td>Input Bias Current</td>
<td>I&lt;sub&gt;B&lt;/sub&gt;</td>
<td>±60</td>
<td>±40</td>
<td>±95</td>
<td>±55</td>
<td>±80</td>
<td>nA MAX</td>
<td></td>
</tr>
<tr>
<td>Input Voltage Range</td>
<td>IVR</td>
<td>±10.3</td>
<td>±11</td>
<td>±10.3</td>
<td>±11</td>
<td>±11</td>
<td>V MIN</td>
<td></td>
</tr>
<tr>
<td>Common Mode Rejection Ratio</td>
<td>CMRR</td>
<td>V&lt;sub&gt;CM&lt;/sub&gt; = ±11 V</td>
<td>108</td>
<td>114</td>
<td>100</td>
<td>106</td>
<td>100</td>
<td>dB MIN</td>
</tr>
<tr>
<td>Power Supply Rejection Ratio</td>
<td>PSRR</td>
<td>T&lt;sub&gt;A&lt;/sub&gt; = 25°C, V&lt;sub&gt;S&lt;/sub&gt; = ±4 V to ±18 V</td>
<td>10</td>
<td>10</td>
<td>10</td>
<td>10</td>
<td>20</td>
<td>µV/V MAX</td>
</tr>
<tr>
<td></td>
<td></td>
<td>T&lt;sub&gt;A&lt;/sub&gt; = 125°C, V&lt;sub&gt;S&lt;/sub&gt; = ±4.5 V to ±18 V</td>
<td>16</td>
<td>20</td>
<td></td>
<td></td>
<td></td>
<td>µV/V MAX</td>
</tr>
<tr>
<td>Large-Signal Voltage Gain</td>
<td>A&lt;sub&gt;VO&lt;/sub&gt;</td>
<td>R&lt;sub&gt;L&lt;/sub&gt; ≥ 2 kΩ, V&lt;sub&gt;O&lt;/sub&gt; = ±10 V</td>
<td>600</td>
<td>1000</td>
<td>500</td>
<td>1000</td>
<td>700</td>
<td>V/mV MIN</td>
</tr>
<tr>
<td></td>
<td></td>
<td>R&lt;sub&gt;L&lt;/sub&gt; ≥ 1 kΩ, V&lt;sub&gt;O&lt;/sub&gt; = ±10 V</td>
<td></td>
<td></td>
<td>800</td>
<td>800</td>
<td></td>
<td>V/mV MIN</td>
</tr>
<tr>
<td>Output Voltage Swing</td>
<td>V&lt;sub&gt;O&lt;/sub&gt;</td>
<td>R&lt;sub&gt;L&lt;/sub&gt; ≥ 2.5 kΩ</td>
<td>±11.5</td>
<td>±12</td>
<td>±11</td>
<td>±12</td>
<td>±11.5</td>
<td>V MIN</td>
</tr>
<tr>
<td></td>
<td></td>
<td>R&lt;sub&gt;L&lt;/sub&gt; ≥ 600 kΩ</td>
<td>±10</td>
<td>±10</td>
<td>±10</td>
<td>±10</td>
<td>V MIN</td>
<td></td>
</tr>
<tr>
<td>Power Consumption</td>
<td>P&lt;sub&gt;d&lt;/sub&gt;</td>
<td>V&lt;sub&gt;O&lt;/sub&gt; = 0</td>
<td>140</td>
<td>140</td>
<td>170</td>
<td></td>
<td></td>
<td>mW MAX</td>
</tr>
</tbody>
</table>

### Notes

- For 25°C characteristics of OP37NT and OP37GT devices, see OP37N and OP37G characteristics, respectively.
- Electrical tests are performed at wafer probe to the limits shown. Due to variations in assembly methods and normal yield loss, yield after packaging is not guaranteed for standard product dice. Consult factory to negotiate specifications based on dice lot qualification through sample lot assembly and testing.
## OP37

Typical Electrical Characteristics \( (V_S = \pm 15 \text{ V}, T_A = 25^\circ \text{C}, \text{unless otherwise noted}) \)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Conditions</th>
<th>OP37NT Typical</th>
<th>OP37N Typical</th>
<th>OP37GT Typical</th>
<th>OP37G Typical</th>
<th>OP37GR Typical</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Average Input Offset Voltage Drift</td>
<td>TCV_{OS} or</td>
<td>Nulled or Unnullled</td>
<td>0.2</td>
<td>0.2</td>
<td>0.3</td>
<td>0.3</td>
<td>0.4</td>
<td>( \mu \text{V/}^\circ \text{C} )</td>
</tr>
<tr>
<td></td>
<td>TCV_{OSN}</td>
<td>( R_P = 8 \text{ k}\Omega ) to 20 k\Omega</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Average Input Offset Current Drift</td>
<td>TCI_{OS}</td>
<td>Nulled</td>
<td>80</td>
<td>80</td>
<td>130</td>
<td>130</td>
<td>180</td>
<td>( \text{pA/}^\circ \text{C} )</td>
</tr>
<tr>
<td>Average Input Bias Current Drift</td>
<td>TCI_{B}</td>
<td>Nulled</td>
<td>100</td>
<td>100</td>
<td>160</td>
<td>160</td>
<td>200</td>
<td>( \text{pA/}^\circ \text{C} )</td>
</tr>
<tr>
<td>Input Noise Voltage Density</td>
<td>( e_n )</td>
<td>( f_0 = 10 \text{ Hz} )</td>
<td>3.5</td>
<td>3.5</td>
<td>3.5</td>
<td>3.5</td>
<td>3.8</td>
<td>( \text{nV/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td></td>
<td>( f_0 = 30 \text{ Hz} )</td>
<td></td>
<td>3.1</td>
<td>3.1</td>
<td>3.1</td>
<td>3.1</td>
<td>3.3</td>
<td>( \text{nV/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td></td>
<td>( f_0 = 1000 \text{ Hz} )</td>
<td></td>
<td>3.0</td>
<td>3.0</td>
<td>3.0</td>
<td>3.0</td>
<td>3.2</td>
<td>( \text{nV/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td>Input Noise Voltage Density</td>
<td>( i_n )</td>
<td>( f_0 = 10 \text{ Hz} )</td>
<td>1.7</td>
<td>1.7</td>
<td>1.7</td>
<td>1.7</td>
<td>1.7</td>
<td>( \text{pA/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td></td>
<td>( f_0 = 30 \text{ Hz} )</td>
<td></td>
<td>1.0</td>
<td>1.0</td>
<td>1.0</td>
<td>1.0</td>
<td>1.0</td>
<td>( \text{pA/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td></td>
<td>( f_0 = 1000 \text{ Hz} )</td>
<td></td>
<td>0.4</td>
<td>0.4</td>
<td>0.4</td>
<td>0.4</td>
<td>0.4</td>
<td>( \text{pA/}^\sqrt{\text{Hz}} )</td>
</tr>
<tr>
<td>Input Noise Voltage</td>
<td>( e_n_{p-p} )</td>
<td>0.1 Hz to 10 Hz</td>
<td>0.08</td>
<td>0.08</td>
<td>0.08</td>
<td>0.08</td>
<td>0.09</td>
<td>( \mu \text{V p-p} )</td>
</tr>
<tr>
<td>Slew Rate</td>
<td>SR</td>
<td>( R_L \geq 2k \text{ \Omega} )</td>
<td>17</td>
<td>17</td>
<td>17</td>
<td>17</td>
<td>17</td>
<td>V/\mu s</td>
</tr>
<tr>
<td>Gain Bandwidth Product</td>
<td>GBW</td>
<td>( f_0 = 10 \text{ kHz} )</td>
<td>63</td>
<td>63</td>
<td>63</td>
<td>63</td>
<td>63</td>
<td>MHz</td>
</tr>
</tbody>
</table>
TPC 1. Noise-Tester Frequency Response (0.1 Hz to 10 Hz)

TPC 2. Voltage Noise Density vs. Frequency

TPC 3. A Comparison of Op Amp Voltage Noise Spectra

TPC 4. Input Wideband Voltage Noise vs. Bandwidth (0.1 Hz to Frequency Indicated)

TPC 5. Total Noise vs. Source Resistance

TPC 6. Voltage Noise Density vs. Temperature

TPC 7. Voltage Noise Density vs. Supply Voltage

TPC 8. Current Noise Density vs. Frequency

TPC 9. Supply Current vs. Supply Voltage
TPC 10. Offset Voltage Drift of Eight Representative Units vs. Temperature

TPC 11. Long-Term Offset Voltage Drift of Six Representative Units

TPC 12. Warm Up Offset Voltage Drift

TPC 13. Offset Voltage Change Due to Thermal Shock

TPC 14. Input Bias Current vs. Temperature

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TPC 16. Open-Loop Gain vs. Frequency

TPC 17. Slew Rate, Gain Bandwidth Product, Phase Margin vs. Temperature

TPC 18. Gain, Phase Shift vs. Frequency
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TPC 19. Open-Loop Voltage Gain vs. Supply Voltage

TPC 20. Maximum Output Swing vs. Frequency

TPC 21. Maximum Output Voltage vs. Load Resistance

TPC 22. Small-Signal Overshoot vs. Capacitive Load

TPC 23. Large-Signal Transient Response

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TPC 31. PSRP vs. Frequency

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TPC 33. Slew Rate vs. Supply Voltage
APPLICATIONS INFORMATION

OP37 Series units may be inserted directly into 725 and OP07 sockets with or without removal of external compensation or nulling components. Additionally, the OP37 may be fitted to unnulled 741 type sockets; however, if conventional 741 nulling circuitry is in use, it should be modified or removed to ensure correct OP37 operation. OP37 offset voltage may be nulled to zero (or other desired setting) using a potentiometer (see offset nulling circuit).

The OP37 provides stable operation with load capacitances of up to 1000 pF and ±10 V swings; larger capacitances should be decoupled with a 50 Ω resistor inside the feedback loop. Closed loop gain must be at least five. For closed loop gain between five to ten, the designer should consider both the OP27 and the OP37. For gains above ten, the OP37 has a clear advantage over the unity stable OP27.

Thermoelectric voltages generated by dissimilar metals at the input terminal contacts can degrade the drift performance. Best operation will be obtained when both input contacts are maintained at the same temperature.

**Noise Measurements**

To measure the 80 nV peak-to-peak noise specification of the OP37 in the 0.1 Hz to 10 Hz range, the following precautions must be observed:

- The device has to be warmed-up for at least five minutes. As shown in the warm-up drift curve, the offset voltage typically changes 4 µV due to increasing chip temperature after power up. In the ten second measurement interval, these temperature-induced effects can exceed tens of nanovolts.
- For similar reasons, the device has to be well-shielded from air currents. Shielding minimizes thermocouple effects.
- Sudden motion in the vicinity of the device can also “feedthrough” to increase the observed noise.
- The test time to measure 0.1 Hz to 10 Hz noise should not exceed 10 seconds. As shown in the noise-tester frequency response curve, the 0.1 Hz corner is defined by only one zero. The test time of ten seconds acts as an additional zero to eliminate noise contributions from the frequency band below 0.1 Hz.
- A noise-voltage-density test is recommended when measuring noise on a large number of units. A 10 Hz noise-voltage-density measurement will correlate well with a 0.1 Hz-to-10 Hz peak-to-peak noise reading, since both results are determined by the white noise and the location of the 1/f corner frequency.

**Optimizing Linearity**

Best linearity will be obtained by designing for the minimum output current required for the application. High gain and excellent linearity can be achieved by operating the op amp with a peak output current of less than ±10 mA.

**Instrumentation Amplifier**

A three-op-amp instrumentation amplifier provides high gain and wide bandwidth. The input noise of the circuit below is 4.9 nV/√Hz. The gain of the input stage is set at 25 and the gain of the second stage is 40; overall gain is 1000. The amplifier bandwidth of 800 kHz is extraordinarily good for a precision instrumentation amplifier. Set to a gain of 1000, this yields a gain bandwidth product of 800 MHz. The full-power bandwidth for a 20 V p-p output is 250 kHz. Potentiometer R7 provides quadrature trimming to optimize the instrumentation amplifier’s ac common-mode rejection.
Comments on Noise

The OP37 is a very low-noise monolithic op amp. The outstanding input voltage noise characteristics of the OP37 are achieved mainly by operating the input stage at a high quiescent current. The input bias and offset currents, which would normally increase, are held to reasonable values by the input bias current cancellation circuit. The OP37A/E has $I_B$ and $I_{OS}$ of only $\pm 40 \text{nA}$ and $35 \text{nA}$ respectively at $25^\circ C$. This is particularly important when the input has a high source resistance. In addition, many audio amplifier designers prefer to use direct coupling. The high $I_B$ TCVOS of previous designs have made direct coupling difficult, if not impossible, to use.

Figure 5. Noise vs. Resistance (Including Resistor Noise @ 1000 Hz)

Voltage noise is inversely proportional to the square-root of bias current, but current noise is proportional to the square-root of bias current. The OP37’s noise advantage disappears when high source-resistors are used. Figures 5, 6, and 7 compare OP-37 observed total noise with the noise performance of other devices in different circuit applications.

Total noise = $\sqrt{[\text{Voltage noise}]^2 + (\text{current noise} \times RS)^2 + \text{(resistor noise)}^2}/2$

Figure 5 shows noise versus source resistance at 1000 Hz. The same plot applies to wideband noise. To use this plot, just multiply the vertical scale by the square-root of the bandwidth.

Figure 6. Peak-to-Peak Noise (0.1 Hz to 10 Hz) vs. Source Resistance (Includes Resistor Noise)

At $R_S < 1 \text{k}\Omega$ key the OP37’s low voltage noise is maintained. With $R_S < 1 \text{k}\Omega$, total noise increases, but is dominated by the resistor noise rather than current or voltage noise. It is only beyond $R_S$ of 20kil that current noise starts to dominate. The argument can be made that current noise is not important for applications with low to-moderate source resistances. The crossover between the OP37 and OP07 and OP08 noise occurs in the 15 k$\Omega$ to 40 k$\Omega$ region.

Figure 7. 10 Hz Noise vs. Source resistance (Includes Resistor Noise)

Figure 6 shows the 0.1 Hz to 10 Hz peak-to-peak noise. Here the picture is less favorable; resistor noise is negligible, current noise becomes important because it is inversely proportional to the square-root of frequency. The crossover with the OP-07 occurs in the 3 k$\Omega$ to 5 k$\Omega$ range depending on whether balanced or unbalanced source resistors are used (at 3 k$\Omega$ the $I_B$. $I_{OS}$ error also can be three times the VOS spec.).

Therefore, for low-frequency applications, the OP07 is better than the OP27/37 when Rs > 3 k$\Omega$. The only exception is when gain error is important. Figure 3 illustrates the 10 Hz noise. As expected, the results are between the previous two figures.

For reference, typical source resistances of some signal sources are listed in Table I.
Table I. TBD

<table>
<thead>
<tr>
<th>Device</th>
<th>Source Impedance</th>
<th>Comments</th>
</tr>
</thead>
<tbody>
<tr>
<td>Strain Gauge</td>
<td>&lt;500 Ω</td>
<td>Typically used in low-frequency applications.</td>
</tr>
<tr>
<td>Magnetic Tapehead</td>
<td>&lt;1500 Ω</td>
<td>Low I_B very important to reduce set-magnetization problems when direct coupling is used. OP37 I_B can be neglected.</td>
</tr>
<tr>
<td>Magnetic Phonograph Cartridges</td>
<td>&lt;1500 Ω</td>
<td>Similar need for low I_B in direct coupled applications. OP47 will not introduce any self-magnetization problem.</td>
</tr>
<tr>
<td>Linear Variable Differential Transformer</td>
<td>&lt;1500 Ω</td>
<td>Used in rugged servo-feedback applications. Bandwidth of interest is 400 Hz to 5 kHz.</td>
</tr>
</tbody>
</table>

Audio Applications
The following applications information has been abstracted from a PMI article in the 12/20/80 issue of Electronic Design magazine and updated.

For initial equalization accuracy and stability, precision metal-film resistors and film capacitors of polystyrene or polypropylene are recommended since they have low voltage coefficients, dissipation factors, and dielectric absorption. (High-K ceramic capacitors should be avoided here, though low-K ceramics—such as NPO types, which have excellent dissipation factors, and somewhat lower dielectric absorption—can be considered for small values or where space is at a premium.)

The OP27 brings a 3.2 nV/√Hz voltage noise and 0.45 pA/√Hz current noise to this circuit. To minimize noise from other sources, R3 is set to a value of 100 Ω, which generates a voltage noise of 1.3 nV/√Hz. The noise increases the 3.2 nV/√Hz of the amplifier by only 0.7 dB. With a 1 kΩ source, the circuit noise measures 63 dB below a 1 mV reference level, unweighted, in a 20 kHz noise bandwidth.

Gain (G) of the circuit at 1 kHz can be calculated by the expression:

\[ G = 0.101 \left(1 + \frac{R_3}{R_1}\right) \]

For the values shown, the gain is just under 100 (or 40 dB). Lower gains can be accommodated by increasing R3, but gains higher than 40 dB will show more equalization errors because of the 8 MHz gain bandwidth of the OP27.

This circuit is capable of very low distortion over its entire range, generally below 0.01% at levels up to 7 V rms. At 3 V output levels, it will produce less than 0.03% total harmonic distortion at frequencies up to 20 kHz.

Capacitor C3 and resistor R4 form a simple –6 dB per octave rumble filter, with a corner at 22 Hz. As an option, the switch selected shunt capacitor C4, a nonpolarized electrolytic, bypasses the low-frequency rolloff. Placing the rumble filter’s high-pass action after the preamp has the desirable result of discriminating against the RIAA amplified low frequency noise components and pickup-produced low-frequency disturbances.

A preamplifier for NAB tape playback is similar to an RIAA phono preamp, though more gain is typically demanded, along with equalization requiring a heavy low-frequency boost. The circuit in Figure 4 can be readily modified for tape use, as shown by Figure 5.

The tape-equalization requirement has a flat high frequency gain above 3 kHz (τ2 = 50 μs), the amplifier need not be stabilized for unity gain. The uncompensated OP37 provides a greater bandwidth and slew rate. For many applications, the idealized time constants shown may require trimming of Ra and R2 to optimize frequency response for non ideal tape head performance and other factors.

The network values of the configuration yield a 50 dB gain at 1 kHz, and the dc gain is greater than 70 dB. Thus, the worst-case output offset is just over 500 mV. A single 0.47 μF output capacitor can block this level without affecting the dynamic range.

The tape head can be coupled directly to the amplifier input, since the worst-case bias current of 85 nA with a 400 mH, 100 μm. head (such as the PRB2H7K) will not be troublesome.

One potential tape-head problem is presented by amplifier bias current transients which can magnetize a head. The OP27 and...
OP37

OP37 are free of bias-current transients upon power up or power down. However, it is always advantageous to control the speed of power supply rise and fall, to eliminate transients.

In addition, the dc resistance of the head should be carefully controlled, and preferably below 1 kΩ. For this configuration, the bias-current induced offset voltage can be greater than the 170 pV maximum offset if the head resistance is not sufficiently controlled.

A simple, but effective, fixed-gain transformerless microphone preamp (Figure 10) amplifies differential signals from low impedance microphones by 50 dB, and has an input impedance of 2 kΩ. Because of the high working gain of the circuit, an OP37 helps to preserve bandwidth, which will be 110 kHz. As the OP37 is a decompensated device (minimum stable gain of 5), a dummy resistor, Rp, may be necessary, if the microphone is to be unplugged. Otherwise the 100% feedback from the open input may cause the amplifier to oscillate.

Common-mode input-noise rejection will depend upon the match of the bridge-resistor ratios. Either close-tolerance (0.1%) types should be used, or R4 should be trimmed for best CMRR. All resistors should be metal-film types for best stability and low noise.

Noise performance of this circuit is limited more by the input resistors R1 and R2 than by the op amp, as R1 and R2 each generate a 4 nV/√Hz noise, while the op amp generates a 3.2 nV/√Hz noise. The rms sum of these predominant noise sources will be about 6 nV/√Hz, equivalent to 0.9 μV in a 20 kHz noise bandwidth, or nearly 61 dB below a 1 mV input signal. Measurements confirm this predicted performance.

For applications demanding appreciably lower noise, a high quality microphone-transformer-coupled preamp (Figure 11) incorporates the internally compensated. T1 is a JE-115K-E 150 Ω/15 kΩ transformer which provides an optimum source resistance for the OP27 device. The circuit has an overall gain of 40 dB, the product of the transformer’s voltage setup and the op amp’s voltage gain.

Gain may be trimmed to other levels, if desired, by adjusting R2 or R1. Because of the low offset voltage of the OP27, the output offset of this circuit will be very low, 1.7 mV or less, for a 40 dB gain. The typical output blocking capacitor can be eliminated in such cases, but is desirable for higher gains to eliminate switching transients.

Capacitor C2 and resistor R2 form a 2 μs time constant in this circuit, as recommended for optimum transient response by the transformer manufacturer. With C2 in use, A1 must have unity-gain stability. For situations where the 2 μs time constant is not necessary, C2 can be deleted, allowing the faster OP37 to be employed.

Some comment on noise is appropriate to understand the capability of this circuit. A 150 Ω resistor and R1 and R2 gain resistors connected to a noiseless amplifier will generate 220 nV of noise in a 20 kHz bandwidth, or 73 dB below a 1 mV reference level. Any practical amplifier can only approach this noise level; it can never exceed it. With the OP27 and T1 specified, the additional noise degradation will be close to 3.6 dB (or -69.5 referenced to 1 mV).

References

Figure 10. TBD

![Figure 11. TBD](image-url)

The circuit has an overall gain of 40 dB, the product of the transformer’s voltage setup and the op amp’s voltage gain.
OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

8-Lead Hermetic DIP
(Z Suffix)

- PIN 1: 0.005 (0.13) MIN, 0.055 (1.4) MAX
- 0.310 (7.87), 0.220 (5.59)
- 0.015 (0.38), 0.008 (0.20)
- 0.320 (8.13), 0.290 (7.37)
- SEATING PLANE: 0.200 (5.08) MAX, 0.125 (3.18) MIN
- 0.015 (0.38), 0.008 (0.20)

Epoxy Mini-Dip
(P Suffix)

- PIN 1: 0.060 (1.52), 0.015 (0.38)
- 0.280 (7.11), 0.224 (5.70)
- 0.022 (0.56), 0.007 (0.19)
- SEATING PLANE: 0.0098 (0.25), 0.0040 (0.10)
- 0.0192 (0.49), 0.0138 (0.35)

8-Lead SO
(S Suffix)

- PIN 1: 0.0500 (1.27)
- 0.0098 (0.25), 0.0040 (0.10)
- 0.0192 (0.49), 0.0138 (0.35)
- SEATING PLANE: 0.0196 (0.50), 0.0099 (0.25)
- 0.0192 (0.49), 0.0138 (0.35)
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