## 捷多邦,专业PCB打样工厂,24小时加急出货

#### October 2004

350mW (typ)

0.1µA (typ)

National Semiconductor LM4879 Boomer<sup>®</sup> Audio Power Amplifier Series

## 1.1 Watt Audio Power Amplifier

## **General Description**

The LM4879 is an audio power amplifier primarily designed for demanding applications in mobile phones and other portable communication device applications. It is capable of delivering 1.1 watt of continuous average power to an  $8\Omega$  BTL load with less than 1% distortion (THD+N) from a  $5V_{DC}$  power supply.

Boomer audio power amplifiers were designed specifically to provide high quality output power with a minimal amount of external components. The LM4879 does not require output coupling capacitors or bootstrap capacitors, and therefore is ideally suited for lower-power portable applications where minimal space and power consumption are primary requirements.

The LM4879 features a low-power consumption global shutdown mode, which is achieved by driving the shutdown pin with logic low. Additionally, the LM4879 features an internal thermal shutdown protection mechanism.

The LM4879 contains advanced pop & click circuitry which eliminates noises which would otherwise occur during turn-on and turn-off transitions.

The LM4879 is unity-gain stable and can be configured by external gain-setting resistors.

## **Key Specifications**

- PSRR: 5V, 3V @ 217Hz
   62dB (typ)

   Power Output at 5V & 1% THD+N
   1.1W (typ)
- Power Output at 3V & 1% THD+N
- Shutdown Current

## **Features**

- No output coupling capacitors, snubber networks or bootstrap capacitors required
- Unity gain stable
- Ultra low current shutdown mode
- Fast turn on: 80ms (typ), 110ms (max) with 1.0μF capacitor
- BTL output can drive capacitive loads up to 100pF
- Advanced pop & click circuitry eliminates noises during turn-on and turn-off transitions
- 2.2V 5.0V operation
- Available in space-saving µSMD, LLP, and MSOP packages

## Applications

- Mobile Phones
- PDAs
- Portable electronic devices



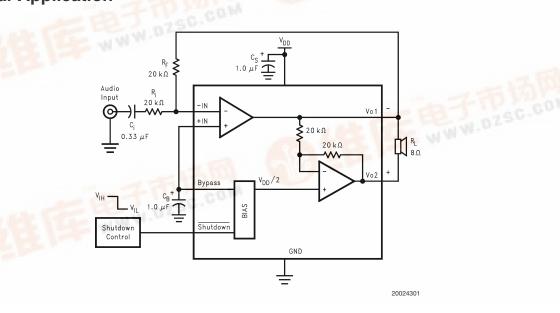
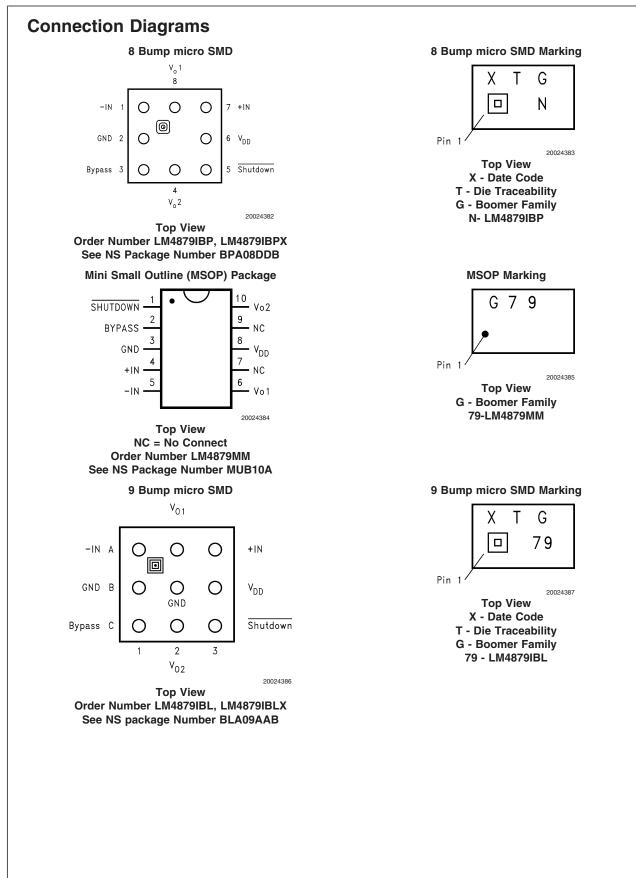


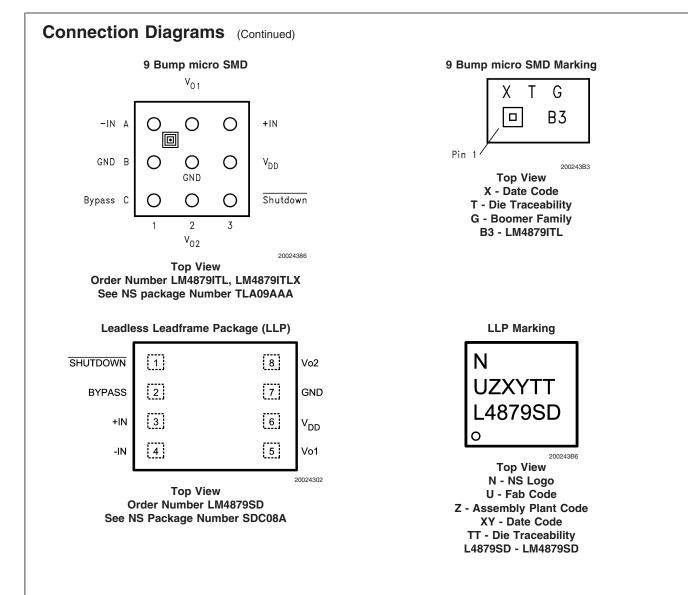
FIGURE 1. Typical Audio Amplifier Application Circuit

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## Absolute Maximum Ratings (Note 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Supply Voltage (Note 9)	6.0V
Storage Temperature	–65°C to +150°C
Input Voltage	–0.3V to V <sub>DD</sub> +0.3V
Power Dissipation (Note 3)	Internally Limited
ESD Susceptibility (Note 4)	2000V
ESD Susceptibility (Note 5)	200V
Junction Temperature	150°C
Thermal Resistance	

$\theta_{JA}$ (BPA08DDB)	220°C/W (Note 10)
$\theta_{JA}$ (SDC08A)	64°C/W (Note 12)
$\theta_{JA}$ (TLA09AAA)	180°C/W (Note 10)
$\theta_{JA}$ (BLA09AAB)	180°C/W (Note 10)
$\theta_{JC}$ (MUB10A)	56°C/W
$\theta_{JA}$ (MUB10A)	190°C/W

## **Operating Ratings**

Temperature Range

$T_{MIN} \le T_A \le T_{MAX}$	$-40^{\circ}C \leq T_A \leq 85^{\circ}C$
Supply Voltage	$2.2V \le V_{DD} \le 5.5V$

**Electrical Characteristics**  $V_{DD} = 5V$  (Notes 1, 2) The following specifications apply for the circuit shown in Figure 1 unless otherwise specified. Limits apply for  $T_A = 25^{\circ}C$ .

			LM4879		
Symbol	Parameter	Conditions	Typical	Limit	Units
			(Note 6)	(Notes 7, 8)	(Limits)
I <sub>DD</sub>	Quiescent Power Supply Current	$V_{IN} = 0V, 8\Omega BTL$	5	10	mA (max)
I <sub>SD</sub>	Shutdown Current	V <sub>shutdown</sub> = GND	0.1	2.0	µA (max)
V <sub>os</sub>	Output Offset Voltage		5	40	mV (max)
Po	Output Power	THD+N = 1% (max); f = 1kHz	1.1	0.9	W (min)
THD+N	Total Harmonic Distortion+Noise	$P_o = 0.4$ Wrms; f = 1kHz	0.1		%
PSRR	Power Supply Rejection Ratio	$V_{ripple} = 200 mVsine p-p, C_B = 1.0 \mu F$ Input terminated with $10\Omega$ to ground	68 (f = 1kHz) 62 (f = 217Hz)	55	dB (min)
V <sub>SDIH</sub>	Shutdown High Input Voltage			1.4	V (min)
V <sub>SDIL</sub>	Shutdown Low Input Voltage			0.4	V (max)
Τ <sub>WU</sub>	Wake-up Time	C <sub>B</sub> = 1.0μF	80	110	ms (max)
N <sub>OUT</sub>	Output Noise	A-Weighted; Measured across $8\Omega$ BTL Input terminated with $10\Omega$ to ground	26		μV <sub>RMS</sub>

**Electrical Characteristics**  $V_{DD}$  = **3.0V** (Notes 1, 2) The following specifications apply for the circuit shown in Figure 1 unless otherwise specified. Limits apply for  $T_A = 25^{\circ}C$ .

			LM4879		l los ito
Symbol	Parameter	Conditions	Typical	Limit	Units (Limits)
			(Note 6)	(Notes 7, 8)	(Linnis)
I <sub>DD</sub>	Quiescent Power Supply Current	$V_{IN} = 0V, 8\Omega BTL$	4.5	9	mA (max)
I <sub>SD</sub>	Shutdown Current	V <sub>shutdown</sub> = GND	0.1	2.0	μA (max)
V <sub>os</sub>	Output Offset Voltage		5	40	mV (max)
Po	Output Power	THD+N = 1% (max); f = 1kHz	350	320	mW
THD+N	Total Harmonic Distortion+Noise	$P_o = 0.15$ Wrms; f = 1kHz	0.1		%
PSRR	Power Supply Rejection Ratio	$V_{ripple} = 200 mVsine p-p, C_B = 1.0 \mu F$ Input terminated with 10 $\Omega$ to ground	68 (f = 1kHz) 62 (f = 217Hz)	55	dB (min)
V <sub>SDIH</sub>	Shutdown High Input Voltage			1.4	V (min)
V <sub>SDIL</sub>	Shutdown Low Input Voltage			0.4	V (max)
Τ <sub>wu</sub>	Wake-up Time	С <sub>в</sub> = 1.0µF	80	110	ms (max)

**Electrical Characteristics**  $V_{DD} = 3.0V$  (Notes 1, 2) The following specifications apply for the circuit shown in Figure 1 unless otherwise specified. Limits apply for T<sub>A</sub> = 25°C. (Continued)

	Parameter	Conditions	LM4879		
Symbol			Typical	Limit	Units (Limits)
			(Note 6)	(Notes 7, 8)	
		A-Weighted; Measured across $8\Omega$			
N <sub>OUT</sub> O	Output Noise	BTL	26		μV <sub>RMS</sub>
		Input terminated with $10\Omega$ to			
		ground			

**Electrical Characteristics**  $V_{DD} = 2.6V$  (Notes 1, 2) The following specifications apply for the circuit shown in Figure 1 unless otherwise specified. Limits apply for  $T_A = 25^{\circ}C$ .

			LM4879		
Symbol	Parameter	Conditions	Typical	Limit	Units
			(Note 6)	(Notes 7, 8)	(Limits)
I <sub>DD</sub>	Quiescent Power Supply Current	$V_{IN} = 0V, 8\Omega BTL$	3.5		mA
I <sub>SD</sub>	Shutdown Current	V <sub>shutdown</sub> = GND	0.1		μA
V <sub>os</sub>	Output Offset Voltage		5		mV
		THD+N = 1% (max); f = 1kHz			
P <sub>o</sub> Output Power	Output Power	$R_L = 8\Omega$	250		100
		$R_L = 4\Omega$	350		mW
THD+N	Total Harmonic Distortion+Noise	$P_o = 0.1$ Wrms; f = 1kHz	0.1		%
		$V_{ripple} = 200 \text{mVsine p-p}, C_{B} =$	55 (f = 1kHz)		
PSRR Power Supply I	Power Supply Pointion Potio	1.0µF	55 (f =		dB
	Power Supply Rejection Ratio	Input terminated with $10\Omega$ to	217Hz)		
		ground			

Note 1: All voltages are measured with respect to the ground pin, unless otherwise specified.

Note 2: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. Electrical Characteristics state DC and AC electrical specifications under particular test conditions which guarantee specific performance limits. This assumes that the device is within the Operating Ratings. Specifications are not guaranteed for parameters where no limit is given, however, the typical value is a good indication of device performance.

Note 3: The maximum power dissipation must be derated at elevated temperatures and is dictated by  $T_{JMAX}$ ,  $\theta_{JA}$ , and the ambient temperature  $T_A$ . The maximum allowable power dissipation is P<sub>DMAX</sub> = (T<sub>JMAX</sub>-T<sub>A</sub>)/θ<sub>JA</sub> or the number given in Absolute Maximum Ratings, whichever is lower. For the LM4879, see power derating curves for additional information.

Note 4: Human body model, 100pF discharged through a 1.5kΩ resistor.

Note 5: Machine Model, 220pF-240pF discharged through all pins.

Note 6: Typicals are measured at 25°C and represent the parametric norm.

Note 7: Limits are guaranteed to National's AOQL (Average Outgoing Quality Level).

Note 8: For micro SMD only, shutdown current is measured in a Normal Room Environment. Exposure to direct sunlight will increase ISD by a maximum of 2µA. Note 9: If the product is in shutdown mode, and V<sub>DD</sub> exceeds 6V (to a max of 8V V<sub>DD</sub>), then most of the excess current will flow through the ESD protection circuits. If the source impedance limits the current to a max of 10ma, then the part will be protected. If the part is enabled when V<sub>DD</sub> is above 6V, circuit performance will be curtailed or the part may be permanently damaged.

Note 10: All bumps have the same thermal resistance and contribute equally when used to lower thermal resistance.

Note 11: Maximum power dissipation (P<sub>DMAX</sub>) in the device occurs at an output power level significantly below full output power. P<sub>DMAX</sub> can be calculated using Equation 1 shown in the Application section. It may also be obtained from the power dissipation graphs.

Note 12: The stated  $\theta_{IA}$  is achieved when the LLP package's DAP is soldered to a 4in<sup>2</sup> copper heatsink plain.

# External Components Description (Figure 1)

Components		Functional Description	
1.	R <sub>i</sub>	Inverting input resistance which sets the closed-loop gain in conjunction with $R_f$ . This resistor also forms a high pass filter with $C_i$ at $f_C = 1/(2\pi R_iC_i)$ .	
2.	Ci	Input coupling capacitor which blocks the DC voltage at the amplifiers input terminals. Also creates a highpass filter with $R_i$ at $f_c = 1/(2\pi R_iC_i)$ . Refer to the section, <b>Proper Selection of External Components</b> , for an explanation of how to determine the value of $C_i$ .	
3.	R <sub>f</sub>	Feedback resistance which sets the closed-loop gain in conjunction with R <sub>i</sub> .	
4.	Cs	Supply bypass capacitor which provides power supply filtering. Refer to the <b>Power Supply Bypassing</b> section for information concerning proper placement and selection of the supply bypass capacitor.	
5.	C <sub>B</sub>	Bypass pin capacitor which provides half-supply filtering. Refer to the section, <b>Proper Selection of External Components</b> , for information concerning proper placement and selection of C <sub>B</sub> .	

**THD+N vs Frequency** 

50 100 200 500 1k

**THD+N vs Frequency** 

FREQUENCY (Hz)

FREQUENCY (Hz)

50 100 200 500 1k 2k

**THD+N vs Power Out** 

 $V_{DD} = 3V, R_L = 8\Omega, f = 1kHz$ 

50m 100m 200m

OUTPUT POWER (W)

500m 1

20024342

5k 10k 20k

20024340

2k

5k 10k 20k

20024338

10

5

2

1 BW < 80 kHz

20

10

5

2

1

RL BW < 80 kHz $A_V = 2$ 

20

20

10

5

2

1

0.5

0.2

0.1

 $V_{DD} = 2.6V$  $P_0 = 100 \text{ mW}$ 

= 4Ω

11111

 $V_{DD} = 3V$ 

f = 1 kHz

 $R_{I} = 8 \Omega$ 

BW < 80 kHz

= 2

Α<sub>V</sub>

10m 20m

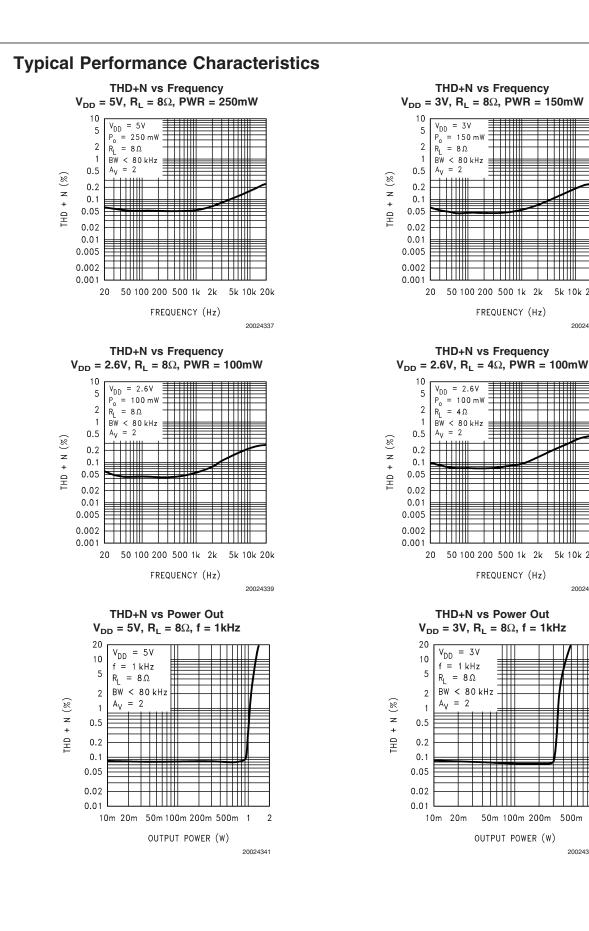
R

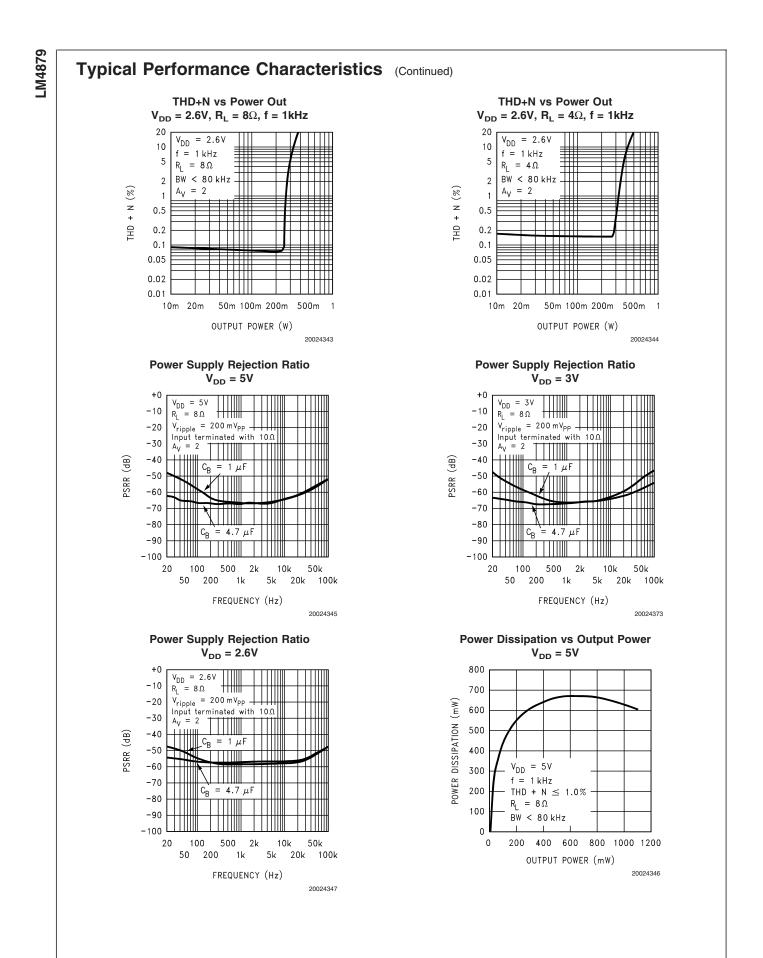
 $V_{DD} = 3V$ 

 $P_{0}^{-} = 150 \text{ mW}$ 

= 8 N

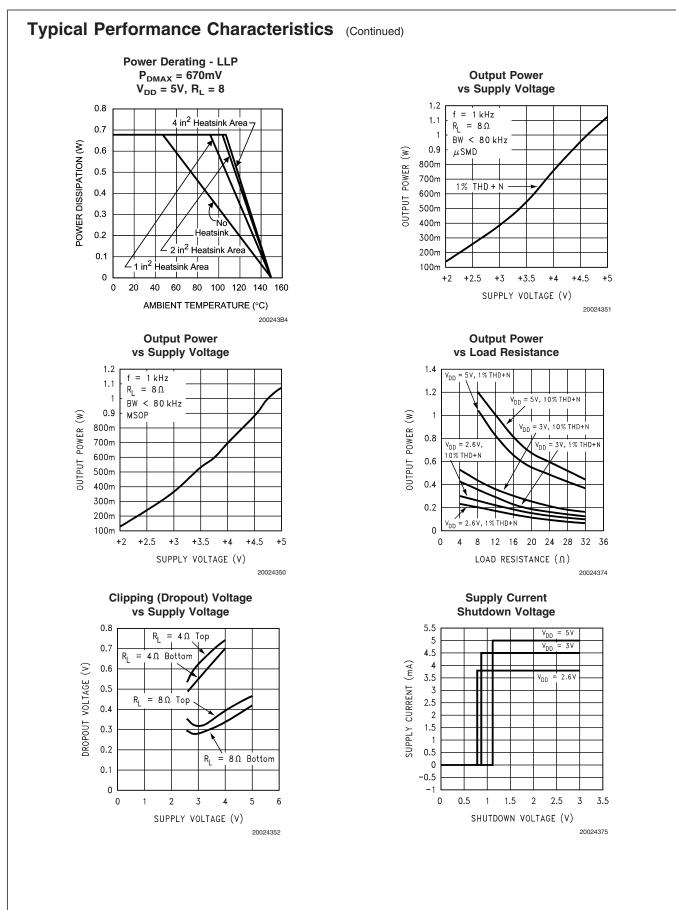
 $A_V = 2$ 





#### Typical Performance Characteristics (Continued) Power Dissipation **Power Dissipation** vs Output Power vs Output Power $V_{DD} = 3V$ $V_{DD} = 2.6V$ 300 350 ÷ 4Ω RL 300 250 POWER DISSIPATION (mW) POWER DISSIPATION (mW) 250 200 200 R = 8Ω 150 150 $V_{DD} = 3V$ 100 f = 1 kHz $V_{DD} = 2.6V$ 100 THD + N $\leq$ 1.0% $= 1 \, \text{kHz}$ f 50 $R_L = 8 \Omega$ 50 THD + N $\leq$ 1.0% BW < 80 kHzBW < 80 kHzΛ 0 0 50 100 150 200 250 300 350 400 450 0 50 100 150 200 250 300 OUTPUT POWER (mW) OUTPUT POWER (mW) 20024349 20024348 Power Dissipation **Power Derating - MSOP** vs Output Power (LLP Package) $P_{DMAX} = 670 mW$ $V_{DD} = 5V, R_L = 8\Omega$ $V_{DD} = 5V$ 0.8 1.4 $R_1 = 4\Omega$ 0.7 1.2 $\widehat{\mathbb{Z}}$ 0.6 POWER DISSIPATION (W) 1.0 MSOP POWER DISSIPATION 0.5 0.8 Note 11 R<sub>L</sub> = 8Ω 0.4 0.6 0.3 0.4 0.2 V<sub>DD</sub> = 5V 0.2 f = 1 kHz0.1 THD + N ≤ 1% BW < 80 kHz 0 0 0.4 1.2 1.6 0 0.8 2 50 100 150 200 0 OUTPUT POWER (W) AMBIENT TEMPERATURE (°C) 20024313 20024379 Power Derating - 8 Bump µSMD Power Derating - 9 Bump µSMD $P_{DMAX} = 670 \text{mW}$ $P_{DMAX} = 670 mW$ $V_{DD} = 5V, R_L = 8\Omega$ $V_{DD} = 5V, R_L = 8\Omega$ 0.8 0.8 PCB Heatsink Area PCB Heatsink Area 0.7 0.7 240 mm<sup>2</sup> 480 mm<sup>2</sup> POWER DISSIPATION (W) POWER DISSIPATION (W) 0.6 0.6 120 mm<sup>2</sup> 120 mm<sup>2</sup> 0.5 0.5 0 mm<sup>2</sup> 0.4 0.4 Note 11 0.3 0.3 $0 \text{ mm}^2$ 0.2 0.2 Note 11 0.1 0.1 0 0 20 40 60 80 100 120 140 160 0 50 100 150 200 0 AMBIENT TEMPERATURE (°C) AMBIENT TEMPERATURE (°C) 20024380 20024381





#### Typical Performance Characteristics (Continued) Shutdown Hysterisis Voltage Shutdown Hysterisis Voltage $V_{DD} = 5V$ $V_{DD} = 3V$ 6 5 V<sub>DD</sub> ÷ 5γ $V_{DD} = 3V$ 5 4 SUPPLY CURRENT (mA) SUPPLY CURRENT (mA) 4 3 OFF 3 OFF ١ I ON ÎON 2 2 1 1 0 0 0 0.5 1.5 2 2.5 3 0 0.5 1.5 2 2.5 3 1 1 SHUTDOWN VOLTAGE (V) SHUTDOWN VOLTAGE (V) 20024376 20024377 Shutdown Hysterisis Voltage **Open Loop** $V_{DD} = 2.6V$ **Frequency Response** 5 80 90 тт $V_{DD} = 2.6V$ GAIN $V_{DD} = 5V, 3V$ 70 60 50 pF С 4 60 30 SUPPLY CURRENT (mA) 50 0 3 40 -30 0 GAIN (dB) PHASE OFF PHASE ( ł 30 -60 ΟN 2 20 -90 10 -120 0 -150 1 -10 -180 -20 0 -210 0.5 1.5 2 2.5 0 1 3 100 1k 10k 100k 1M 10M SHUTDOWN VOLTAGE (V) FREQUENCY (Hz) 20024378 20024354 **Frequency Response** vs Input Capacitor Size +1 $\downarrow C_i = 1 \mu F$ -0 - 1 C; = $0.33 \ \mu F$ -2 OUTPUT LEVEL (dB) -3 -4 -5 -6 -7 -8 -9 -10 50 100 200 500 1k 2k 20 5k 10k 20k FREQUENCY (Hz) 20024356

## **Application Information**

### **BRIDGE CONFIGURATION EXPLANATION**

As shown in *Figure 1*, the LM4879 has two operational amplifiers internally, allowing for a few different amplifier configurations. The first amplifier's gain is externally configurable, while the second amplifier is internally fixed in a unity-gain, inverting configuration. The closed-loop gain of the first amplifier is set by selecting the ratio of R<sub>f</sub> to R<sub>i</sub> while the second amplifier's gain is fixed by the two internal 20 k $\Omega$  resistors. *Figure 1* shows that the output of amplifier one serves as the input to amplifier two which results in both amplifiers producing signals identical in magnitude, but out of phase by 180°. Consequently, the differential gain for the IC is

#### $A_{VD} = 2 (R_f/R_i)$

By driving the load differentially through outputs Vo1 and Vo2, an amplifier configuration commonly referred to as "bridged mode" is established. Bridged mode operation is different from the classical single-ended amplifier configuration where one side of the load is connected to ground.

A bridge amplifier design has a few distinct advantages over the single-ended configuration, as it provides differential drive to the load, thus doubling output swing for a specified supply voltage. Four times the output power is possible as compared to a single-ended amplifier under the same conditions. This increase in attainable output power assumes that the amplifier is not current limited or clipped. In order to choose an amplifier's closed-loop gain without causing excessive clipping, please refer to the **Audio Power Amplifier Design** section.

A bridge configuration, such as the one used in LM4879, also creates a second advantage over single-ended amplifiers. Since the differential outputs, Vo1 and Vo2, are biased at half-supply, no net DC voltage exists across the load. This eliminates the need for an output coupling capacitor which is required in a single supply, single-ended amplifier configuration. Without an output coupling capacitor, the half-supply bias across the load would result in both increased internal IC power dissipation and also possible loudspeaker damage.

#### POWER DISSIPATION

Power dissipation is a major concern when designing a successful amplifier, whether the amplifier is bridged or single-ended. A direct consequence of the increased power delivered to the load by a bridge amplifier is an increase in internal power dissipation. Since the LM4879 has two operational amplifiers in one package, the maximum internal power dissipation is 4 times that of a single-ended amplifier. The maximum power dissipation for a given application can be derived from the power dissipation graphs or from Equation 1.

$$P_{\rm DMAX} = 4^{*} (V_{\rm DD})^{2} / (2\pi^{2} R_{\rm L}) \qquad (1)$$

It is critical that the maximum junction temperature ( $T_{JMAX}$ ) of 150°C is not exceeded.  $T_{JMAX}$  can be determined from the power derating curves by using  $P_{DMAX}$  and the PC board foil area. By adding additional copper foil, the thermal resistance of the application can be reduced from a free air value of 150°C/W, resulting in higher  $P_{DMAX}$ . Additional copper foil can be added to any of the leads connected to the LM4879. It is especially effective when connected to  $V_{DD}$ , GND, and the output pins. Refer to the application information on the LM4879 reference design board for an example of good heat sinking. If  $T_{JMAX}$  still exceeds 150°C, then additional changes must be made. These changes can include re-

duced supply voltage, higher load impedance, or reduced ambient temperature. Internal power dissipation is a function of output power. Refer to the **Typical Performance Characteristics** curves for power dissipation information for different output powers and output loading.

### POWER SUPPLY BYPASSING

As with any amplifier, proper supply bypassing is critical for low noise performance and high power supply rejection. The capacitor location on both the bypass and power supply pins should be as close to the device as possible. Typical applications employ a 5V regulator with 10  $\mu$ F tantalum or electrolytic capacitor and a ceramic bypass capacitor which aid in supply stability. This does not eliminate the need for bypassing the supply nodes of the LM4879. The selection of a bypass capacitor, especially C<sub>B</sub>, is dependent upon PSRR requirements, click and pop performance (as explained in the section, **Proper Selection of External Components**), system cost, and size constraints.

#### SHUTDOWN FUNCTION

In order to reduce power consumption while not in use, the LM4879 contains a shutdown pin to externally turn off the amplifier's bias circuitry. This shutdown feature turns the amplifier off when a logic low is placed on the shutdown pin. By switching the shutdown pin to ground, the LM4879 supply current draw will be minimized in idle mode. While the device will be disabled with shutdown pin voltages less than  $0.4V_{DC}$ , the idle current may be greater than the typical value of  $0.1\mu$ A. (Idle current is measured with the shutdown pin tied to ground).

In many applications, a microcontroller or microprocessor output is used to control the shutdown circuitry to provide a quick, smooth transition into shutdown. Another solution is to use a single-pole, single-throw switch in conjunction with an external pull-up resistor. When the switch is closed, the shutdown pin is connected to ground which disables the amplifier. If the switch is open, then the external pull-up resistor to V<sub>DD</sub> will enable the LM4879. This scheme guarantees that the shutdown pin will not float thus preventing unwanted state changes.

#### **PROPER SELECTION OF EXTERNAL COMPONENTS**

Proper selection of external components in applications using integrated power amplifiers is critical to optimize device and system performance. While the LM4879 is tolerant of external component combinations, consideration to component values must be used to maximize overall system quality.

The LM4879 is unity-gain stable which gives the designer maximum system flexibility. The LM4879 should be used in low gain configurations to minimize THD+N values, and maximize the signal to noise ratio. Low gain configurations require large input signals to obtain a given output power. Input signals equal to or greater than 1 Vrms are available from sources such as audio codecs. Please refer to the section, **Audio Power Amplifier Design**, for a more complete explanation of proper gain selection.

Besides gain, one of the major considerations is the closedloop bandwidth of the amplifier. To a large extent, the bandwidth is dictated by the choice of external components shown in *Figure 1*. The input coupling capacitor,  $C_i$ , forms a first order high pass filter which limits low frequency response. This value should be chosen based on needed frequency response for a few distinct reasons.

(2)

## Application Information (Continued)

#### Selection Of Input Capacitor Size

Large input capacitors are both expensive and space hungry for portable designs. Clearly, a certain sized capacitor is needed to couple in low frequencies without severe attenuation. But in many cases the speakers used in portable systems, whether internal or external, have little ability to reproduce signals below 100 Hz to 150 Hz. Thus, using a large input capacitor may not increase actual system performance.

In addition to system cost and size, click and pop performance is effected by the size of the input coupling capacitor,  $C_i$ , A larger input coupling capacitor requires more charge to reach its quiescent DC voltage (nominally 1/2  $V_{DD}$ ). This charge comes from the output via the feedback and is apt to create pops upon device enable. Thus, by minimizing the capacitor size based on necessary low frequency response, turn-on pops can be minimized.

Besides minimizing the input capacitor size, careful consideration should be paid to the bypass capacitor value. Bypass capacitor, C<sub>B</sub>, is the most critical component to minimize turn-on pops since it determines how fast the LM4879 turns on. The slower the LM4879's outputs ramp to their quiescent DC voltage (nominally 1/2 V<sub>DD</sub>), the smaller the turn-on pop. Choosing C<sub>B</sub> equal to 1.0 µF along with a small value of C<sub>i</sub> (in the range of 0.1 µF to 0.39 µF), should produce a virtually clickless and popless shutdown function. While the device will function properly, (no oscillations or motorboating), with C<sub>B</sub> equal to 0.1 µF, the device will be much more susceptible to turn-on clicks and pops. Thus, a value of C<sub>B</sub> equal to 1.0 µF is recommended in all but the most cost sensitive designs.

#### AUDIO POWER AMPLIFIER DESIGN

#### A 1W/8Ω Audio Amplifier

Given:

Power Output	1 Wrms
Load Impedance	8Ω
Input Level	1 Vrms
Input Impedance	20 kΩ
Bandwidth	100 Hz–20 kHz ± 0.25 dB

A designer must first determine the minimum supply rail to obtain the specified output power. By extrapolating from the Output Power vs Supply Voltage graphs in the **Typical Per**- formance Characteristics section, the supply rail can be easily found. A second way to determine the minimum supply rail is to calculate the required V<sub>opeak</sub> using Equation 2 and add the output voltage. Using this method, the minimum supply voltage would be (V<sub>opeak</sub> + (V<sub>ODTOP</sub> + V<sub>ODBOT</sub>)), where V<sub>ODBOT</sub> and V<sub>ODTOP</sub> are extrapolated from the Dropout Voltage vs Supply Voltage curve in the **Typical Performance Characteristics** section.

$$V_{\text{opeak}} = \sqrt{(2R_LP_0)}$$

5V is a standard voltage, in most applications, chosen for the supply rail. Extra supply voltage creates headroom that allows the LM4879 to reproduce peaks in excess of 1W without producing audible distortion. At this time, the designer must make sure that the power supply choice along with the output impedance does not violate the conditions explained in the **Power Dissipation** section.

Once the power dissipation equations have been addressed, the required differential gain can be determined from Equation 3.

$$A_{VD} \ge \sqrt{(P_0 R_L)} / (V_{IN}) = V_{orms} / V_{inrms}$$

$$A_{VD} = (R_t / R_i) 2$$
(3)

From Equation 3, the minimum  $A_{VD}$  is 2.83; use  $A_{VD} = 3$ . Since the desired input impedance was 20 k $\Omega$ , and with a  $A_{VD}$  of 3, a ratio of 1.5:1 of  $R_f$  to  $R_i$  results in an allocation of  $R_i = 20 \ k\Omega$  and  $R_f = 30 \ k\Omega$ . The final design step is to address the bandwidth requirements which must be stated as a pair of -3 dB frequency points. Five times away from a -3 dB point is 0.17 dB down from passband response which is better than the required ±0.25 dB specified.

f<sub>L</sub> = 100 Hz/5 = 20 Hz

 $f_{H} = 20 \text{ kHz} * 5 = 100 \text{ kHz}$ 

As stated in the **External Components** section,  $R_i$  in conjunction with  $C_i$  create a highpass filter.

 $C_i \ge 1/(2\pi^20 \text{ k}\Omega^20 \text{ Hz}) = 0.397 \text{ }\mu\text{F}; \text{ use } 0.39 \text{ }\mu\text{F}$ 

The high frequency pole is determined by the product of the desired frequency pole,  $f_H$ , and the differential gain,  $A_{VD}$ . With a  $A_{VD}$  = 3 and  $f_H$  = 100 kHz, the resulting GBWP = 300 kHz which is much smaller than the LM4879 GBWP of 10 MHz. This figure displays that if a designer has a need to design an amplifier with a higher differential gain, the LM4879 can still be used without running into bandwidth limitations.

## Application Information (Continued)

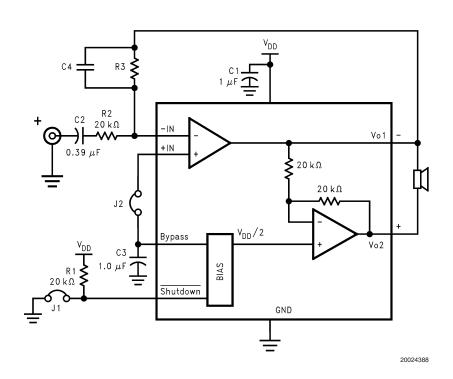


FIGURE 2. HIGHER GAIN AUDIO AMPLIFIER

The LM4879 is unity-gain stable and requires no external components besides gain-setting resistors, an input coupling capacitor, and proper supply bypassing in the typical application. However, if a closed-loop differential gain of greater than 10 is required, a feedback capacitor (C4) may be needed as shown in Figure 2 to bandwidth limit the amplifier. This feedback capacitor creates a low pass filter that elimi-

nates possible high frequency oscillations. Care should be taken when calculating the -3dB frequency in that an incorrect combination of R<sub>3</sub> and C<sub>4</sub> will cause rolloff before 20kHz. A typical combination of feedback resistor and capacitor that will not produce audio band high frequency rolloff is R<sub>3</sub> = 20k $\Omega$  and C<sub>4</sub> = 25pf. These components result in a -3dB point of approximately 320 kHz.

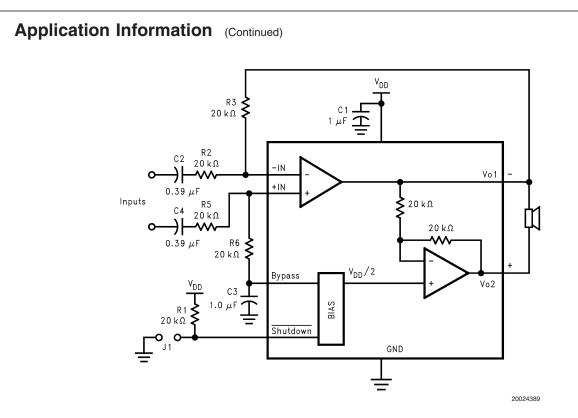


FIGURE 3. DIFFERENTIAL AMPLIFIER CONFIGURATION FOR LM4879

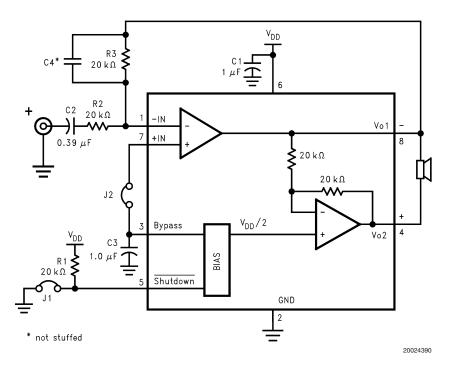
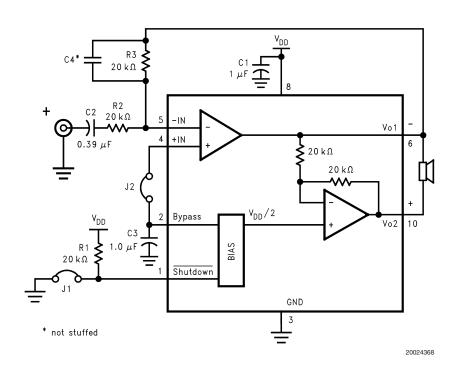


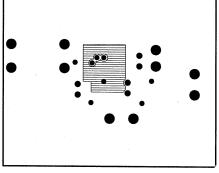
FIGURE 4. REFERENCE DESIGN BOARD and LAYOUT - micro SMD

## Application Information (Continued)



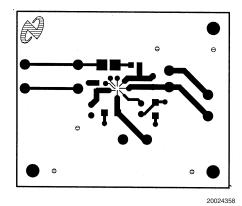
### FIGURE 5. REFERENCE DESIGN BOARD and PCB LAYOUT GUIDELINES - MSOP & SO Boards

## Application Information (Continued) LM4879 micro SMD BOARD ARTWORK Silk Screen NATIONAL SEMICONDUCTOR (BOOMER) micro SMD CZ R 2 **OINPUT** 🔵 GND 7 LIId. Э C I J2 GND VDD 20024357 **Bottom Layer** 551011282-001 rev B UL94V-0 20024359 Inner Layer V<sub>DD</sub>

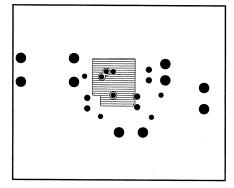


20024361

Top Layer



Inner Layer Ground

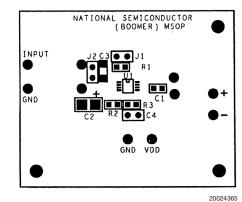


20024360

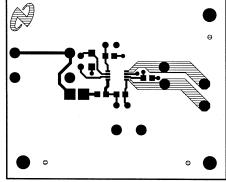
## Application Information (Continued)

### LM4879 MSOP DEMO BOARD ARTWORK

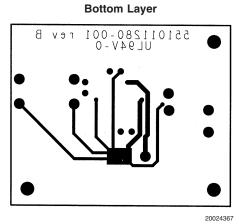
Silk Screen



**Top Layer** 



20024366



### TABLE 1. Mono LM4879 Reference Design Boards Bill of Material for all 3 Demo Boards

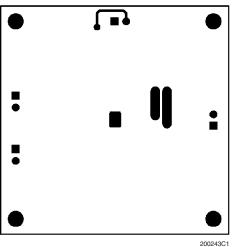
Item	Part Number	Part Description	Qty	Ref Designator
1	551011208-001	LM4879 Mono Reference Design Board	1	
10	482911183-001	LM4879 Audio AMP	1	U1
20	151911207-001	Tant Cap 1uF 16V 10	1	C1
21	151911207-002	Cer Cap 0.39uF 50V Z5U 20% 1210	1	C2
25	152911207-001	Tant Cap 1.0uF 16V 10	1	C3
30	472911207-001	Res 20K Ohm 1/10W 5	3	R1, R2, R3
35	210007039-002	Jumper Header Vertical Mount 2X1 0.100	2	J1, J2

Application Information (Continued) LM4879 LLP DEMO BOARD ARTWORK Silk Screen GND∎●∨DD JP2 JP1 IR3 IR3 SHUTDOWN OUT+ 2 C2 V\_OUT-GND ↓ ↓ ↓ ₽ 4 R2 C1 NSC LM4879SD Mono 1W BTL Audio Amplifier

200243C2

Top Layer 200243C0

**Bottom Layer** 



## Application Information (Continued)

### PCB LAYOUT GUIDELINES

This section provides practical guidelines for mixed signal PCB layout that involves various digital/analog power and ground traces. Designers should note that these are only "rule-of-thumb" recommendations and the actual results will depend heavily on the final layout.

#### **General Mixed Signal Layout Recommendation**

#### **Power and Ground Circuits**

For 2 layer mixed signal design, it is important to isolate the digital power and ground trace paths from the analog power and ground trace paths. Star trace routing techniques (bringing individual traces back to a central point rather than daisy chaining traces together in a serial manner) can have a major impact on low level signal performance. Star trace routing refers to using individual traces to feed power and ground to each circuit or even device. This technique will take require a greater amount of design time but will not increase the final price of the board. The only extra parts required may be some jumpers.

#### Single-Point Power / Ground Connections

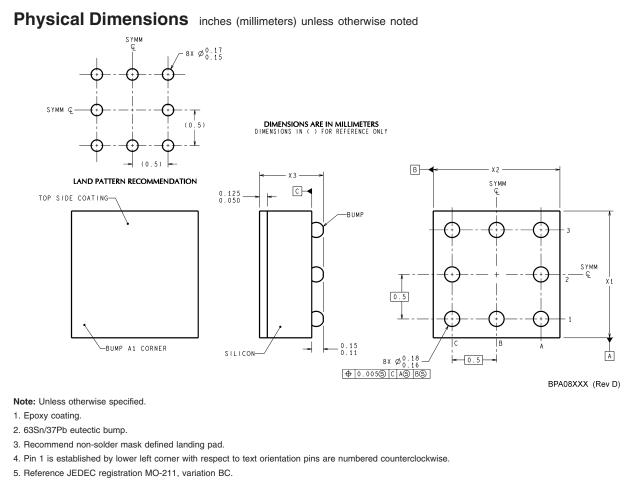
The analog power traces should be connected to the digital traces through a single point (link). A "Pi-filter" can be helpful in minimizing high frequency noise coupling between the analog and digital sections. It is further recommended to put digital and analog power traces over the corresponding digital and analog ground traces to minimize noise coupling.

#### **Placement of Digital and Analog Components**

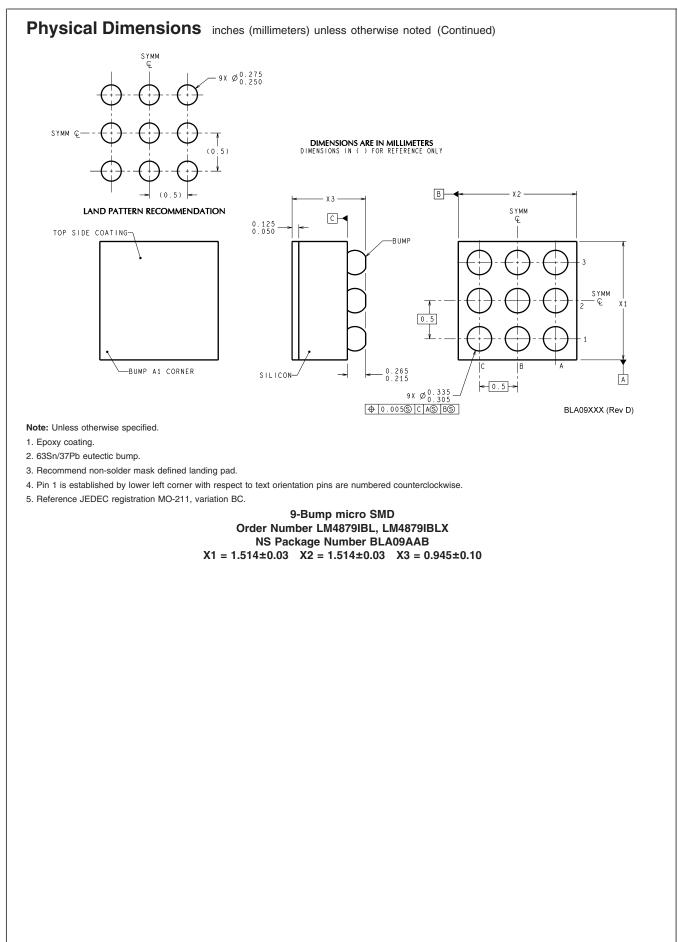
All digital components and high-speed digital signals traces should be located as far away as possible from analog components and circuit traces.

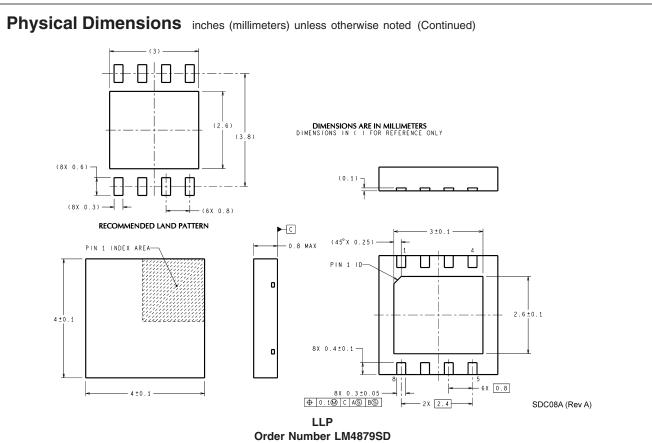
#### **Avoiding Typical Design / Layout Problems**

Avoid ground loops or running digital and analog traces parallel to each other (side-by-side) on the same PCB layer. When traces must cross over each other do it at 90 degrees. Running digital and analog traces at 90 degrees to each other from the top to the bottom side as much as possible will minimize capacitive noise coupling and cross talk.



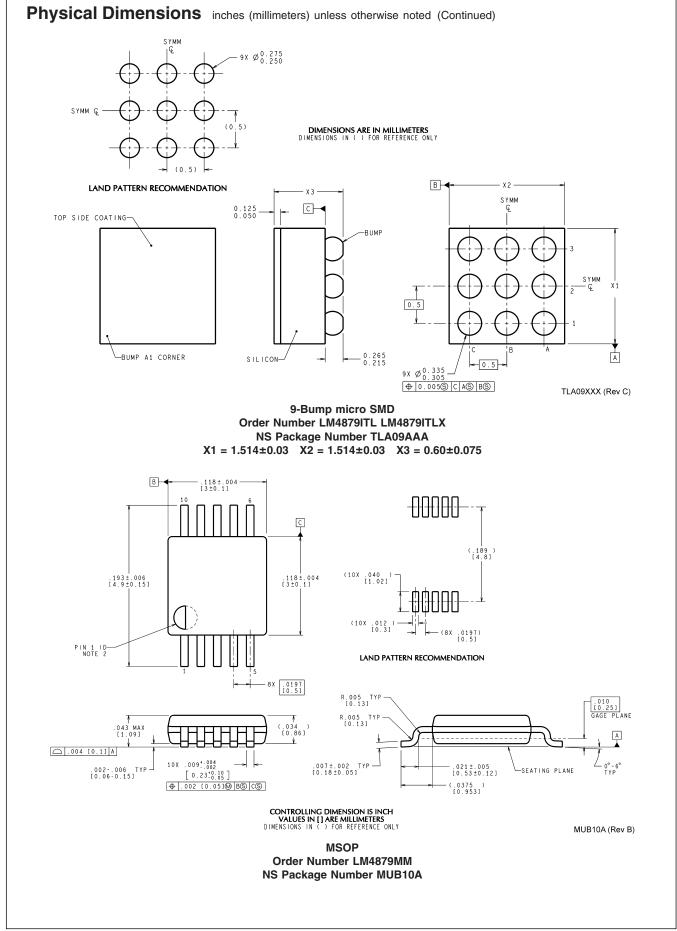
8-Bump micro SMD Order Number LM4879IBP, LM4879IBPX NS Package Number BPA08DDB X1 = 1.361±0.03 X2 = 1.361±0.03 X3 = 0.850±0.10





Order Number LM4879SD NS Package Number SDC08A





**Notes** 

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