

# FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B - SEPTEMBER 2003 - REVISED APRIL 2006

- Qualified for Automotive Applications
- Customer-Specific Configuration Control Can Be Supported Along With Major-Change Approval
- High Slew Rate . . . 10.5 V/ $\mu$ s Typ
- High-Gain Bandwidth . . . 5.1 MHz Typ
- Supply Voltage Range 2.5 V to 5.5 V

- Rail-to-Rail Output
- 360  $\mu$ V Input Offset Voltage
- Low Distortion Driving 600- $\Omega$  0.005% THD+N
- 1 mA Supply Current (Per Channel)
- 17 nV/ $\sqrt{\text{Hz}}$  Input Noise Voltage
- 2 pA Input Bias Current
- Characterized From  $T_A = -55^\circ\text{C}$  to  $125^\circ\text{C}$
- Available in MSOP and SOT-23 Packages
- Micropower Shutdown Mode . . .  $I_{DD} < 1 \mu\text{A}$

## description

The TLV277x CMOS operational amplifier family combines high slew rate and bandwidth, rail-to-rail output swing, high output drive, and excellent dc-precision. The device provides 10.5 V/ $\mu$ s of slew rate and 5.1 MHz of bandwidth while only consuming 1 mA of supply current per channel. This ac-performance is much higher than current competitive CMOS amplifiers. The rail-to-rail output swing and high output drive make these devices a good choice for driving the analog input or reference of analog-to-digital converters. These devices also have low distortion while driving a 600- $\Omega$  load for use in telecom systems.

These amplifiers have a 360- $\mu$ V input offset voltage, a 17 nV/ $\sqrt{\text{Hz}}$  input noise voltage, and a 2-pA input bias current for measurement, medical, and industrial applications. The TLV277x family is also specified across an extended temperature range ( $-40^\circ\text{C}$  to  $125^\circ\text{C}$ ), making it useful for automotive systems.

These devices operate from a 2.5-V to 5.5-V single supply voltage and are characterized at 2.7 V and 5 V. The single-supply operation and low power consumption make these devices a good solution for portable applications. The following table lists the packages available.

FAMILY PACKAGE TABLE

DEVICE	NUMBER OF CHANNELS	PACKAGE TYPES			SHUTDOWN	See the EVM Selection Guide (SLOU060)
		SOIC	TSSOP	SOT-23		
TLV2770	1	8	—	—	Yes	
TLV2771	1	8	—	5	—	
TLV2772	2	8	8	—	—	
TLV2773	2	14	—	—	Yes	
TLV2774	4	14	14	—	—	
TLV2775	4	16	16	—	Yes	

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

# TLV277x-Q1, TLV277xA-Q1

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### OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

#### A SELECTION OF SINGLE-SUPPLY OPERATIONAL AMPLIFIER PRODUCTS†

DEVICE	V <sub>DD</sub> (V)	BW (MHz)	SLEW RATE (V/μs)	I <sub>DD</sub> (per channel) (μA)	RAIL-TO-RAIL
TLV277X	2.5 – 6	5.1	10.5	1000	O
TLV247X	2.7 – 6	2.8	1.5	600	I/O
TLV245X	2.7 – 6	0.22	0.11	23	I/O
TLV246X	2.7 – 6	6.4	1.6	550	I/O

† All specifications measured at 5 V.

#### ORDERING INFORMATION

T <sub>A</sub>	V <sub>I0max</sub> AT 25°C (mV)	PACKAGE‡		ORDERABLE PART NUMBER	TOP-SIDE MARKING
–40°C to 125°C	2.5	SOIC (D)	Tape and reel	TLV2770QDRQ1\$	
	1.6	SOIC (D)	Tape and reel	TLV2770AQDRQ1\$	
–40°C to 125°C	2.5	SOT-23	Tape and reel	TLV2771QDBVRQ1	VBPQ
	2.5	SOIC (D)	Tape and reel	TLV2771QDRQ1\$	
	1.6	SOIC (D)	Tape and reel	TLV2771AQDRQ1\$	
–40°C to 125°C	2.5	SOIC (D)	Tape and reel	TLV2772QDRQ1	TLV2772QI
		TSSOP (PW)	Tape and reel	TLV2772QPWRQ1	TLV2772QI
	1.6	SOIC (D)	Tape and reel	TLV2772AQDRQ1	TLV2772AQ
		TSSOP (PW)	Tape and reel	TLV2772AQPWRQ1	TLV2772AQ
–40°C to 125°C	2.5	SOIC (D)	Tape and reel	TLV2773QDRQ1\$	
	1.6	SOIC (D)	Tape and reel	TLV2773AQDRQ1\$	
–40°C to 125°C	2.7	SOIC (D)	Tape and reel	TLV2774QDRQ1\$	
		TSSOP (PW)	Tape and reel	TLV2774QPWRQ1\$	
	2.1	SOIC (D)	Tape and reel	TLV2774AQDRQ1\$	
		TSSOP (PW)	Tape and reel	TLV2774AQPWRQ1\$	
–40°C to 125°C	2.7	SOIC (D)	Tape and reel	TLV2775QDRQ1\$	
		TSSOP (PW)	Tape and reel	TLV2775QPWRQ1\$	
	2.1	SOIC (D)	Tape and reel	TLV2775AQDRQ1\$	
		TSSOP (PW)	Tape and reel	TLV2775AQPWRQ1\$	

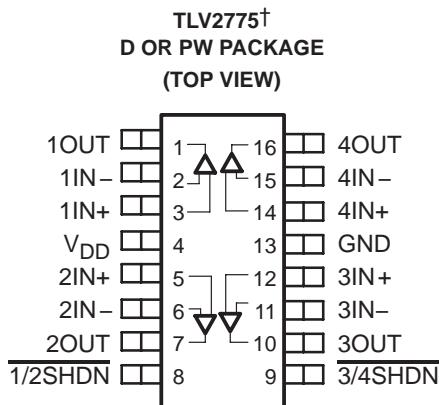
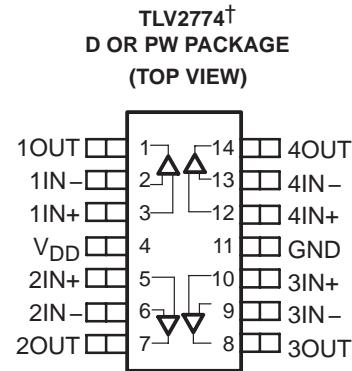
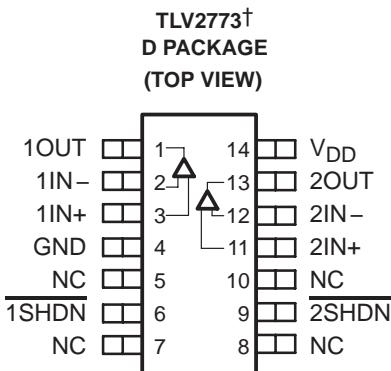
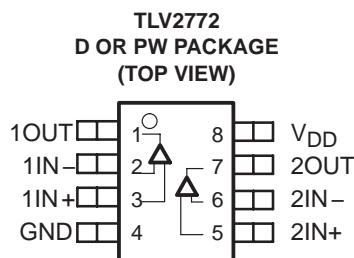
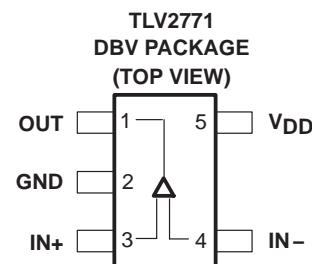
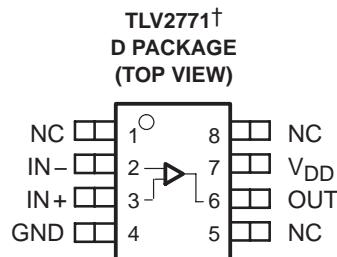
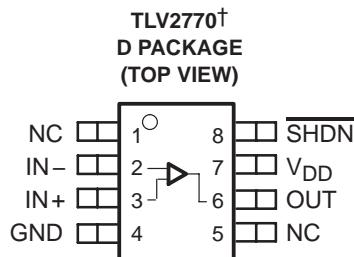
‡ Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at [www.ti.com/sc/package](http://www.ti.com/sc/package).

\$ Product Preview

**TLV277x-Q1, TLV277xA-Q1**  
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SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TLV277x PACKAGE PINOUTS**



NC – No internal connection

† This device is in the Product Preview stage of development. Contact your local Texas Instruments sales office for availability.

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### OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003 – REVISED APRIL 2006

#### absolute maximum ratings over operating free-air temperature range (unless otherwise noted)<sup>†</sup>

Supply voltage, $V_{DD}$ (see Note 1) .....	7 V
Differential input voltage, $V_{ID}$ (see Note 2) .....	$\pm V_{DD}$
Input voltage range, $V_I$ (any input, see Note 1) .....	–0.3 V to $V_{DD}$
Input current, $I_I$ (any input) .....	±4 mA
Output current, $I_O$ .....	±50 mA
Total current into $V_{DD+}$ .....	±50 mA
Total current out of GND .....	±50 mA
Duration of short-circuit current (at or below) 25°C (see Note 3) .....	unlimited
Continuous total power dissipation .....	See Dissipation Rating Table
Operating free-air temperature range, $T_A$ : Q suffix .....	–40°C to 125°C
Storage temperature range, $T_{Stg}$ .....	–65°C to 150°C
Lead temperature 1.6 mm (1/16 inch) from case for 10 seconds .....	260°C

<sup>†</sup> Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTES: 1. All voltage values, except differential voltages, are with respect to GND.

2. Differential voltages are at the noninverting input with respect to the inverting input. Excessive current flows when input is brought below GND – 0.3 V.
3. The output may be shorted to either supply. Temperature and/or supply voltages must be limited to ensure that the maximum dissipation rating is not exceeded.

ESD RATING TABLE

ESD rating (4)	Human Body Model	2 (H1C)	kV
	Charged-Device Model	1 (C5)	
	Machine Model	150 (M2)	

NOTE 4: ESD protection level per AEC Q100 Classification TLV2771QDBVRQ1

DISSIPATION RATING TABLE

PACKAGE	$T_A \leq 25^\circ\text{C}$ POWER RATING	DERATING FACTOR ABOVE $T_A = 25^\circ\text{C}$	$T_A = 70^\circ\text{C}$ POWER RATING	$T_A = 85^\circ\text{C}$ POWER RATING	$T_A = 125^\circ\text{C}$ POWER RATING
D	725 mW	5.8 mW/°C	464 mW	377 mW	145 mW
DBV	437 mW	3.5 mW/°C	280 mW	227 mW	87 mW
PW	700 mW	5.6 mW/°C	448 mW	364 mW	140 mW

#### recommended operating conditions

	Q SUFFIX		UNIT
	MIN	MAX	
Supply voltage, $V_{DD}$	2.5	6	V
Input voltage range, $V_I$	GND	$V_{DD+} - 1.3$	V
Common-mode input voltage, $V_{IC}$	GND	$V_{DD+} - 1.3$	V
Operating free-air temperature, $T_A$	–40	125	°C

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**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**electrical characteristics at specified free-air temperature,  $V_{DD} = 2.7$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	TA <sup>†</sup>	TLV2771-Q1			UNIT
			MIN	TYP	MAX	
V <sub>IO</sub>	Input offset voltage $V_{IC} = 0, V_O = 0, R_S = 50 \Omega$ $V_{DD} = \pm 1.35$ V, No load	25°C	0.48	2.5	2.5	mV
		Full range	0.53	2.7	2.7	
$\alpha V_{IO}$	Temperature coefficient of input offset voltage	25°C to 125°C	2	2	2	$\mu\text{V}/^\circ\text{C}$
		25°C	1	60	60	
I <sub>IO</sub>	Input offset current $V_{IC} = 0, V_O = 0, R_S = 50 \Omega$	Full range	2	125	125	pA
		25°C	2	60	60	
I <sub>IB</sub>	Input bias current	Full range	6	350	350	pA
		25°C	2	60	60	
V <sub>OH</sub>	High-level output voltage $I_{OH} = -0.675$ mA	25°C	2.6	2.6	2.6	V
		Full range	2.5	2.5	2.5	
		25°C	2.4	2.4	2.4	
		Full range	2.1	2.1	2.1	
V <sub>OL</sub>	Low-level output voltage $V_{IC} = 1.35$ V, $I_{OL} = 0.675$ mA	25°C	0.1	0.1	0.1	V
		Full range	0.2	0.2	0.2	
		25°C	0.21	0.21	0.21	
		Full range	0.6	0.6	0.6	
AVD	Large-signal differential voltage amplification $V_{IC} = 1.35$ V, $R_L = 10 \text{ k}\Omega$ <sup>‡</sup> , $V_O = 0.6$ V to 2.1 V	25°C	20	380	380	V/mV
		Full range	13	13	13	
r <sub>i(d)</sub>	Differential input resistance	25°C	10 <sup>12</sup>	10 <sup>12</sup>	10 <sup>12</sup>	Ω
c <sub>i(c)</sub>	Common-mode input capacitance	25°C	8	8	8	pF
z <sub>o</sub>	Closed-loop output impedance	f = 100 kHz, A <sub>V</sub> = 10	25°C	25	25	Ω
CMRR	Common-mode rejection ratio $V_{IC} = 0$ to 1.5 V, $V_O = V_{DD}/2$ , $R_S = 50 \Omega$	25°C	60	84	84	dB
		Full range	60	82	82	
k <sub>SVR</sub>	Supply voltage rejection ratio ( $\Delta V_{DD} / \Delta V_{IO}$ ) $V_{DD} = 2.7$ V to 5 V, $V_{IC} = V_{DD}/2$ , No load	25°C	70	89	89	dB
		Full range	70	84	84	
I <sub>DD</sub>	Supply current (per channel) $V_O = V_{DD}/2$ , No load	25°C	1	2	2	mA
		Full range	2	2	2	

<sup>†</sup> Full range is –40°C to 125°C for Q level part.

<sup>‡</sup> Referenced to 1.35 V

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**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B—SEPTEMBER 2003 – REVISED APRIL 2006

operating characteristics at specified free-air temperature,  $V_{DD} = 2.7$  V (unless otherwise noted)

PARAMETER	TEST CONDITIONS	TA <sup>†</sup>	TLV2771-Q1			UNIT	
			MIN	TYP	MAX		
SR	Slew rate at unity gain $V_O(PP) = 0.8$ V, $C_L = 100$ pF, $R_L = 10$ k $\Omega$	25°C	5	9		V/ $\mu$ s	
		Full range	4.7	6			
V <sub>n</sub>	Equivalent input noise voltage $f = 1$ kHz	25°C	21			nV/ $\sqrt{\text{Hz}}$	
		25°C	17				
V <sub>N(PP)</sub>	Peak-to-peak equivalent input noise voltage $f = 0.1$ Hz to 1 Hz	25°C	0.33			$\mu$ V	
		25°C	0.86				
I <sub>n</sub>	Equivalent input noise current $f = 100$ Hz	25°C	0.6			fA/ $\sqrt{\text{Hz}}$	
THD + N	Total harmonic distortion plus noise $R_L = 600$ $\Omega$ , $f = 1$ kHz	A <sub>V</sub> = 1 A <sub>V</sub> = 10 A <sub>V</sub> = 100	25°C	0.0085%			
				0.025%			
				0.12%			
Gain-bandwidth product		$f = 10$ kHz, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	25°C	4.8		MHz	
t <sub>s</sub>	Settling time $A_V = -1$ , Step = 0.85 V to 1.85 V, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	0.1%	25°C	0.186		$\mu$ s	
		0.01%	25°C	3.92			
$\phi_m$	Phase margin at unity gain	$R_L = 600$ $\Omega$ , $C_L = 100$ pF	25°C	46°			
	Gain margin		25°C	12		dB	

<sup>†</sup>Full range is –40°C to 125°C.

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**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**electrical characteristics at specified free-air temperature,  $V_{DD} = 5$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	TA <sup>†</sup>	TLV2771-Q1			UNIT
			MIN	TYP	MAX	
V <sub>IO</sub> Input offset voltage	$V_{IC} = 0$ , No load $V_O = 0$ , $R_S = 50 \Omega$ , $V_{DD} = \pm 2.5$ V	25°C	0.5	2.5		mV
		Full range	0.6	2.7		
$\alpha V_{IO}$ Temperature coefficient of input offset voltage		25°C to 125°C		2		$\mu\text{V}/\text{C}$
		25°C	1	60		
I <sub>IO</sub> Input offset current	$V_{IC} = 0$ , $V_O = 0$ , $R_S = 50 \Omega$ , $V_{DD} = \pm 2.5$ V	Full range	2	125		pA
		25°C	2	60		
I <sub>IB</sub> Input bias current		Full range	6	350		pA
V <sub>OH</sub> High-level output voltage	$I_{OH} = -1.3$ mA	25°C	4.9			V
		Full range	4.8			
	$I_{OH} = -4.2$ mA	25°C	4.7			
		Full range	4.4			
V <sub>OL</sub> Low-level output voltage	$V_{IC} = 2.5$ V, $I_{OL} = 1.3$ mA	25°C	0.1			V
		Full range	0.2			
	$V_{IC} = 2.5$ V, $I_{OL} = 4.2$ mA	25°C	0.21			
		Full range	0.6			
AVD Large-signal differential voltage amplification	$V_{IC} = 2.5$ V, $R_L = 10 \text{ k}\Omega^{\ddagger}$ , $V_O = 1$ V to 4 V	25°C	20	450		V/mV
		Full range	13			
r <sub>i(d)</sub> Differential input resistance		25°C	10 <sup>12</sup>			Ω
c <sub>i(c)</sub> Common-mode input capacitance	f = 10 kHz	25°C	8			pF
z <sub>o</sub> Closed-loop output impedance	f = 100 kHz, A <sub>v</sub> = 10	25°C	20			Ω
CMRR Common-mode rejection ratio	$V_{IC} = 0$ to 3.7 V, $V_O = V_{DD}/2$ , $R_S = 50 \Omega$	25°C	60	96		dB
		Full range	60	93		
k <sub>SVR</sub> Supply voltage rejection ratio ( $\Delta V_{DD} / \Delta V_{IO}$ )	$V_{DD} = 2.7$ V to 5 V, $V_{IC} = V_{DD}/2$ , No load	25°C	70	89		dB
		Full range	70	84		
I <sub>DD</sub> Supply current (per channel)	$V_O = V_{DD}/2$ , No load	25°C	1	2		mA
		Full range			2	

<sup>†</sup> Full range is –40°C to 125°C for Q level part.

<sup>‡</sup> Referenced to 2.5 V

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

**operating characteristics at specified free-air temperature,  $V_{DD} = 5$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	$T_A^\dagger$	TLV2771-Q1			UNIT
			MIN	TYP	MAX	
SR	Slew rate at unity gain $V_{O(PP)} = 1.5$ V, $C_L = 100$ pF, $R_L = 10$ k $\Omega$	25°C	5	10.5		V/ $\mu$ s
		Full range	4.7	6		
$V_n$	Equivalent input noise voltage $f = 1$ kHz	25°C		17		nV/ $\sqrt{\text{Hz}}$
		25°C		12		
$V_{N(PP)}$	Peak-to-peak equivalent input noise voltage $f = 0.1$ Hz to 1 Hz	25°C		0.33		$\mu$ V
		25°C		0.86		
$I_n$	Equivalent input noise current $f = 100$ Hz	25°C		0.6		fA/ $\sqrt{\text{Hz}}$
THD + N	Total harmonic distortion plus noise $R_L = 600$ $\Omega$ , $f = 1$ kHz	$A_V = 1$			0.005%	
		$A_V = 10$			0.016%	
		$A_V = 100$			0.095%	
Gain-bandwidth product		$f = 10$ kHz, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	25°C		5.1	MHz
$t_s$	Settling time $A_V = -1$ , Step = 1.5 V to 3.5 V, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	0.1%	25°C		0.134	$\mu$ s
		0.01%	25°C		1.97	
$\phi_m$	Phase margin at unity gain $R_L = 600$ $\Omega$ , $C_L = 100$ pF		25°C		46°	
			25°C		12	dB

<sup>†</sup>Full range is  $-40$ °C to  $125$ °C.

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**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**electrical characteristics at specified free-air temperature,  $V_{DD} = 2.7$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	$T_A \dagger$	TLV2772-Q1			TLV2772A-Q1			UNIT
			MIN	TYP	MAX	MIN	TYP	MAX	
$V_{IO}$	$V_{DD} = \pm 1.35$ V, $V_{IC} = 0$ , $R_S = 50 \Omega$	25°C	0.44	2.5		0.44	1.6		mV
$\alpha V_{IO}$		Full range	0.47	2.7		0.47	1.9		
$I_{IO}$		25°C to 125°C		2			2		$\mu\text{V}/^\circ\text{C}$
$I_{IB}$		25°C	1	60		1	60		pA
$I_{IB}$		Full range	2	125		2	125		
$V_{ICR}$		25°C	2	60		2	60		pA
$V_{ICR}$	$CMRR > 60$ dB, $R_S = 50 \Omega$	Full range	6	350		6	350		
$V_{OH}$		25°C	0 to 1.4	-0.3 to 1.7		0 to 1.4	-0.3 to 1.7		V
$V_{OH}$		Full range	0 to 1.4	-0.3 to 1.7		0 to 1.4	-0.3 to 1.7		
$V_{OL}$		25°C	2.6			2.6			
$V_{OL}$	$V_{IC} = 1.35$ V, $I_{OL} = 0.675$ mA	Full range	2.45			2.45			V
$V_{OL}$		25°C	2.4			2.4			
$V_{OL}$		Full range	2.1			2.1			
$A_{VD}$		25°C	0.1			0.1			V/mV
$r_{i(d)}$	$V_{IC} = 1.35$ V, $V_O = 0.6$ V to 2.1 V	Full range	0.2			0.2			
$C_{i(c)}$		25°C	0.21			0.21			
$Z_O$	$V_{IC} = 1.35$ V, $I_{OL} = 2.2$ mA	Full range	0.6			0.6			
$CMRR$		25°C	20	380		20	380		dB
$k_{SVR}$	$V_{DD} = 2.7$ V to 5 V, $V_{IC} = V_{DD}/2$ , No load	Full range	13			13			
$I_{DD}$		25°C	10 <sup>12</sup>			10 <sup>12</sup>			$\Omega$
$C_{i(c)}$		25°C	8			8			pF
$Z_O$		25°C	25			25			$\Omega$
$CMRR$	$V_{IC} = V_{ICR}$ (min), $V_O = 1.5$ V, $R_S = 50 \Omega$	25°C	60	84		60	84		dB
$k_{SVR}$		Full range	60	82		60	82		
$I_{DD}$	$V_O = 1.5$ V, No load	25°C	70	89		70	89		dB
$I_{DD}$		Full range	70	84		70	84		

<sup>†</sup> Full range is  $-40^\circ\text{C}$  to  $125^\circ\text{C}$  for Q level part.

<sup>‡</sup> Referenced to 1.35 V

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

operating characteristics at specified free-air temperature,  $V_{DD} = 2.7$  V (unless otherwise noted)

PARAMETER	TEST CONDITIONS	$T_A^\dagger$	TLV2772-Q1			TLV2772A-Q1			UNIT
			MIN	TYP	MAX	MIN	TYP	MAX	
SR	Slew rate at unity gain $V_{O(PP)} = 0.8$ V, $C_L = 100$ pF, $R_L = 10$ k $\Omega$	25°C	5	9		5	9		V/ $\mu$ s
		Full range	4.7	6		4.7	6		
V <sub>n</sub>	Equivalent input noise voltage $f = 1$ kHz	25°C	21	21		21	21		nV/ $\sqrt{\text{Hz}}$
		25°C	17	17		17	17		
V <sub>N(PP)</sub>	Peak-to-peak equivalent input noise voltage $f = 0.1$ Hz to 1 Hz	25°C	0.33	0.33		0.33	0.33		$\mu$ V
		25°C	0.86	0.86		0.86	0.86		
I <sub>n</sub>	Equivalent input noise current $f = 100$ Hz	25°C	0.6	0.6		0.6	0.6		fA/ $\sqrt{\text{Hz}}$
THD + N	Total harmonic distortion plus noise $R_L = 600$ $\Omega$ , $f = 1$ kHz	$A_V = 1$ $A_V = 10$ $A_V = 100$	25°C	0.0085%	0.0085%	0.025%	0.025%	0.12%	
			25°C	0.025%	0.025%				
			25°C	0.12%	0.12%				
	Gain-bandwidth product $f = 10$ kHz, $C_L = 100$ pF	$R_L = 600$ $\Omega$ ,	25°C	4.8	4.8	4.8	4.8	4.8	MHz
t <sub>s</sub>	Settling time $A_V = -1$ , Step = 0.85 V to 1.85 V, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	0.1% 0.01%	25°C	0.186	0.186	0.186	0.186	0.186	$\mu$ s
			25°C	3.92	3.92	3.92	3.92	3.92	
$\phi_m$	Phase margin at unity gain $R_L = 600$ $\Omega$ , $C_L = 100$ pF		25°C	46°	46°	46°	46°	46°	
			25°C	12	12	12	12	12	
									dB

† Full range is  $-40^\circ\text{C}$  to  $125^\circ\text{C}$  for Q level part.

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**electrical characteristics at specified free-air temperature,  $V_{DD} = 5$  V (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	$T_A \dagger$	TLV2772-Q1			TLV2772A-Q1			UNIT	
			MIN	TYP	MAX	MIN	TYP	MAX		
$V_{IO}$ Input offset voltage	$V_{DD} = \pm 2.5$ V, $V_O = 0$ , $V_{IC} = 0$ , $R_S = 50 \Omega$	25°C	0.36	2.5		0.36	1.6		mV	
		Full range	0.4	2.7		0.4	1.9			
		25°C to 125°C		2			2		µV/°C	
		25°C	1	60		1	60		pA	
		Full range	2	125		2	125			
		25°C	2	60		2	60		pA	
$I_{IB}$ Input bias current		Full range	6	350		6	350			
		25°C	0	-0.3	to	0	-0.3	to	V	
			3.7	3.8		3.7	3.8			
		Full range	0	-0.3	to	0	-0.3	to	V	
			3.7	3.8		3.7	3.8			
		25°C	4.9			4.9			V	
$V_{OH}$ High-level output voltage	$I_{OH} = -1.3$ mA	Full range	4.8			4.8			V	
		25°C	4.7			4.7				
	$I_{OH} = -4.2$ mA	Full range	4.4			4.4			V	
		25°C	0.1			0.1				
$V_{OL}$ Low-level output voltage	$V_{IC} = 2.5$ V, $I_{OL} = 1.3$ mA	Full range	0.2			0.2			V	
		25°C	0.21			0.21				
	$V_{IC} = 2.5$ V, $I_{OL} = 4.2$ mA	Full range	0.6			0.6			V	
		25°C	20	450		20	450			
$A_{VD}$ Large-signal differential voltage amplification	$V_{IC} = 2.5$ V, $V_O = 1$ V to 4 V	Full range	13			13			V/mV	
		25°C	10 <sup>12</sup>			10 <sup>12</sup>				
$r_{i(d)}$ Differential input resistance		25°C							Ω	
$C_{i(c)}$ Common-mode input capacitance	$f = 10$ kHz,	25°C	8			8			pF	
$z_O$ Closed-loop output impedance	$f = 100$ kHz, $A_V = 10$	25°C	20			20			Ω	
CMRR Common-mode rejection ratio	$V_{IC} = V_{ICR}$ (min), $V_O = 3.7$ V, $R_S = 50 \Omega$	25°C	60	96		60	96		dB	
		Full range	60	93		60	93			
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{DD} / \Delta V_{IO}$ )	$V_{DD} = 2.7$ V to 5 V, No load	25°C	70	89		70	89		dB	
		Full range	70	84		70	84			
$I_{DD}$ Supply current (per channel)	$V_O = 1.5$ V, No load	25°C	1	2		1	2		mA	
		Full range		2			2			

† Full range is -40°C to 125°C for Q level part.

‡ Referenced to 2.5 V

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

operating characteristics at specified free-air temperature,  $V_{DD} = 5$  V (unless otherwise noted)

PARAMETER	TEST CONDITIONS	$T_A^\dagger$	TLV2772-Q1			TLV2772A-Q1			UNIT
			MIN	TYP	MAX	MIN	TYP	MAX	
SR	Slew rate at unity gain $V_{O(PP)} = 1.5$ V, $C_L = 100$ pF, $R_L = 10$ k $\Omega$	25°C	5	10.5		5	10.5		V/ $\mu$ s
		Full range	4.7	6		4.7	6		
V <sub>n</sub>	Equivalent input noise voltage $f = 1$ kHz	25°C	17	17		17	17		nV/ $\sqrt{\text{Hz}}$
		25°C	12	12		12	12		
V <sub>N(PP)</sub>	Peak-to-peak equivalent input noise voltage $f = 0.1$ Hz to 1 Hz	25°C	0.33	0.33		0.33	0.33		$\mu$ V
		25°C	0.86	0.86		0.86	0.86		
I <sub>n</sub>	Equivalent input noise current $f = 100$ Hz	25°C	0.6	0.6		0.6	0.6		fA/ $\sqrt{\text{Hz}}$
THD + N	Total harmonic distortion plus noise $R_L = 600$ $\Omega$ , $f = 1$ kHz	$A_V = 1$ $A_V = 10$ $A_V = 100$	25°C	0.005%	0.005%	25°C	0.016%	0.016%	
			25°C	0.095%	0.095%	25°C	0.095%	0.095%	
			25°C	5.1	5.1	25°C	5.1	5.1	MHz
t <sub>s</sub>	Settling time $A_V = -1$ , Step = 1.5 V to 3.5 V, $R_L = 600$ $\Omega$ , $C_L = 100$ pF	0.1%	25°C	0.134	0.134	25°C	1.97	1.97	$\mu$ s
		0.01%	25°C	1.97	1.97	25°C	1.97	1.97	
$\phi_m$	Phase margin at unity gain $R_L = 600$ $\Omega$ , $C_L = 100$ pF	25°C	46°	46°		25°C	12	12	dB
		25°C	12	12		25°C	12	12	

† Full range is  $-40^\circ\text{C}$  to  $125^\circ\text{C}$  for Q level part.

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

**Table of Graphs**

			<b>FIGURE</b>
$V_{IO}$	Input offset voltage	Distribution vs Common-mode input voltage Distribution	1, 2 3, 4 5, 6
$I_{IB}/I_{IO}$	Input bias and input offset currents	vs Free-air temperature	7
$V_{OH}$	High-level output voltage	vs High-level output current	8, 9
$V_{OL}$	Low-level output voltage	vs Low-level output current	10, 11
$V_{O(PP)}$	Maximum peak-to-peak output voltage	vs Frequency	12, 13
$I_{OS}$	Short-circuit output current	vs Supply voltage vs Free-air temperature	14 15
$V_O$	Output voltage	vs Differential input voltage	16
AVD	Large-signal differential voltage amplification and phase margin	vs Frequency	17, 18
AVD	Differential voltage amplification	vs Load resistance vs Free-air temperature	19 20, 21
$z_o$	Output impedance	vs Frequency	22, 23
CMRR	Common-mode rejection ratio	vs Frequency vs Free-air temperature	24 25
kSVR	Supply-voltage rejection ratio	vs Frequency	26, 27
IDD	Supply current (per channel)	vs Supply voltage	28
SR	Slew rate	vs Load capacitance vs Free-air temperature	29 30
$V_O$	Voltage-follower small-signal pulse response		31, 32
$V_O$	Voltage-follower large-signal pulse response		33, 34
$V_O$	Inverting small-signal pulse response		35, 36
$V_O$	Inverting large-signal pulse response		37, 38
$V_n$	Equivalent input noise voltage	vs Frequency	39, 40
	Noise voltage (referred to input)	Over a 10-second period	41
THD + N	Total harmonic distortion plus noise	vs Frequency	42, 43
	Gain-bandwidth product	vs Supply voltage	44
B <sub>1</sub>	Unity-gain bandwidth	vs Load capacitance	45
$\phi_m$	Phase margin	vs Load capacitance	46
	Gain margin	vs Load capacitance	47
	Amplifier with shutdown pulse turnon/off characteristics		48–50
	Supply current with shutdown pulse turnon/off characteristics		51–53
	Shutdown supply current	vs Free-air temperature	54
	Shutdown forward/reverse isolation	vs Frequency	55, 56

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

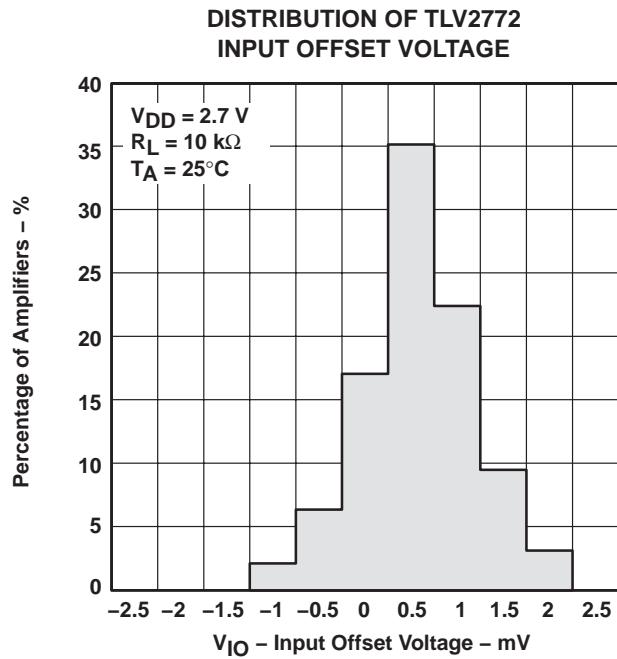


Figure 1

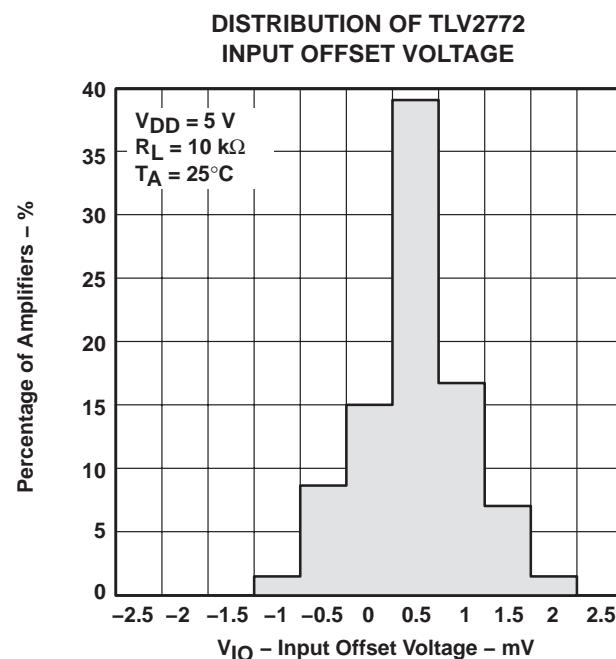


Figure 2

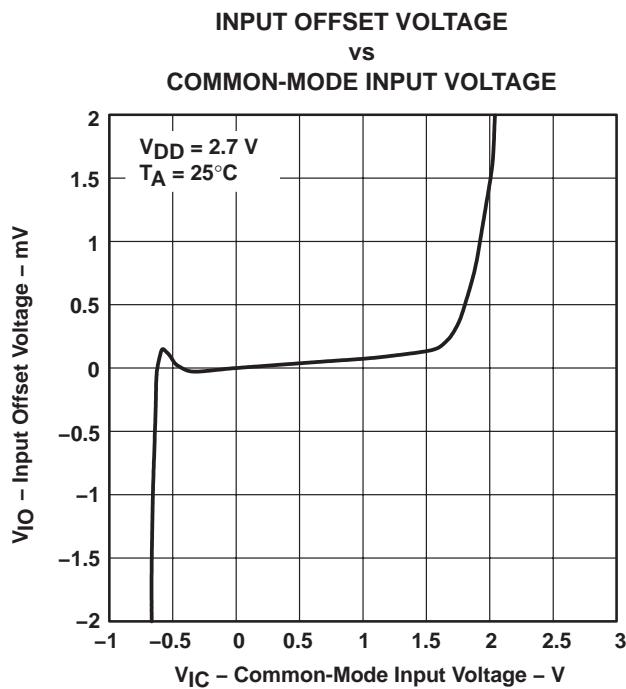


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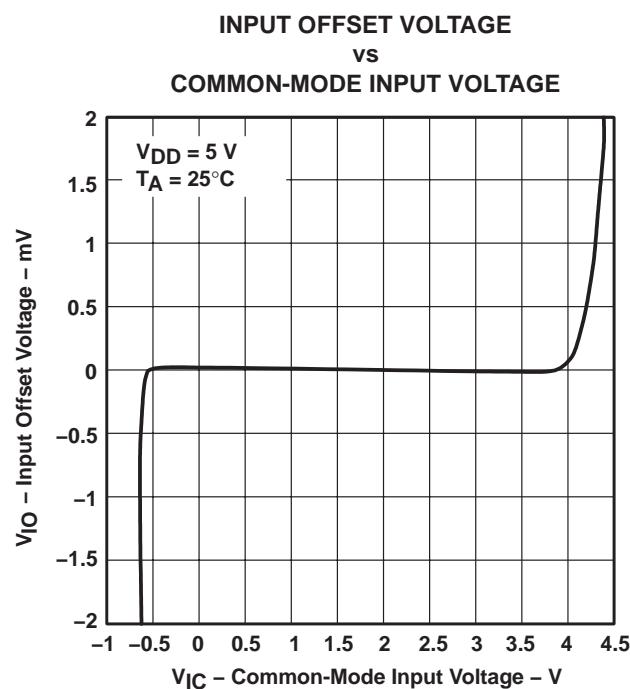
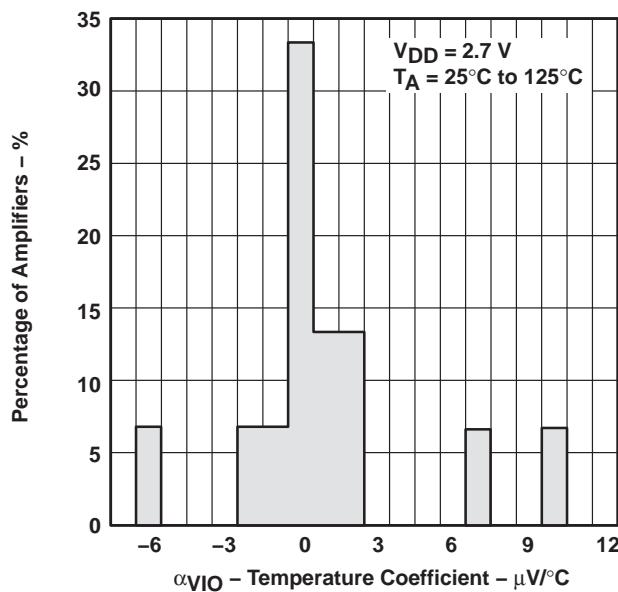


Figure 4

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

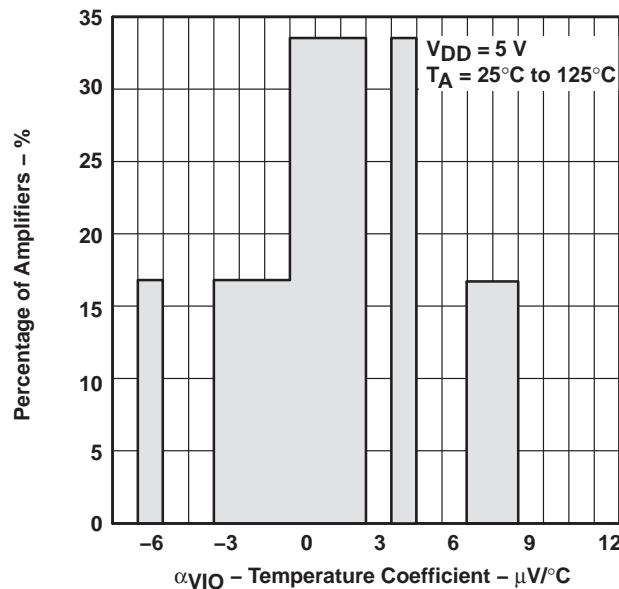
**TYPICAL CHARACTERISTICS**

**DISTRIBUTION OF TLV2772  
INPUT OFFSET VOLTAGE**



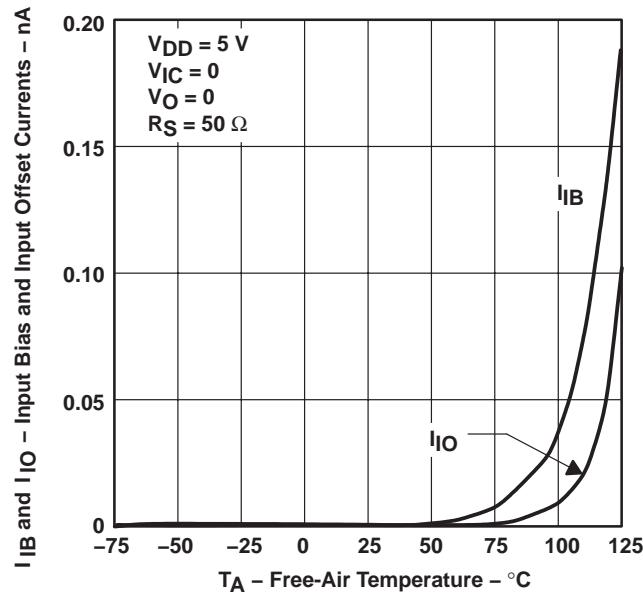
**Figure 5**

**DISTRIBUTION OF TLV2772  
INPUT OFFSET VOLTAGE**



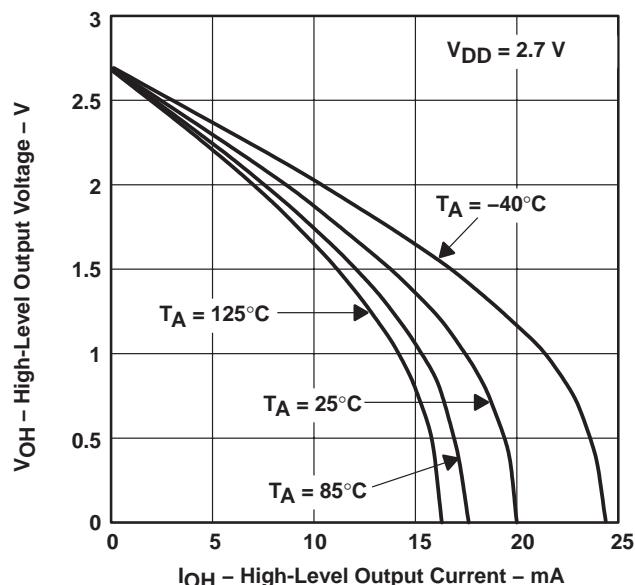
**Figure 6**

**INPUT BIAS AND OFFSET CURRENT  
vs  
FREE-AIR TEMPERATURE**



**Figure 7**

**HIGH-LEVEL OUTPUT VOLTAGE  
vs  
HIGH-LEVEL OUTPUT CURRENT**



**Figure 8**

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

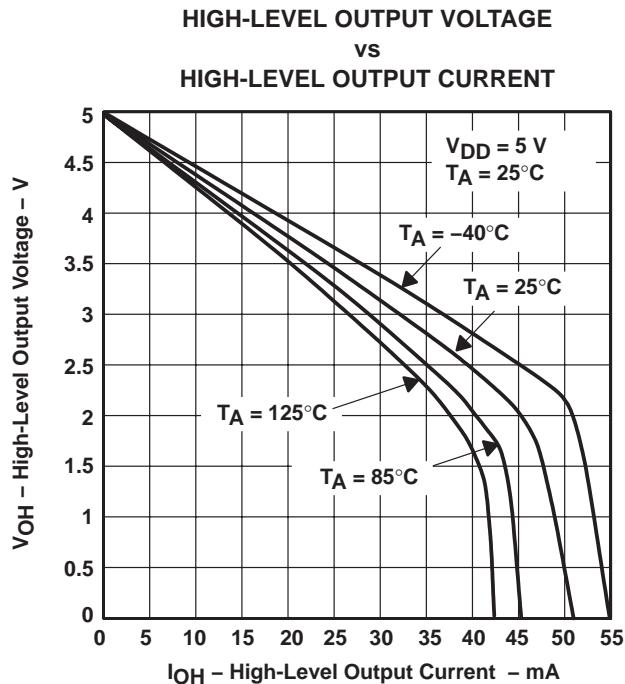


Figure 9

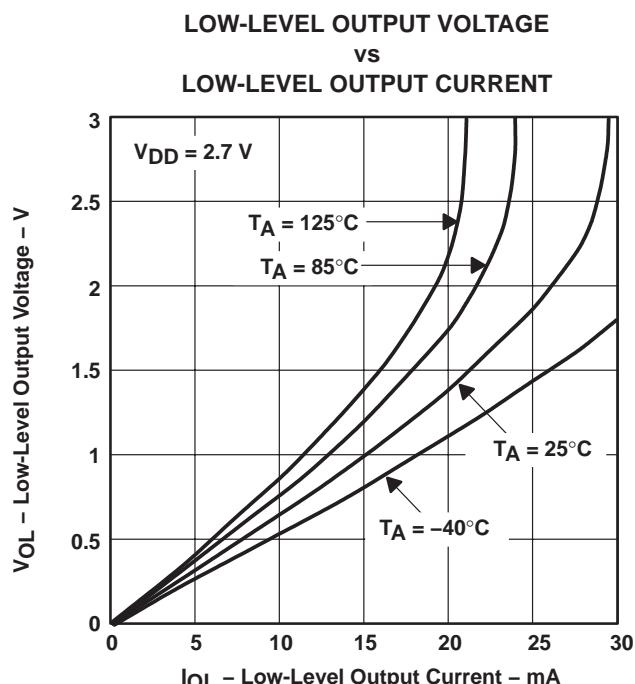


Figure 10

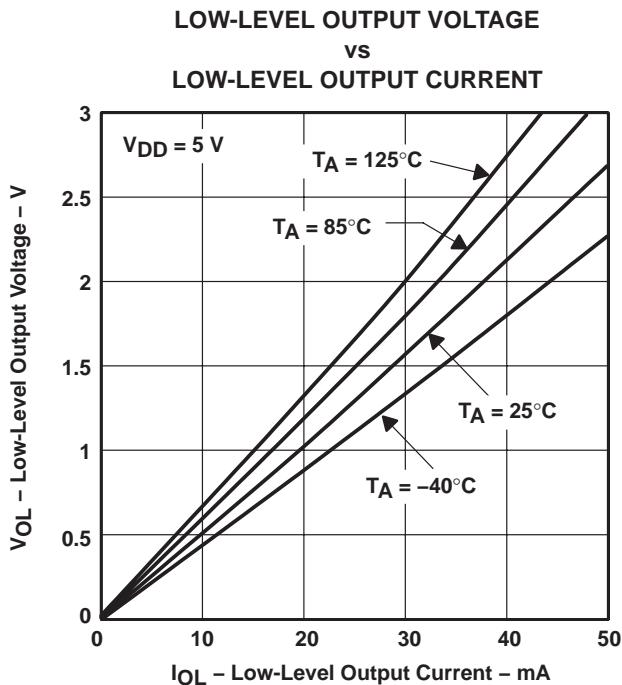


Figure 11

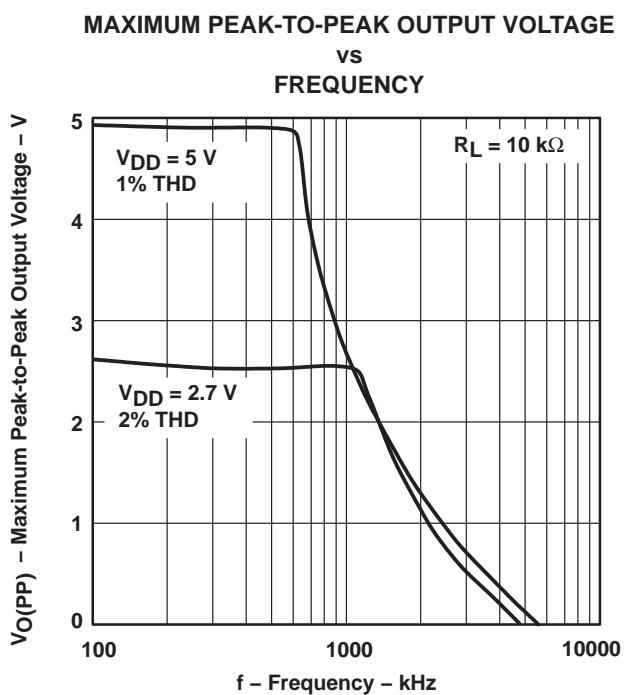


Figure 12

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

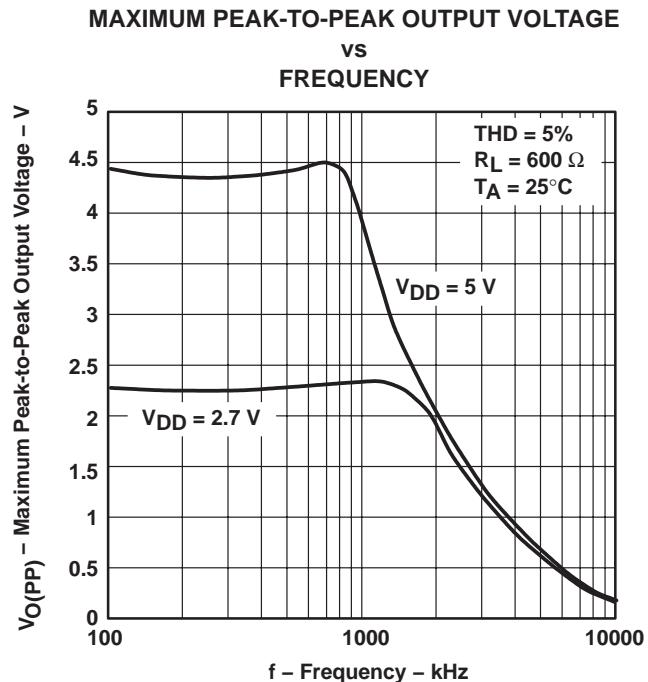


Figure 13

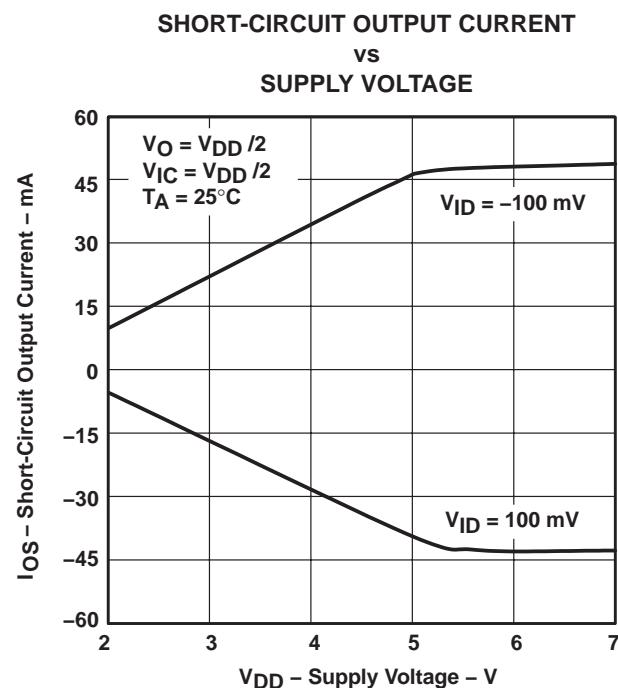


Figure 14

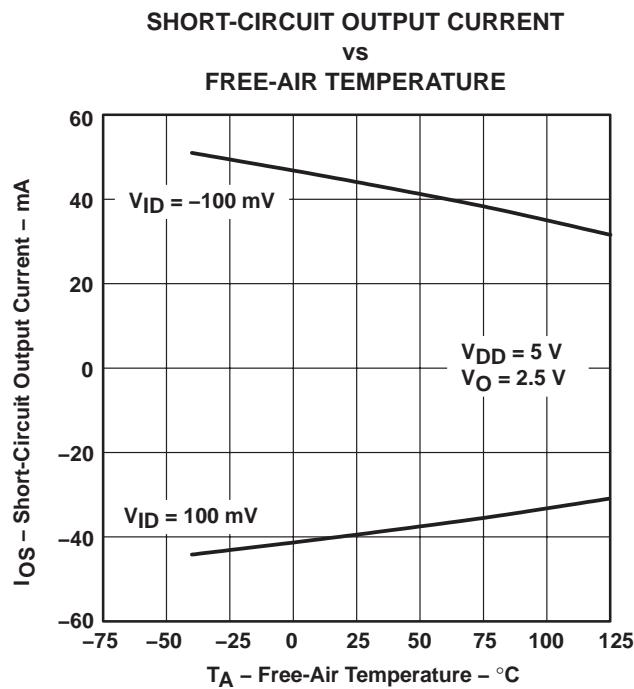


Figure 15

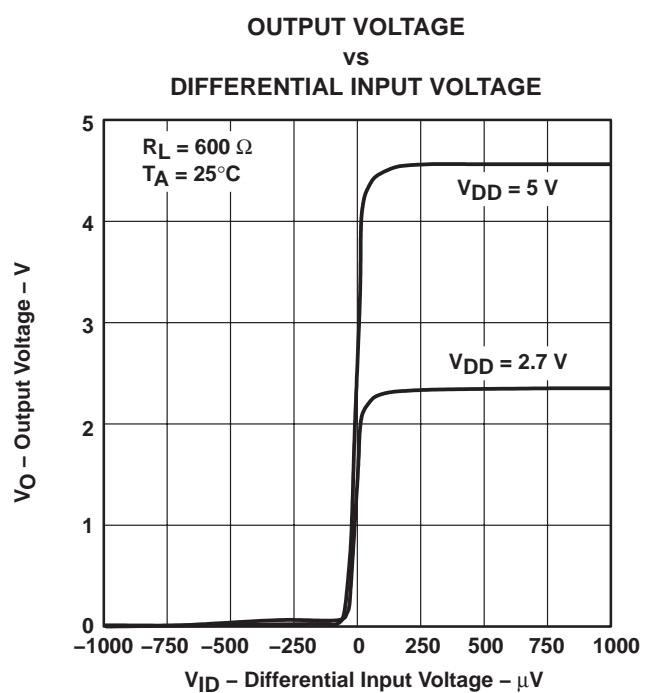


Figure 16

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

### TYPICAL CHARACTERISTICS

LARGE-SIGNAL DIFFERENTIAL VOLTAGE AMPLIFICATION  
AND PHASE MARGIN  
vs  
FREQUENCY

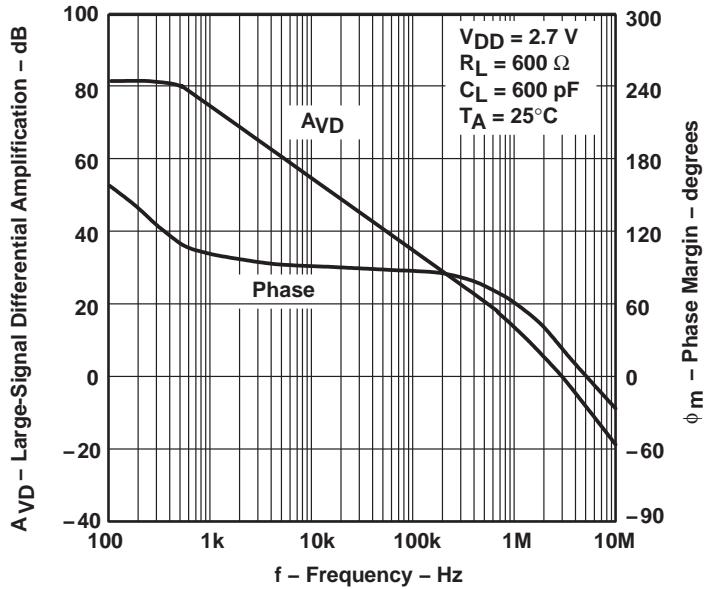


Figure 17

LARGE-SIGNAL DIFFERENTIAL VOLTAGE AMPLIFICATION  
AND PHASE MARGIN  
vs  
FREQUENCY

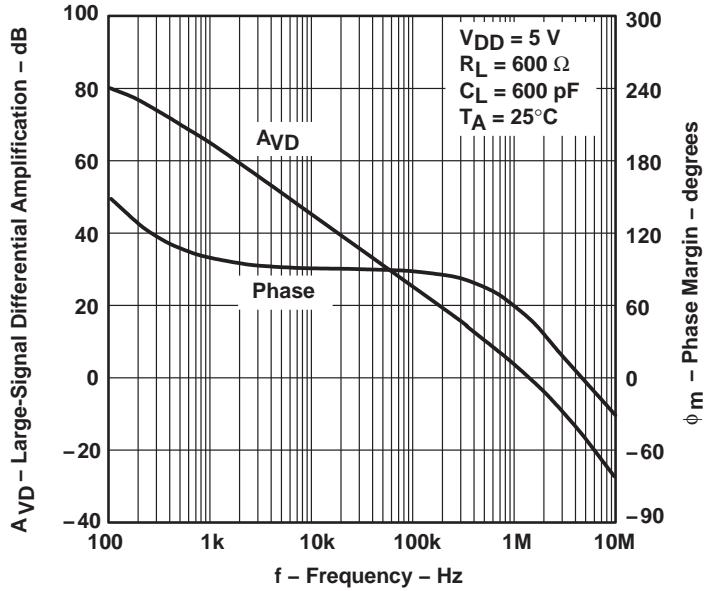


Figure 18

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

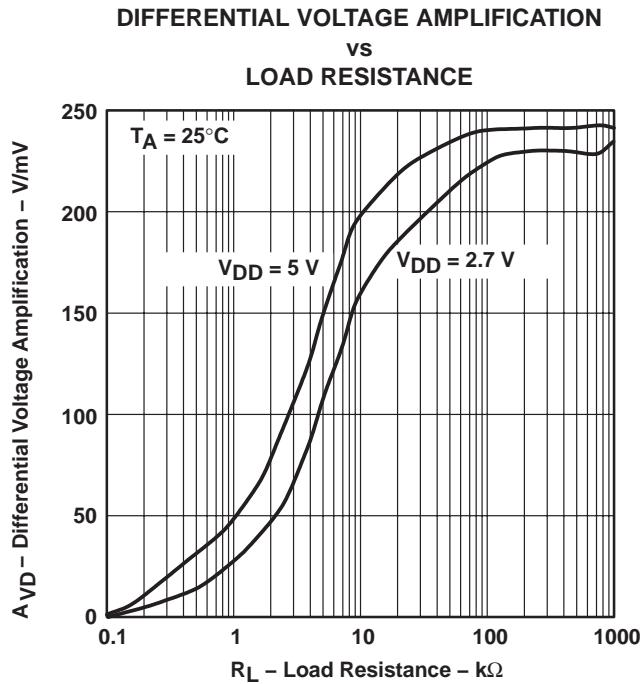


Figure 19

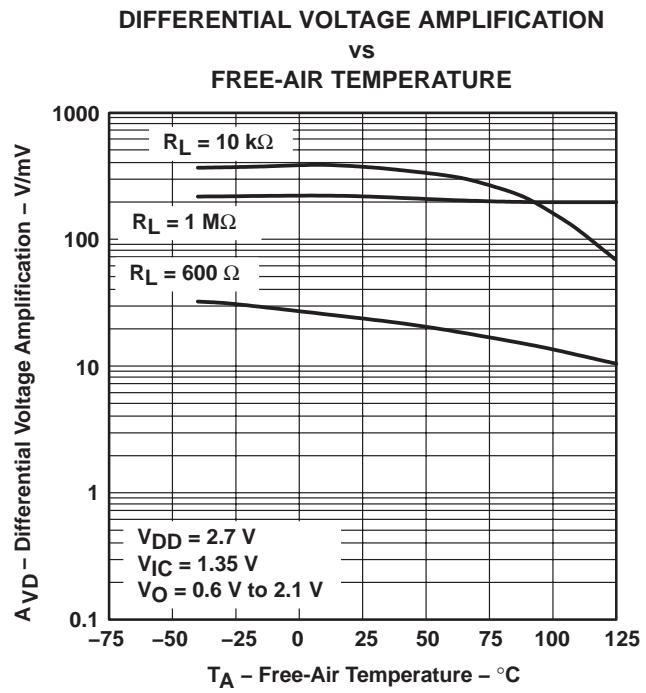


Figure 20

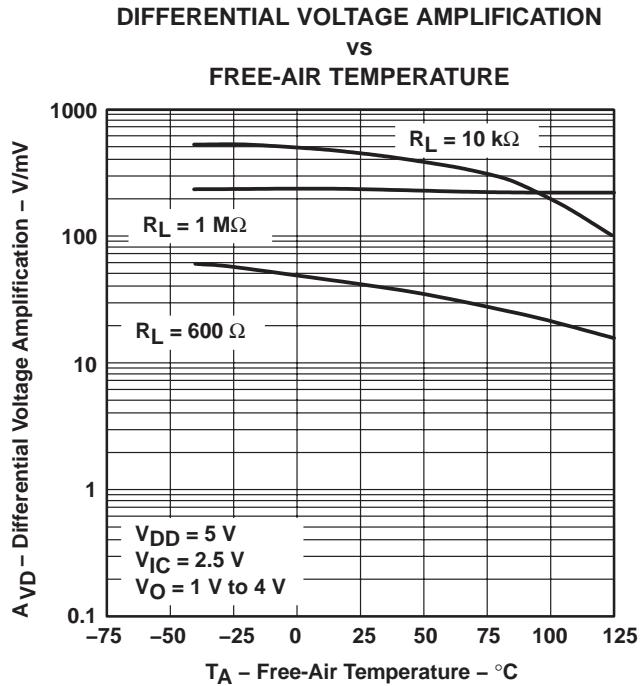


Figure 21

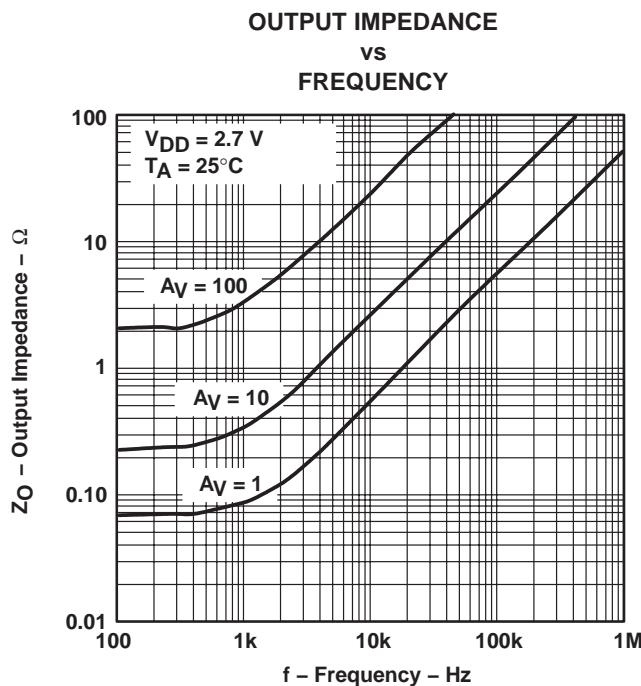


Figure 22

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

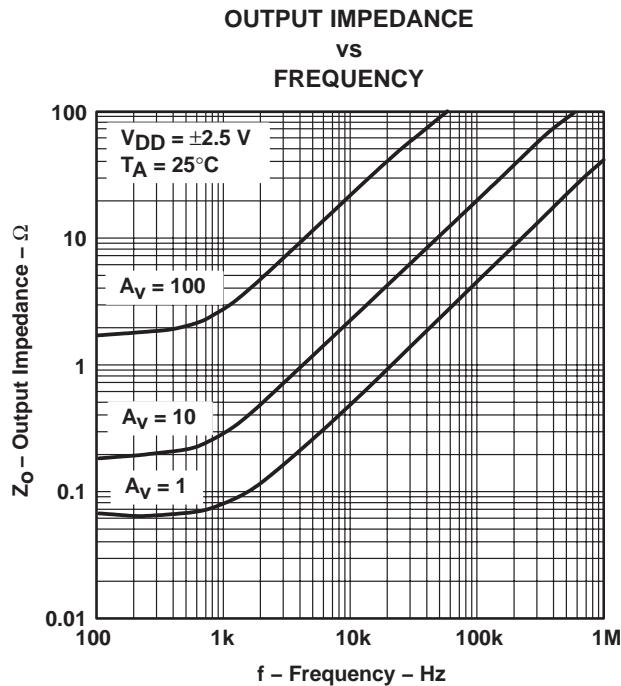


Figure 23

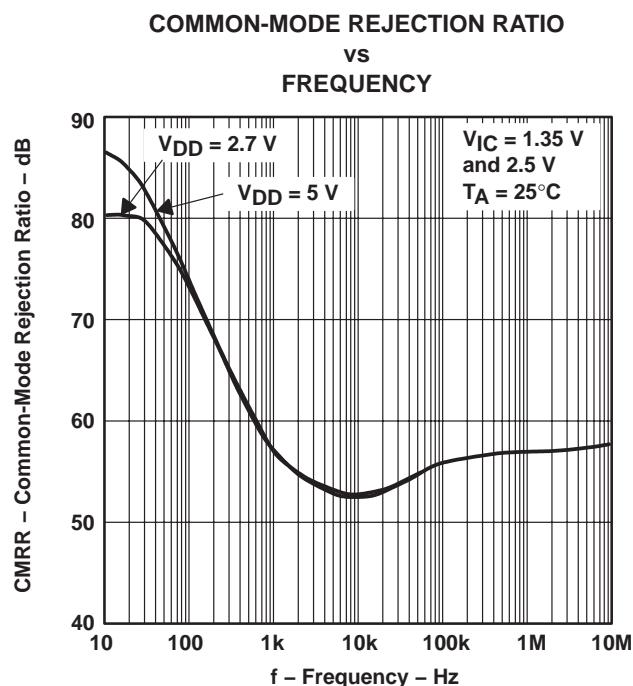


Figure 24

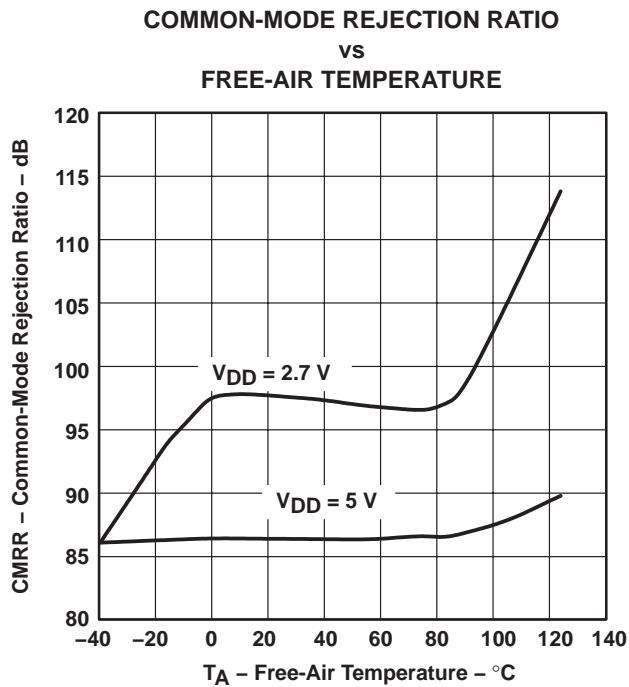


Figure 25

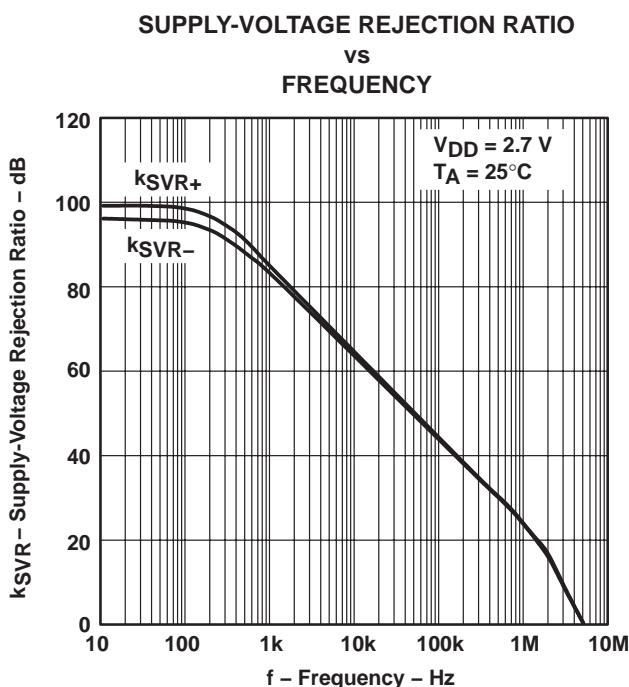


Figure 26

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

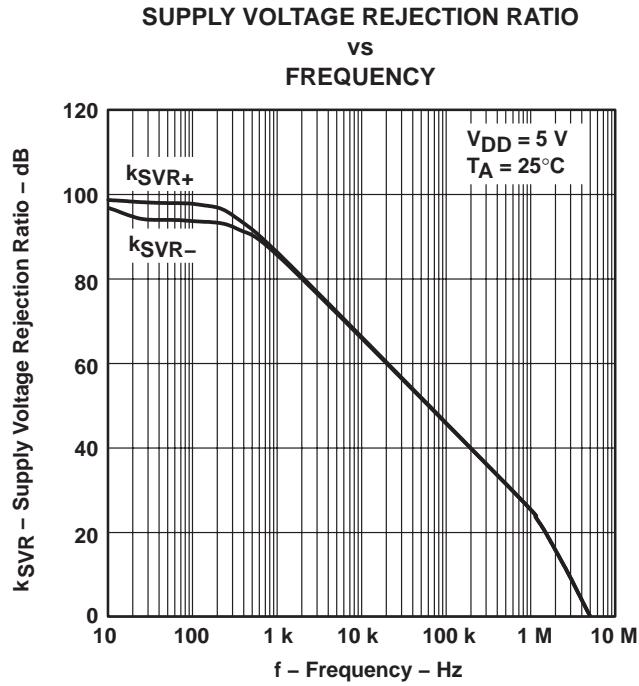


Figure 27

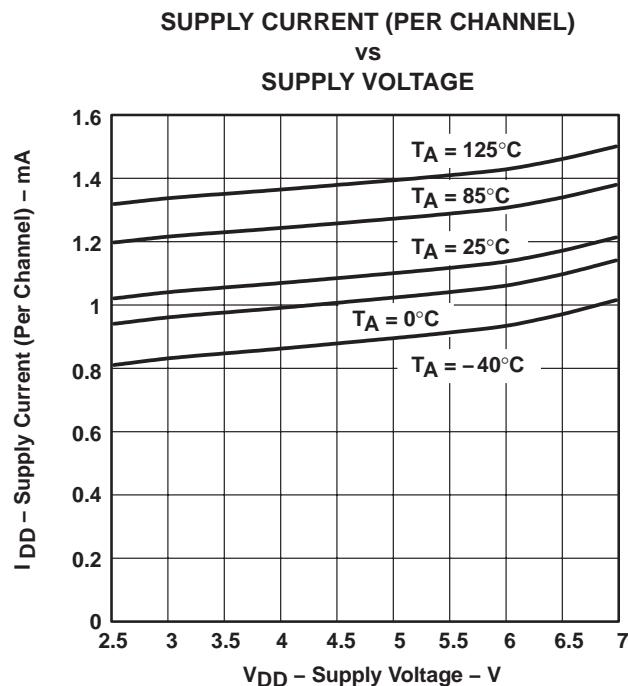


Figure 28

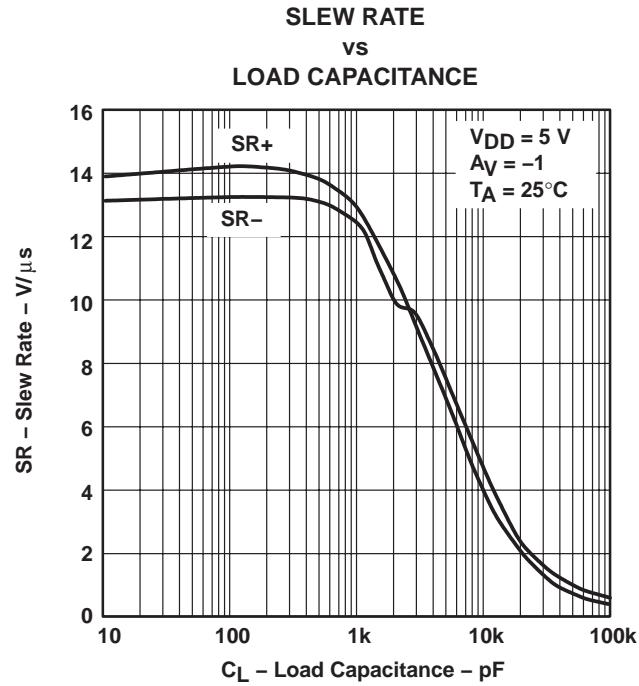


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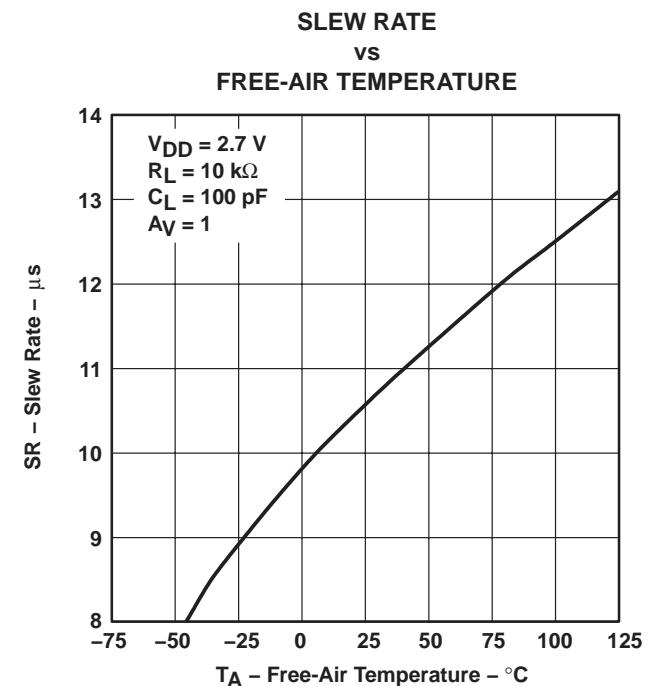


Figure 30

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT

### OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

## TYPICAL CHARACTERISTICS

### VOLTAGE-FOLLOWER SMALL-SIGNAL PULSE RESPONSE

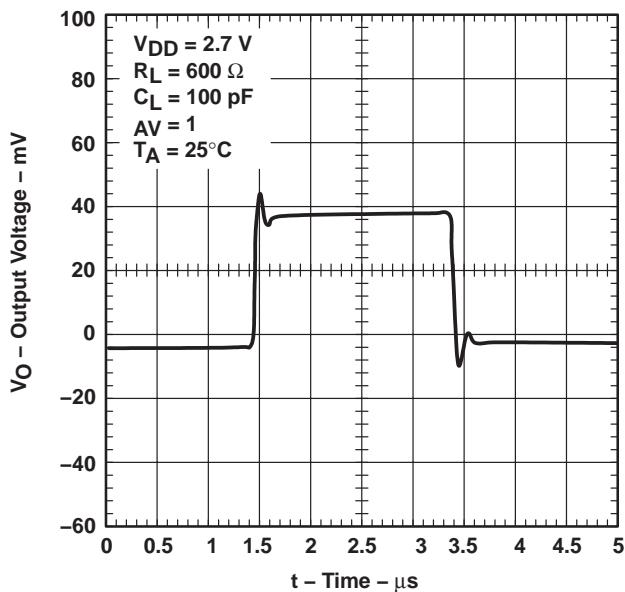


Figure 31

### VOLTAGE-FOLLOWER SMALL-SIGNAL PULSE RESPONSE

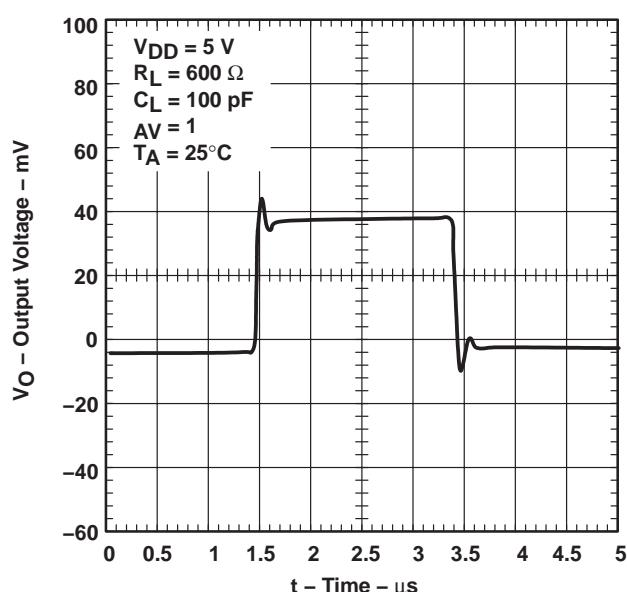


Figure 32

### VOLTAGE-FOLLOWER LARGE-SIGNAL PULSE RESPONSE

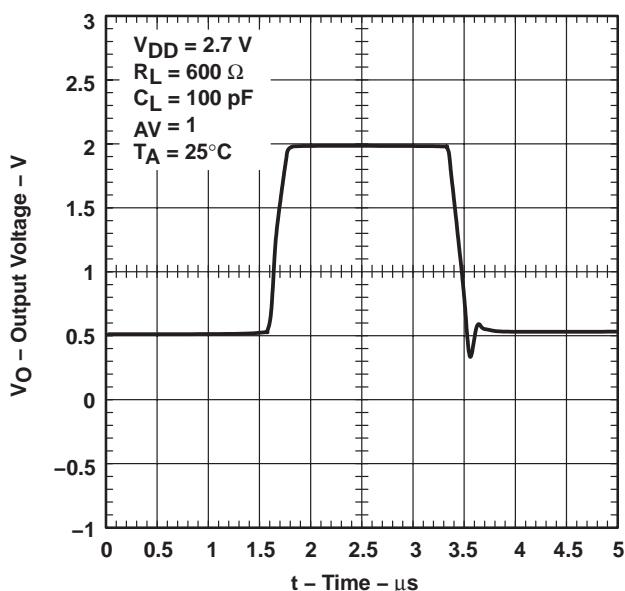


Figure 33

### VOLTAGE-FOLLOWER LARGE-SIGNAL PULSE RESPONSE

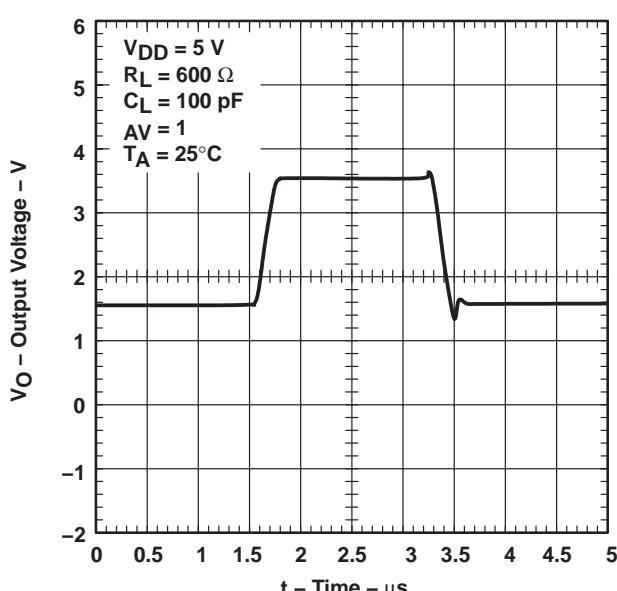
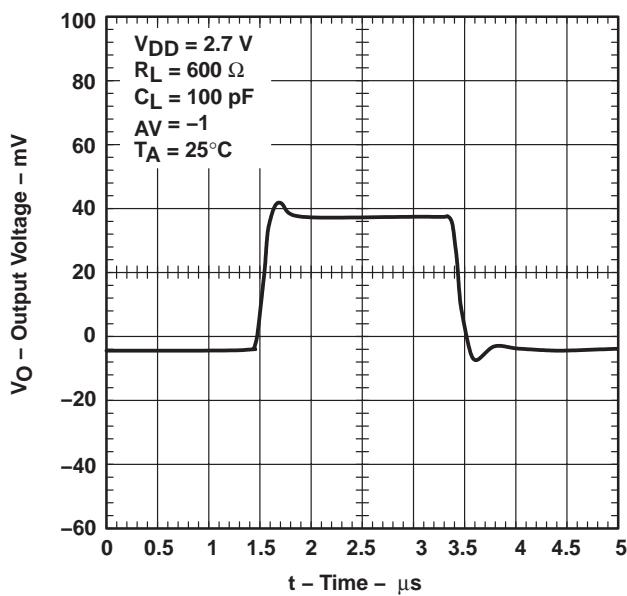


Figure 34

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

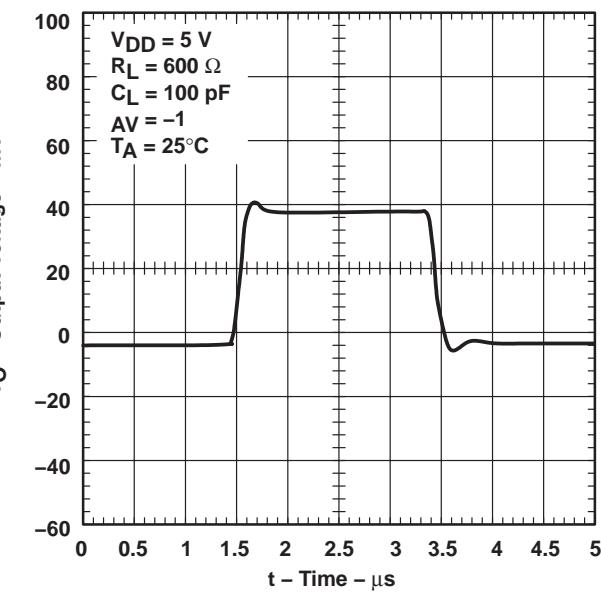
**TYPICAL CHARACTERISTICS**

**INVERTING SMALL-SIGNAL  
PULSE RESPONSE**



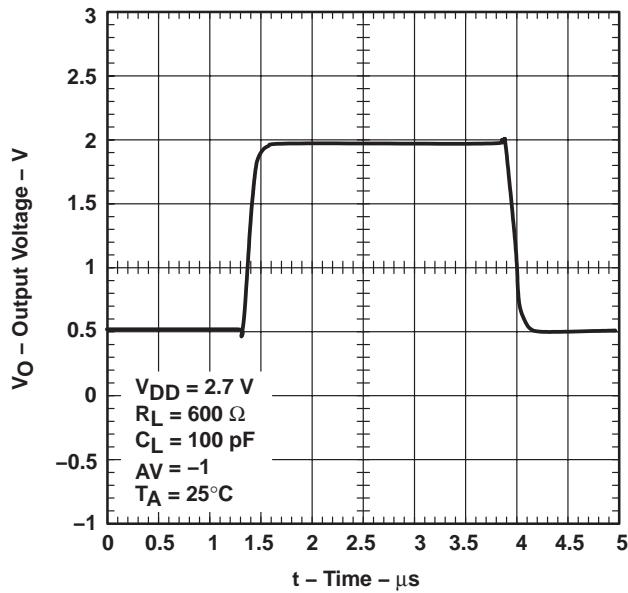
**Figure 35**

**INVERTING SMALL-SIGNAL  
PULSE RESPONSE**



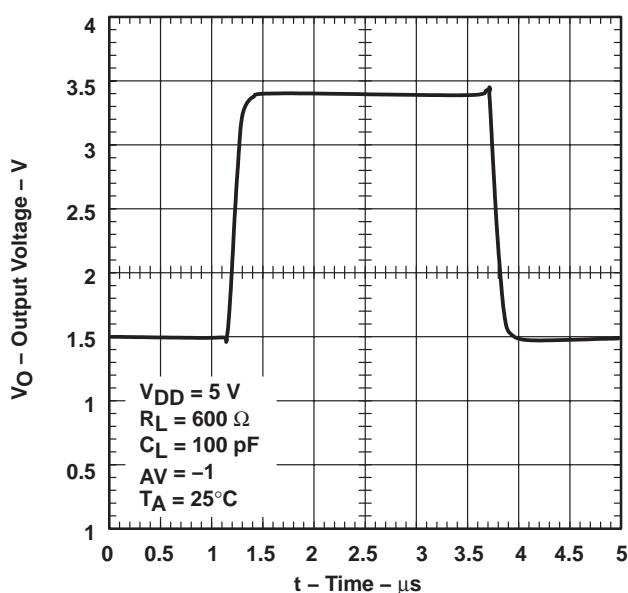
**Figure 36**

**INVERTING LARGE-SIGNAL  
PULSE RESPONSE**



**Figure 37**

**INVERTING LARGE-SIGNAL  
PULSE RESPONSE**



**Figure 38**

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

**EQUIVALENT INPUT NOISE VOLTAGE  
VS  
FREQUENCY**

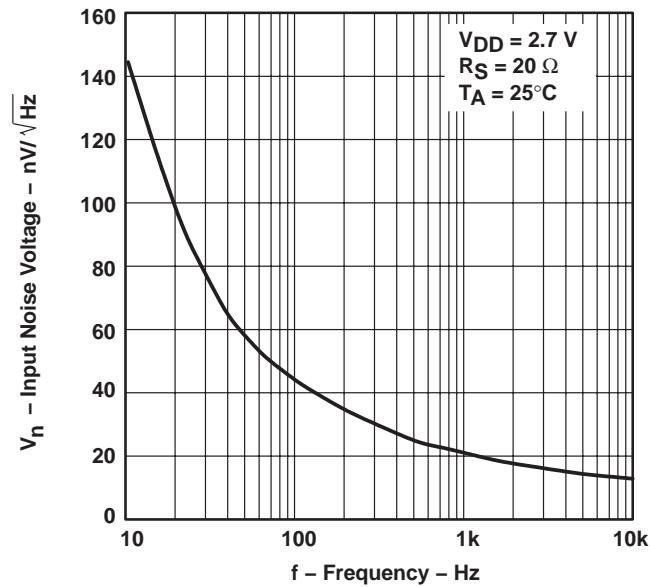


Figure 39

**EQUIVALENT INPUT NOISE VOLTAGE  
VS  
FREQUENCY**

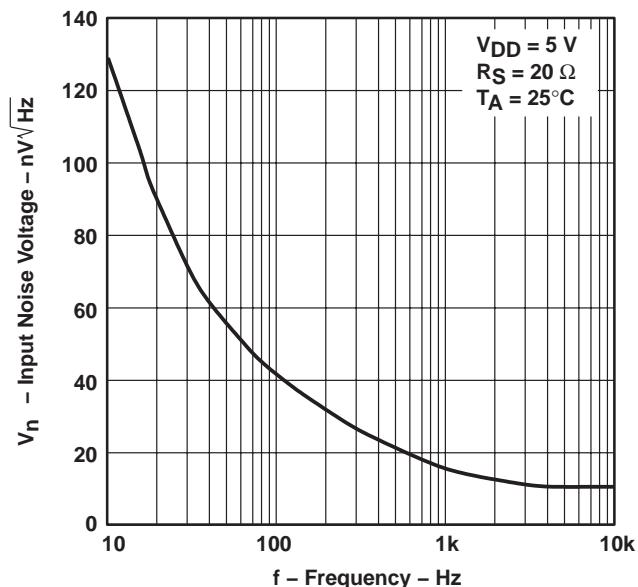


Figure 40

**NOISE VOLTAGE  
OVER A 10 SECOND PERIOD**

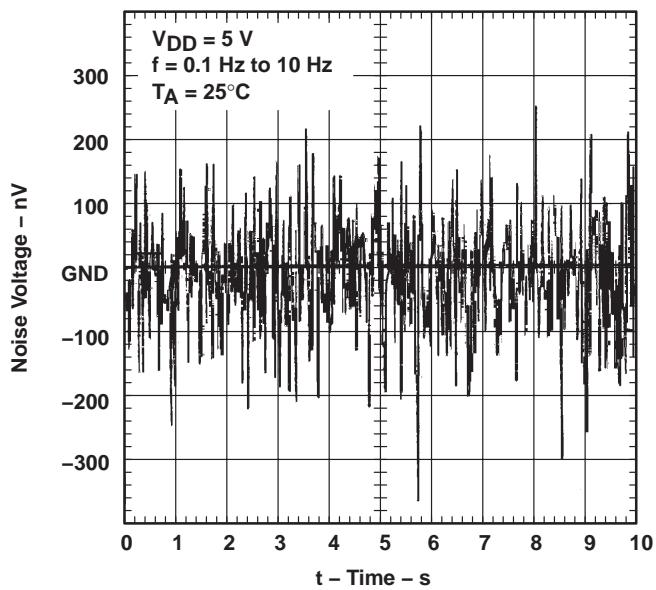


Figure 41

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

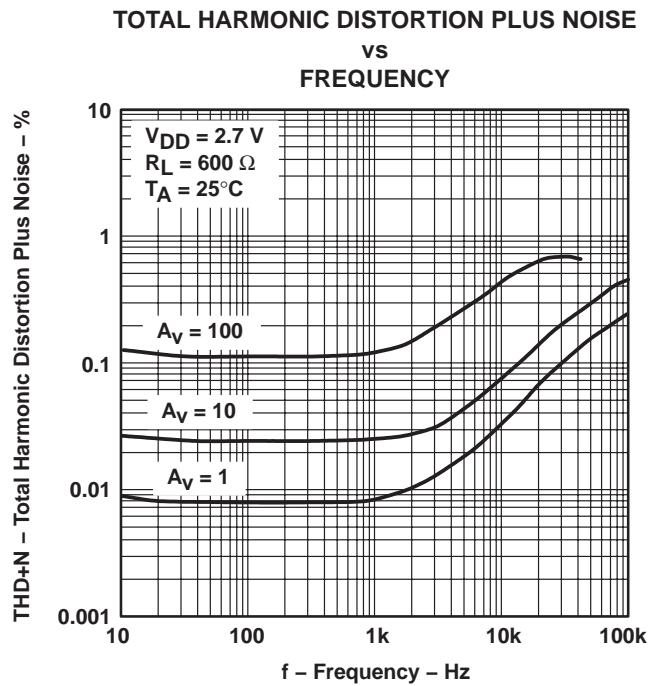


Figure 42

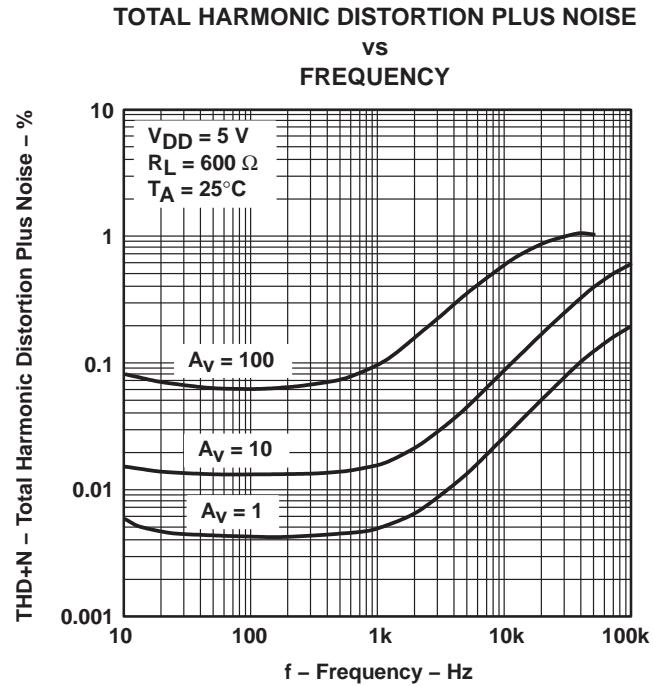


Figure 43

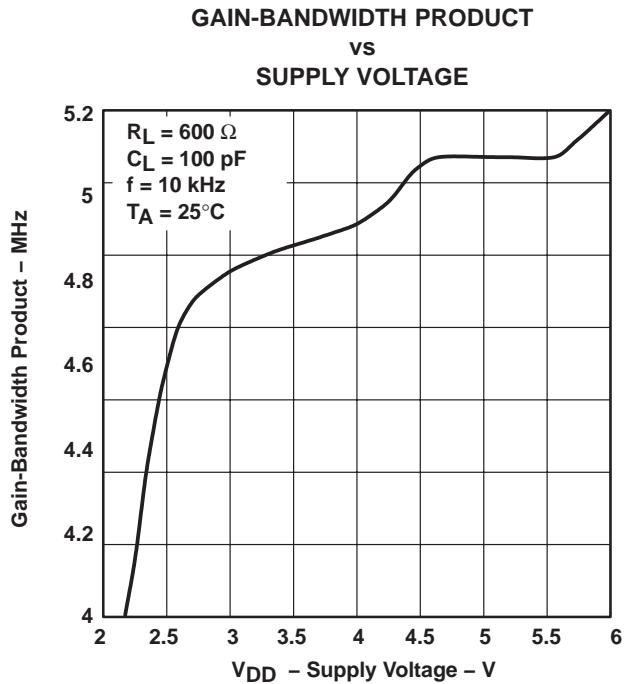


Figure 44

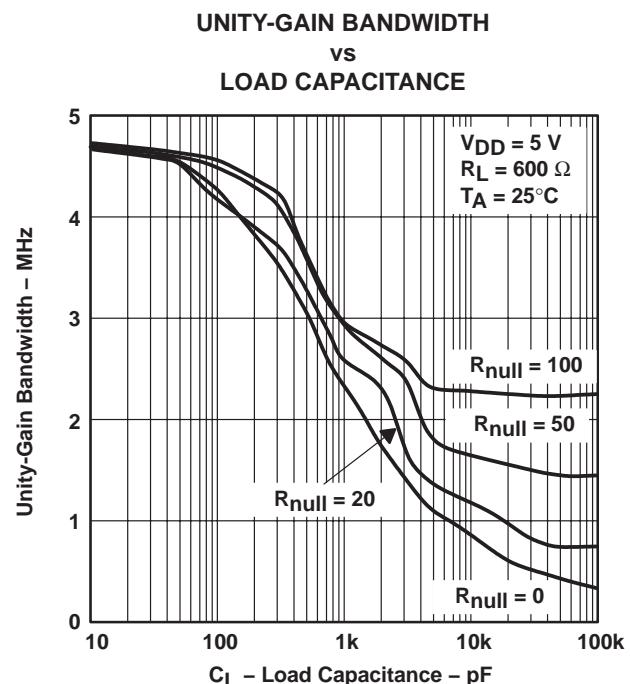


Figure 45

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

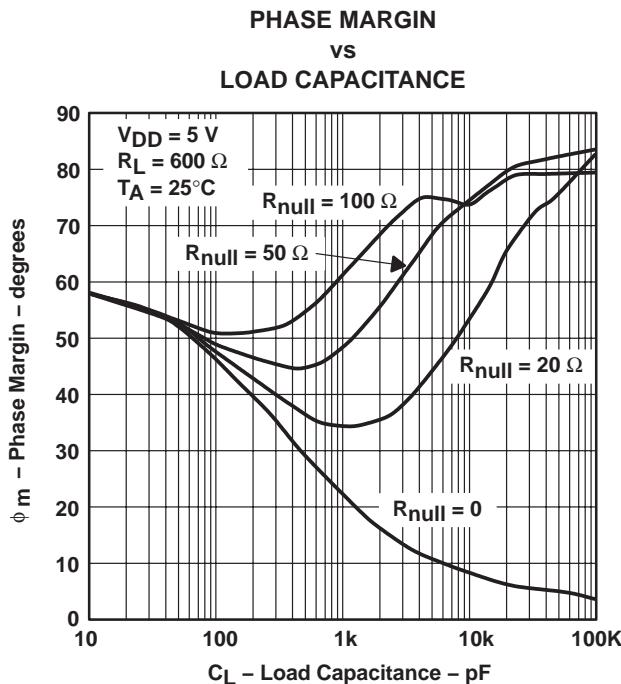


Figure 46

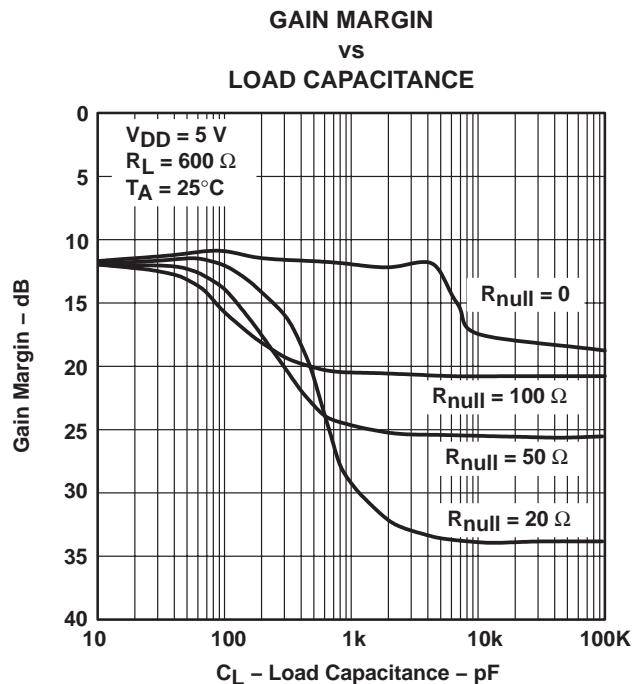


Figure 47

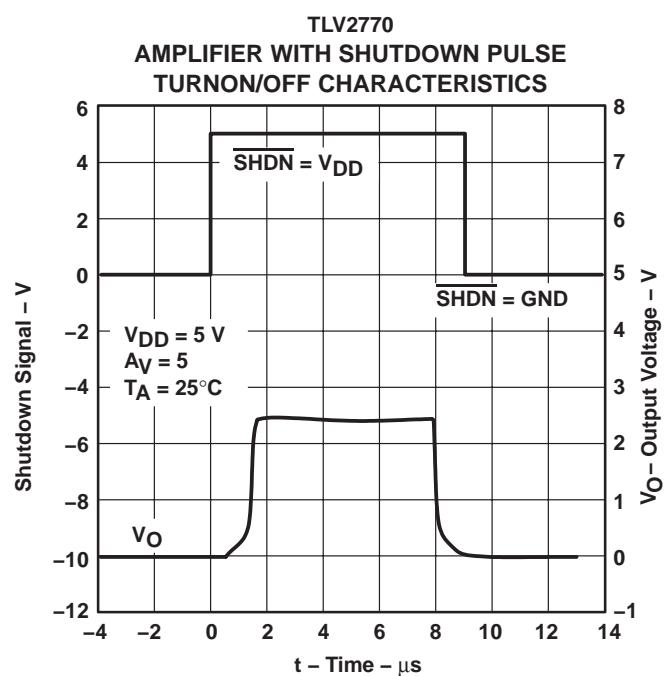


Figure 48

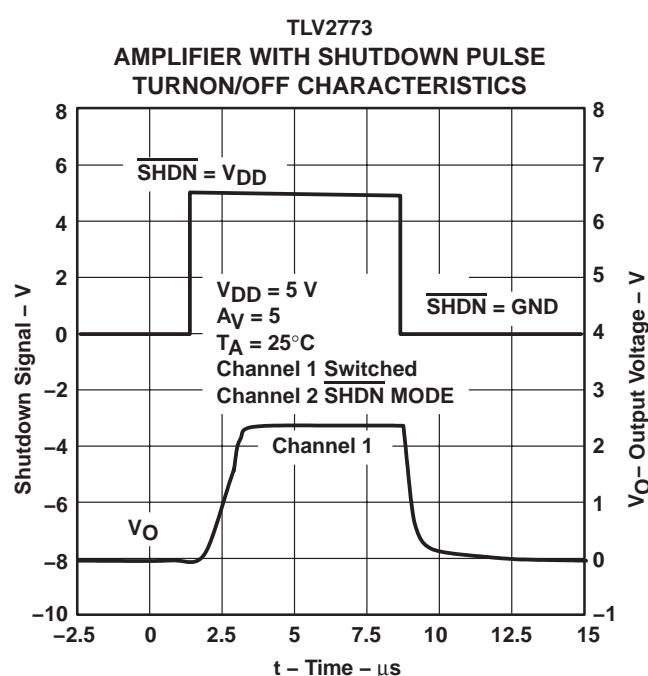


Figure 49

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

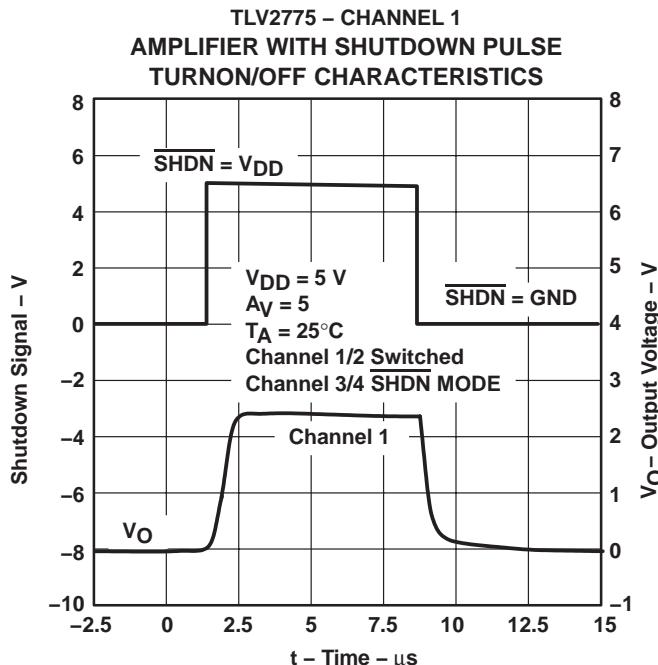


Figure 50

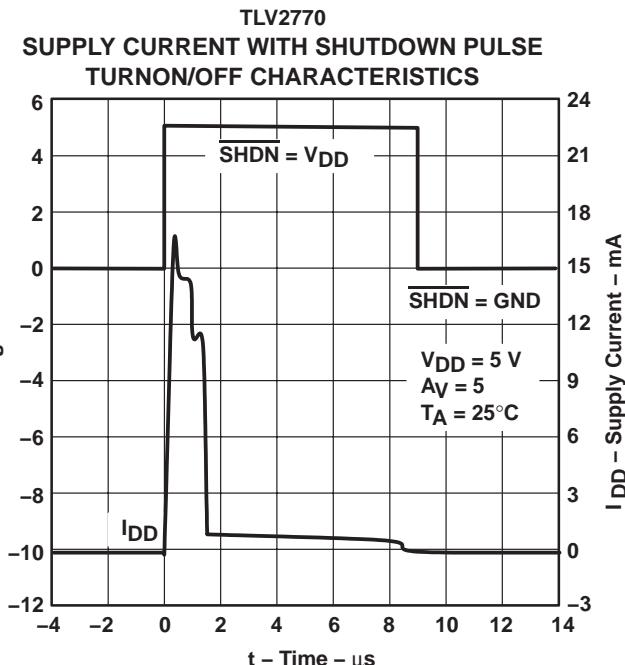


Figure 51

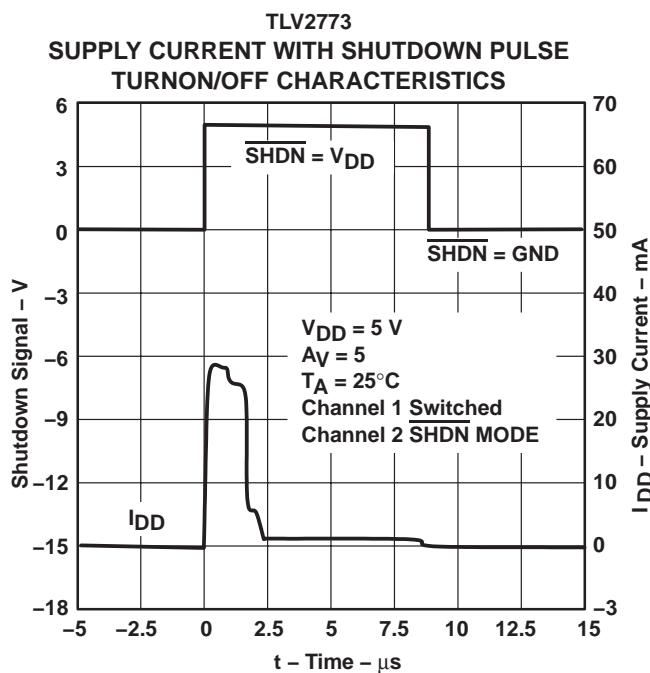


Figure 52

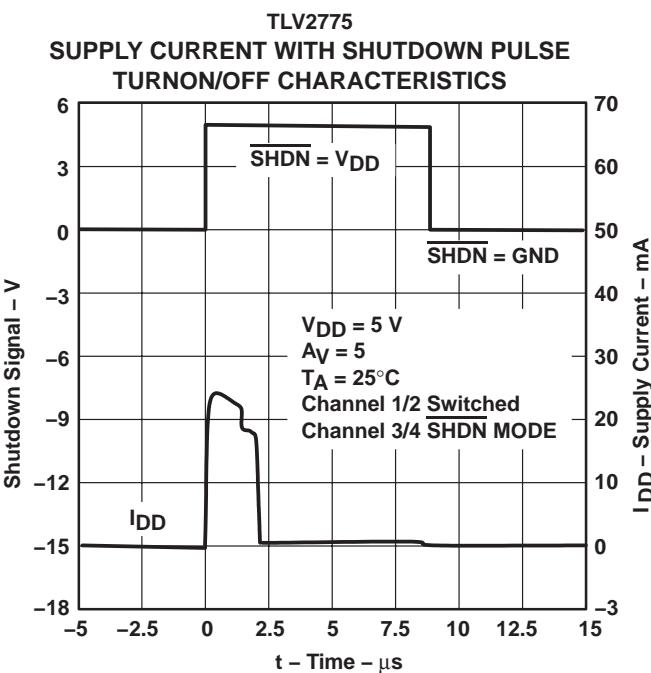


Figure 53

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B—SEPTEMBER 2003—REVISED APRIL 2006

**TYPICAL CHARACTERISTICS**

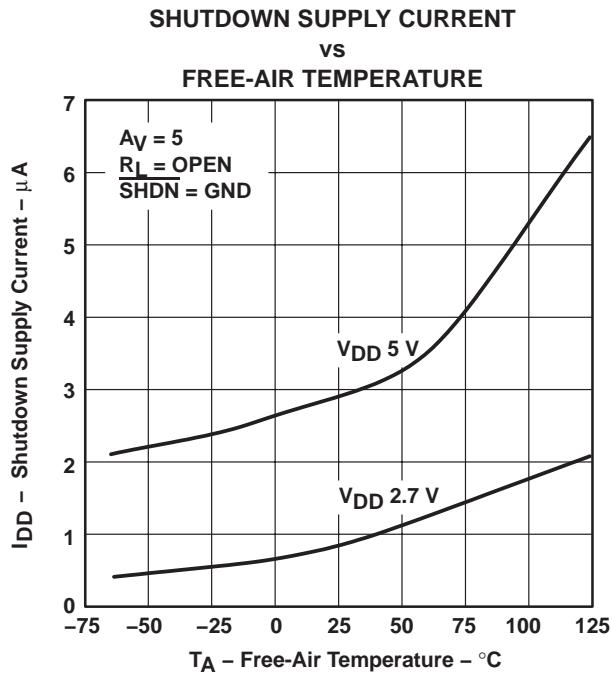


Figure 54

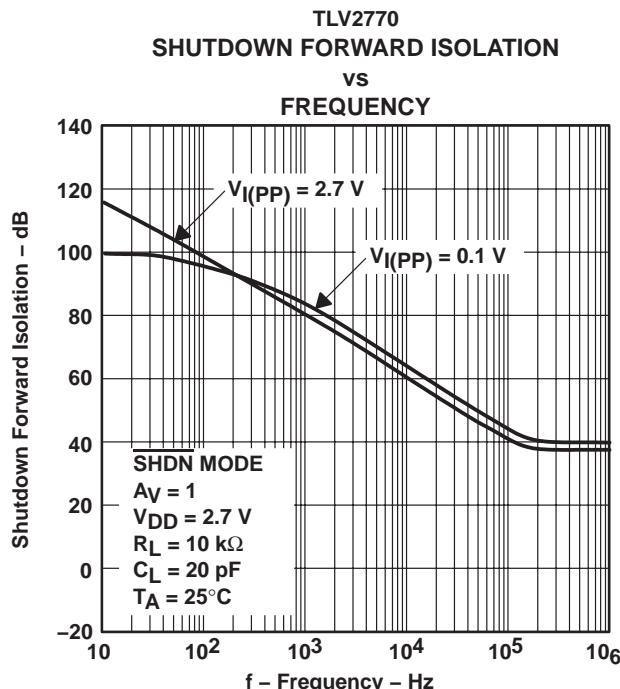


Figure 55

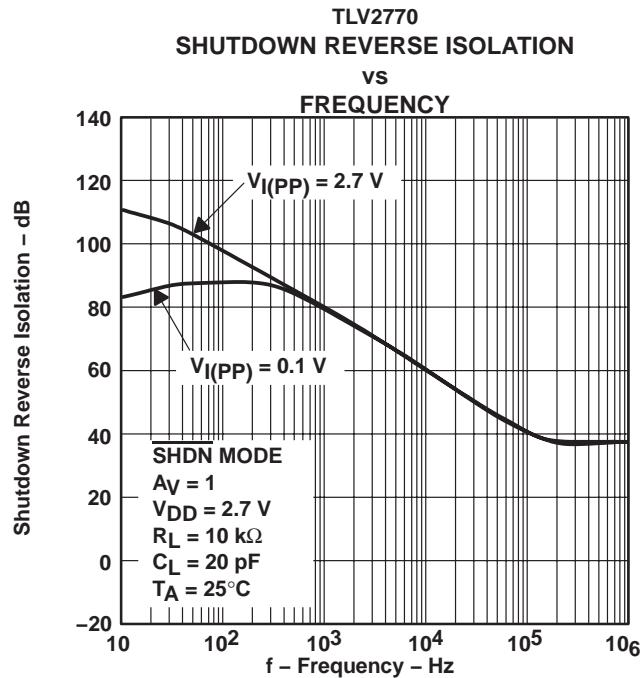
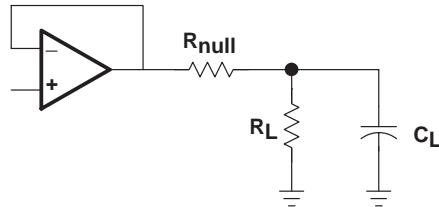


Figure 56

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

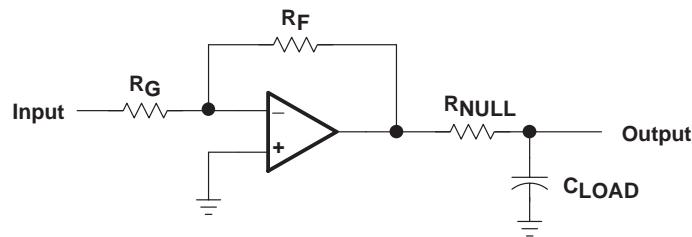
**PARAMETER MEASUREMENT INFORMATION**



**Figure 57**

**driving a capacitive load**

When the amplifier is configured in this manner, capacitive loading directly on the output decreases the device's phase margin leading to high frequency ringing or oscillations. Therefore, for capacitive loads of greater than 10 pF, it is recommended that a resistor be placed in series ( $R_{NULL}$ ) with the output of the amplifier, as shown in Figure 58. A minimum value of 20  $\Omega$  should work well for most applications.



**Figure 58. Driving a Capacitive Load**

# TLV277x-Q1, TLV277xA-Q1 FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003 – REVISED APRIL 2006

## APPLICATION INFORMATION

### offset voltage

The output offset voltage, ( $V_{OO}$ ) is the sum of the input offset voltage ( $V_{IO}$ ) and both input bias currents ( $I_{IB}$ ) times the corresponding gains. The following schematic and formula can be used to calculate the output offset voltage:

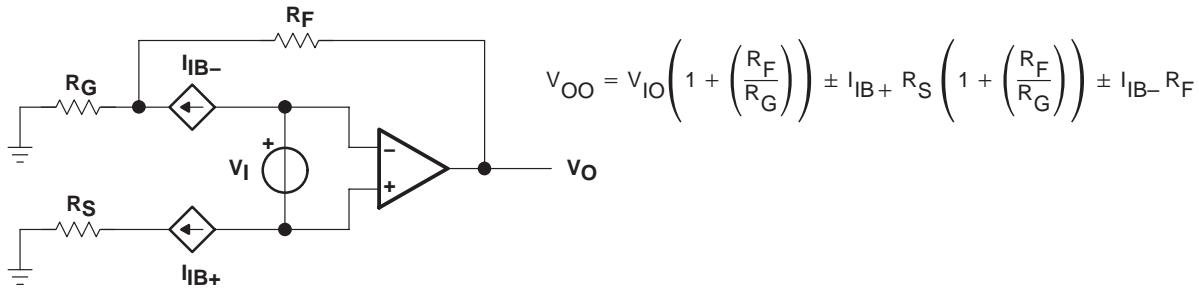


Figure 59. Output Offset Voltage Model

### general configurations

When receiving low-level signals, limiting the bandwidth of the incoming signals into the system is often required. The simplest way to accomplish this is to place an RC filter at the noninverting terminal of the amplifier (see Figure 60).

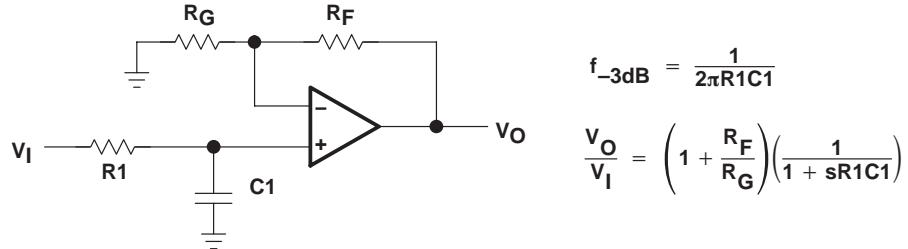


Figure 60. Single-Pole Low-Pass Filter

If even more attenuation is needed, a multiple pole filter is required. The Sallen-Key filter can be used for this task. For best results, the amplifier should have a bandwidth that is 8 to 10 times the filter frequency bandwidth. Failure to do this can result in phase shift of the amplifier.

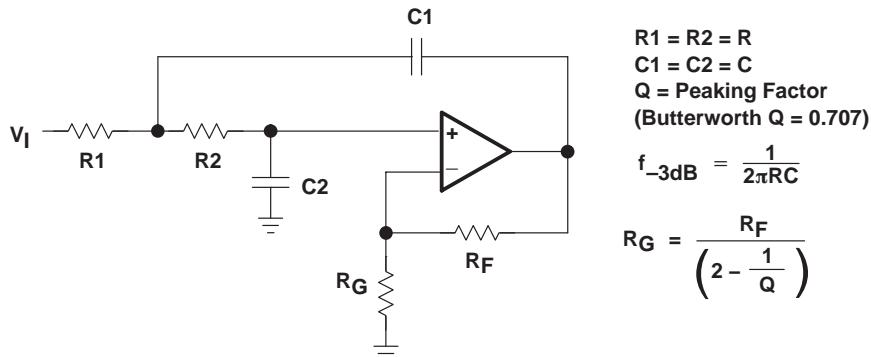


Figure 61. 2-Pole Low-Pass Sallen-Key Filter

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
 SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

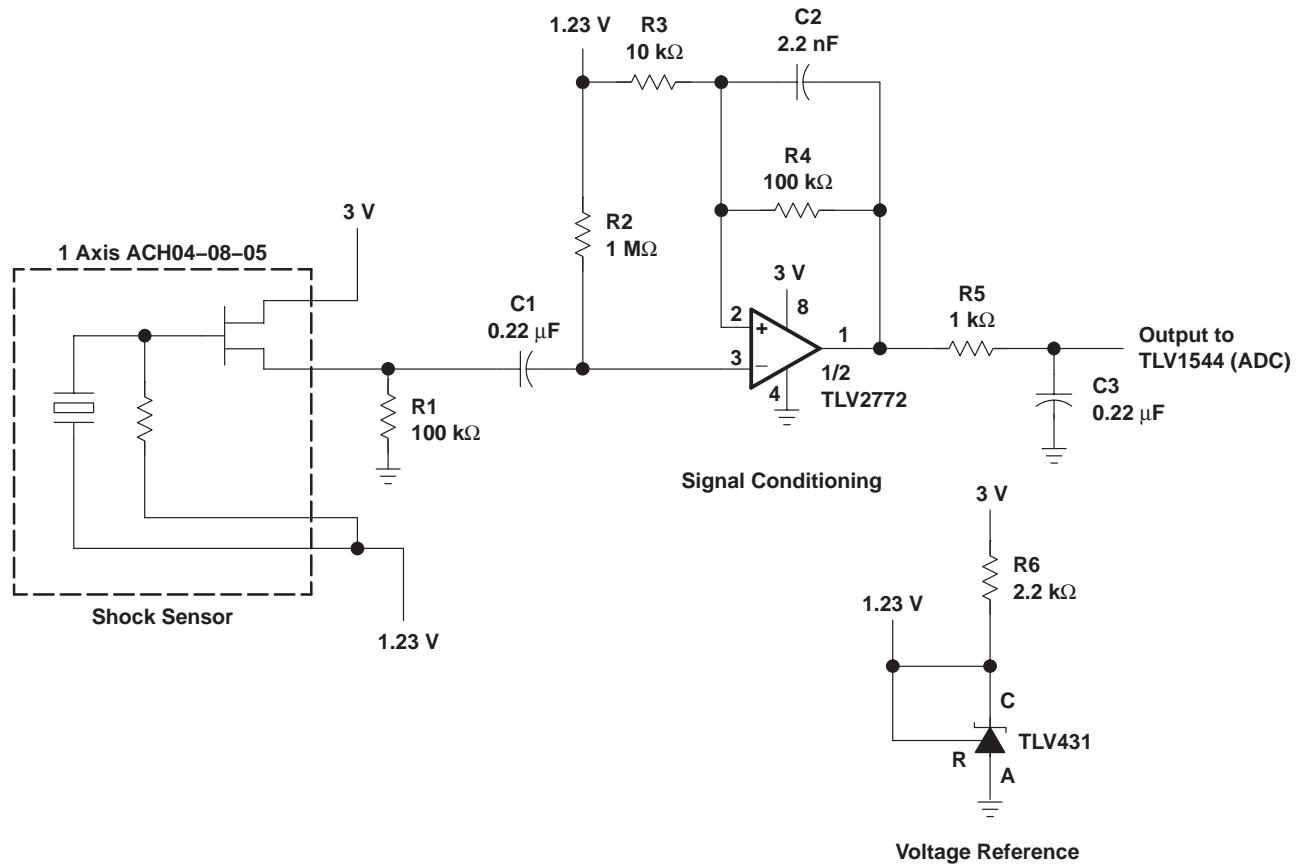
**APPLICATION INFORMATION**

**using the TLV2772 as an accelerometer interface**

The schematic, shown in Figure 62, shows the ACH04-08-05 interfaced to the TLV1544 10-bit analog-to-digital converter (ADC).

The ACH04-08-05 is a shock sensor designed to convert mechanical acceleration into electrical signals. The sensor contains three piezoelectric sensing elements oriented to simultaneously measure acceleration in three orthogonal, linear axes (x, y, z). The operating frequency is 0.5 Hz to 5 kHz. The output is buffered with an internal JFET and has a typical output voltage of 1.80 mV/g for the x and y axis and 1.35 mV/g for the z axis.

Amplification and frequency shaping of the shock sensor output is done by the TLV2772 rail-to-rail operational amplifier. The TLV2772 is ideal for this application as it offers high input impedance, good slew rate, and excellent dc precision. The rail-to-rail output swing and high output drive are perfect for driving the analog input of the TLV1544 ADC.



**Figure 62. Accelerometer Interface Schematic**

The sensor signal must be amplified and frequency-shaped to provide a signal the ADC can properly convert into the digital domain. Figure 62 shows the topology used in this application for one axis of the sensor. This system is powered from a single 3-V supply. Configuring the TLV431 with a 2.2-kΩ resistor produces a reference voltage of 1.23 V. This voltage is used to bias the operational amplifier and the internal JFETs in the shock sensor.

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT

### OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003 – REVISED APRIL 2006

## APPLICATION INFORMATION

### gain calculation

Since the TLV2772 is capable of rail-to-rail output using a 3-V supply,  $V_O = 0$  (min) to 3 V (max). With no signal from the sensor, nominal  $V_O$  = reference voltage = 1.23 V. Therefore, the maximum negative swing from nominal is  $0\text{ V} - 1.23\text{ V} = -1.23\text{ V}$  and the maximum positive swing is  $3\text{ V} - 1.23\text{ V} = 1.77\text{ V}$ . By modeling the shock sensor as a low impedance voltage source with output of 2.25 mV/g (max) in the x and y axis and 1.7 mV/g (max) in the z axis, the gain of the circuit is calculated by equation 1.

$$\text{Gain} = \frac{\text{Output Swing}}{\text{Sensor Signal} \times \text{Acceleration}} \quad (1)$$

To avoid saturation of the operational amplifier, the gain calculations are based on the maximum negative swing of  $-1.23\text{ V}$  and the maximum sensor output of 2.25 mV/g (x and y axis) and 1.70 mV/g (z axis).

$$\text{Gain (x, y)} = \frac{-1.23\text{ V}}{2.25\text{ mV/g} \times -50\text{ g}} = 10.9 \quad (2)$$

and

$$\text{Gain (z)} = \frac{-1.23\text{ V}}{1.70\text{ mV/g} \times -50\text{ g}} = 14.5 \quad (3)$$

By selecting  $R_3 = 10\text{ k}\Omega$  and  $R_4 = 100\text{ k}\Omega$ , in the x and y channels, a gain of 11 is realized. By selecting  $R_3 = 7.5\text{ k}\Omega$  and  $R_4 = 100\text{ k}\Omega$ , in the z channel, a gain of 14.3 is realized. The schematic shows the configuration for either the x- or y-axis.

### bandwidth calculation

To calculate the component values for the frequency shaping characteristics of the signal conditioning circuit, 1 Hz and 500 Hz are selected as the minimum required 3-dB bandwidth.

To minimize the value of the input capacitor (C1) required to set the lower cutoff frequency requires a large value resistor for R2 is required. A 1-M $\Omega$  resistor is used in this example. To set the lower cutoff frequency, the required capacitor value for C1 is:

$$C_1 = \frac{1}{2\pi f_{\text{LOW}} R_2} = 0.159\text{ }\mu\text{F} \quad (4)$$

Using a value of 0.22  $\mu\text{F}$ , a more common value of capacitor, the lower cutoff frequency is 0.724 Hz.

To minimize the phase shift in the feedback loop caused by the input capacitance of the TLV2772, it is best to minimize the value of the feedback resistor R4. However, to reduce the required capacitance in the feedback loop a large value for R4 is required. Therefore, a compromise for the value of R4 must be made. In this circuit, a value of 100 k $\Omega$  has been selected. To set the upper cutoff frequency, the required capacitor value for C2 is:

$$C_2 = \frac{1}{2\pi f_{\text{HIGH}} R_4} = 3.18\text{ }\mu\text{F} \quad (5)$$

Using a 2.2-nF capacitor, the upper cutoff frequency is 724 Hz.

R5 and C3 also cause the signal response to roll off. Therefore, it is beneficial to design this roll-off point to begin at the upper cutoff frequency. Assuming a value of 1 k $\Omega$  for R5, the value for C3 is calculated to be 0.22  $\mu\text{F}$ .

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**  
SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

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## APPLICATION INFORMATION

### circuit layout considerations

To achieve the levels of high performance of the TLV277x, follow proper printed-circuit board design techniques. A general set of guidelines is given in the following.

- **Ground planes**—It is highly recommended that a ground plane be used on the board to provide all components with a low inductive ground connection. However, in the areas of the amplifier inputs and output, the ground plane can be removed to minimize the stray capacitance.
- **Proper power supply decoupling**—Use a 6.8- $\mu$ F tantalum capacitor in parallel with a 0.1- $\mu$ F ceramic capacitor on each supply terminal. It may be possible to share the tantalum among several amplifiers depending on the application, but a 0.1- $\mu$ F ceramic capacitor should always be used on the supply terminal of every amplifier. In addition, the 0.1- $\mu$ F capacitor should be placed as close as possible to the supply terminal. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. The designer should strive for distances of less than 0.1 inches between the device power terminals and the ceramic capacitors.
- **Sockets**—Sockets can be used but are not recommended. The additional lead inductance in the socket pins will often lead to stability problems. Surface-mount packages soldered directly to the printed-circuit board is the best implementation.
- **Short trace runs/compact part placements**—Optimum high performance is achieved when stray series inductance has been minimized. To realize this, the circuit layout should be made as compact as possible, thereby minimizing the length of all trace runs. Particular attention should be paid to the inverting input of the amplifier. Its length should be kept as short as possible. This helps to minimize stray capacitance at the input of the amplifier.
- **Surface-mount passive components**—Using surface-mount passive components is recommended for high performance amplifier circuits for several reasons. First, because of the extremely low lead inductance of surface-mount components, the problem with stray series inductance is greatly reduced. Second, the small size of surface-mount components naturally leads to a more compact layout thereby minimizing both stray inductance and capacitance. If leaded components are used, it is recommended that the lead lengths be kept as short as possible.

# TLV277x-Q1, TLV277xA-Q1

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT

### OPERATIONAL AMPLIFIERS WITH SHUTDOWN

SGLS179B—SEPTEMBER 2003 – REVISED APRIL 2006

## APPLICATION INFORMATION

### general power dissipation considerations

For a given  $\theta_{JA}$ , the maximum power dissipation is shown in Figure 63 and is calculated by the following formula:

$$P_D = \left( \frac{T_{MAX} - T_A}{\theta_{JA}} \right)$$

Where:

$P_D$  = Maximum power dissipation of TLV277x IC (watts)

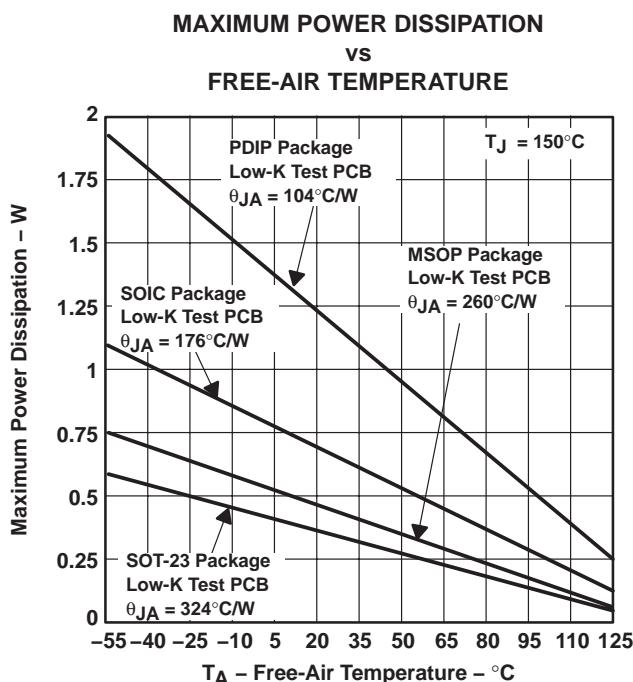
$T_{MAX}$  = Absolute maximum junction temperature (150°C)

$T_A$  = Free-ambient air temperature (°C)

$\theta_{JA}$  =  $\theta_{JC} + \theta_{CA}$

$\theta_{JC}$  = Thermal coefficient from junction-to-case

$\theta_{CA}$  = Thermal coefficient from case to ambient air (°C/W)



NOTE A: Results are with no air flow and using JEDEC Standard Low-K test PCB.

Figure 63.

**TLV277x-Q1, TLV277xA-Q1**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

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## APPLICATION INFORMATION

### shutdown function

Three members of the TLV277x family (TLV2770/3/5) have a shutdown terminal for conserving battery life in portable applications. When the shutdown terminal is tied low, the supply current is reduced to  $0.8 \mu\text{A}/\text{channel}$ , the amplifier is disabled, and the outputs are placed in a high impedance mode. To enable the amplifier, the shutdown terminal can either be left floating or pulled high. When the shutdown terminal is left floating, care needs to be taken to ensure that parasitic leakage current at the shutdown terminal does not inadvertently place the operational amplifier into shutdown. The shutdown terminal threshold is always referenced to  $V_{DD}/2$ . Therefore, when operating the device with split supply voltages (e.g.  $\pm 2.5 \text{ V}$ ), the shutdown terminal needs to be pulled to  $V_{DD-}$  (not GND) to disable the operational amplifier.

The amplifier's output with a shutdown pulse is shown in Figure 48 through Figure 50. The amplifier is powered with a single 5-V supply and configured as a noninverting configuration with a gain of 5. The amplifier turnon and turnoff times are measured from the 50% point of the shutdown pulse to the 50% point of the output waveform. The times for the single, dual, and quad are listed in the data tables. The *bump* on the rising edge of the TLV2770 output waveform is due to the start-up circuit on the bias generator. For the dual and quad (TLV2773/5), this *bump* is attributed to the bias generator's start-up circuit as well as the crosstalk between the other channel(s), which are in shutdown.

Figure 55 and Figure 56 show the amplifier's forward and reverse isolation in shutdown. The operational amplifier is powered by  $\pm 1.35\text{-V}$  supplies and configured as a voltage follower ( $A_V = 1$ ). The isolation performance is plotted across frequency for both  $0.1\text{-V}_{PP}$  and  $2.7\text{-V}_{PP}$  input signals. During normal operation, the amplifier would not be able to handle a  $2.7\text{-V}_{PP}$  input signal with a supply voltage of  $\pm 1.35 \text{ V}$  since it exceeds the common-mode input voltage range ( $V_{ICR}$ ). However, this curve illustrates that the amplifier remains in shutdown even under a worst case scenario.

# **TLV277x-Q1, TLV277xA-Q1** **FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT** **OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

SGLS179B – SEPTEMBER 2003 – REVISED APRIL 2006

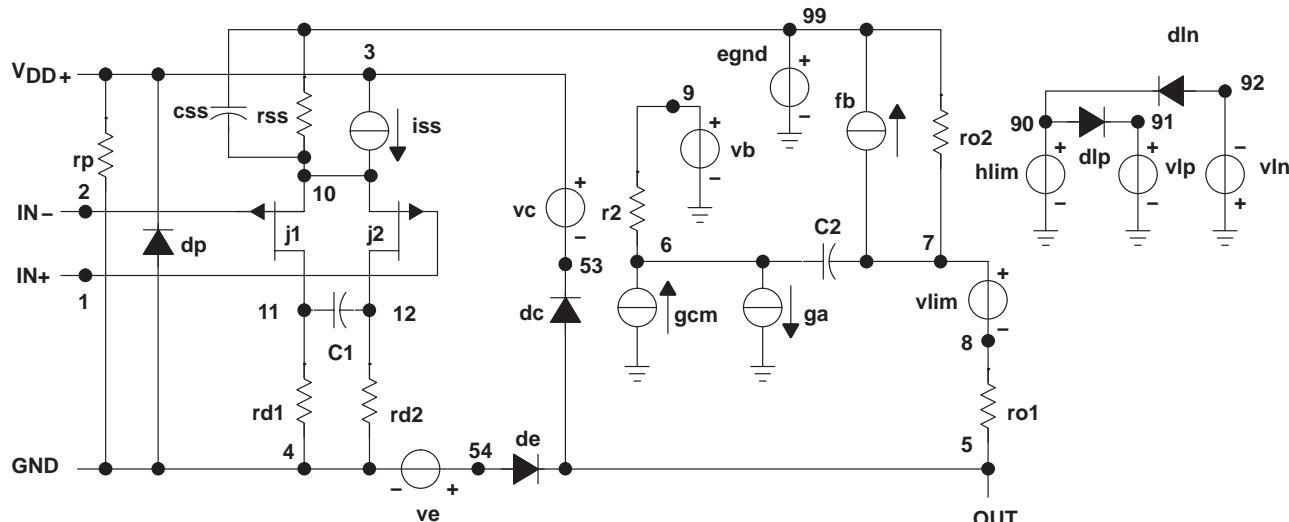
## APPLICATION INFORMATION

## macromodel information

Macromodel information provided was derived using Microsim *Parts*<sup>TM</sup> Release 8, the model generation software used with Microsim *PSpice*<sup>TM</sup>. The Boyle macromodel (see Note 4) and subcircuit in Figure 64 are generated using the TLV2772 typical electrical and operating characteristics at  $T_A = 25^\circ\text{C}$ . Using this information, output simulations of the following key parameters can be generated to a tolerance of 20% (in most cases):

- Maximum positive output voltage swing
- Maximum negative output voltage swing
- Slew rate
- Quiescent power dissipation
- Input bias current
- Open-loop voltage amplification
- Unity-gain frequency
- Common-mode rejection ratio
- Phase margin
- DC output resistance
- AC output resistance
- Short-circuit output current limit

NOTE 5: G. R. Boyle, B. M. Cohn, D. O. Pederson, and J. E. Solomon, "Macromodeling of Integrated Circuit Operational Amplifiers", *IEEE Journal of Solid-State Circuits*, SC-9, 353 (1974).



\* TLV2772 operational amplifier macromodel subcircuit  
\* created using Parts release 8.0 on 12/12/97 at 10:08

\* Parts is a MicroSim product.

\*

\* connections: noninverting input

\* inverting input

\* positive power supply  
\* negative power supply

\* \* neg  
\* 2

\*

subckt TL V2772

• \*

c1	11	12	2.8868E-12
c2	6	7	10.000E-12
css	10	99	2.6302E-12
dc	5	53	dy
de	54	5	dy
dlp	90	91	dx
dln	92	90	dx
dp	4	3	dx
egnd	99	0	poly(2) (3,0) (4,0) 0 .5 .5
fb	7	99	poly(5) vb vc ve vlp vln 0
			15.513E6 -1E3 1E3 16E6 -16E6
ga	6	0	11 12 188.50E-6
gcm	0	6	10 99 9.4472E-9

```

iss      3      10      dc      145.50E-6
hlim    90      0       vlim 1K
j1      11      2       10 jx1
j2      12      1       10 jx2
r2      6       9       100.00E3
rd1     4       11      5.3052E3
rd2     4       12      5.3052E3
ro1     8       5       17.140
ro2     7       99      17.140
rp      3       4       4.5455E3
rss     10      99      1.3746E6
vb      9       0       dc 0
vc      3       53      dc .82001
ve      54      4       dc .82001
vlim    7       8       dc 0
vlp     91      0       dc 47
vln     0       92      dc 47
.model  dx      D(Is=800.00E-18)
.model  dy      D(Is=800.00E-18 Rs=1m Cjo=10p)
.model  jx1     PJF(Is=2.2500E-12 Beta=244.20E-6
+ Vto=-.99765)
.model  jx2     PJF(Is=1.7500E-12 Beta=244.20E-6
+ Vto=-1.002350)

```

10\*

**Figure 64. Boyle Macromodel and Subcircuit**

*PSpice* and *Parts* are trademarks of MicroSim Corporation.

**PACKAGING INFORMATION**

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
TLV2771QDBVRQ1	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TLV2772AQDRQ1	ACTIVE	SOIC	D	8	2500	TBD	Call TI	Call TI
TLV2772AQPWRQ1	ACTIVE	TSSOP	PW	8	2000	TBD	Call TI	Call TI
TLV2772QDRQ1	ACTIVE	SOIC	D	8	2500	TBD	Call TI	Call TI
TLV2772QPWRQ1	ACTIVE	TSSOP	PW	8	2000	TBD	CU NIPDAU	Level-1-220C-UNLIM

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBsolete:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

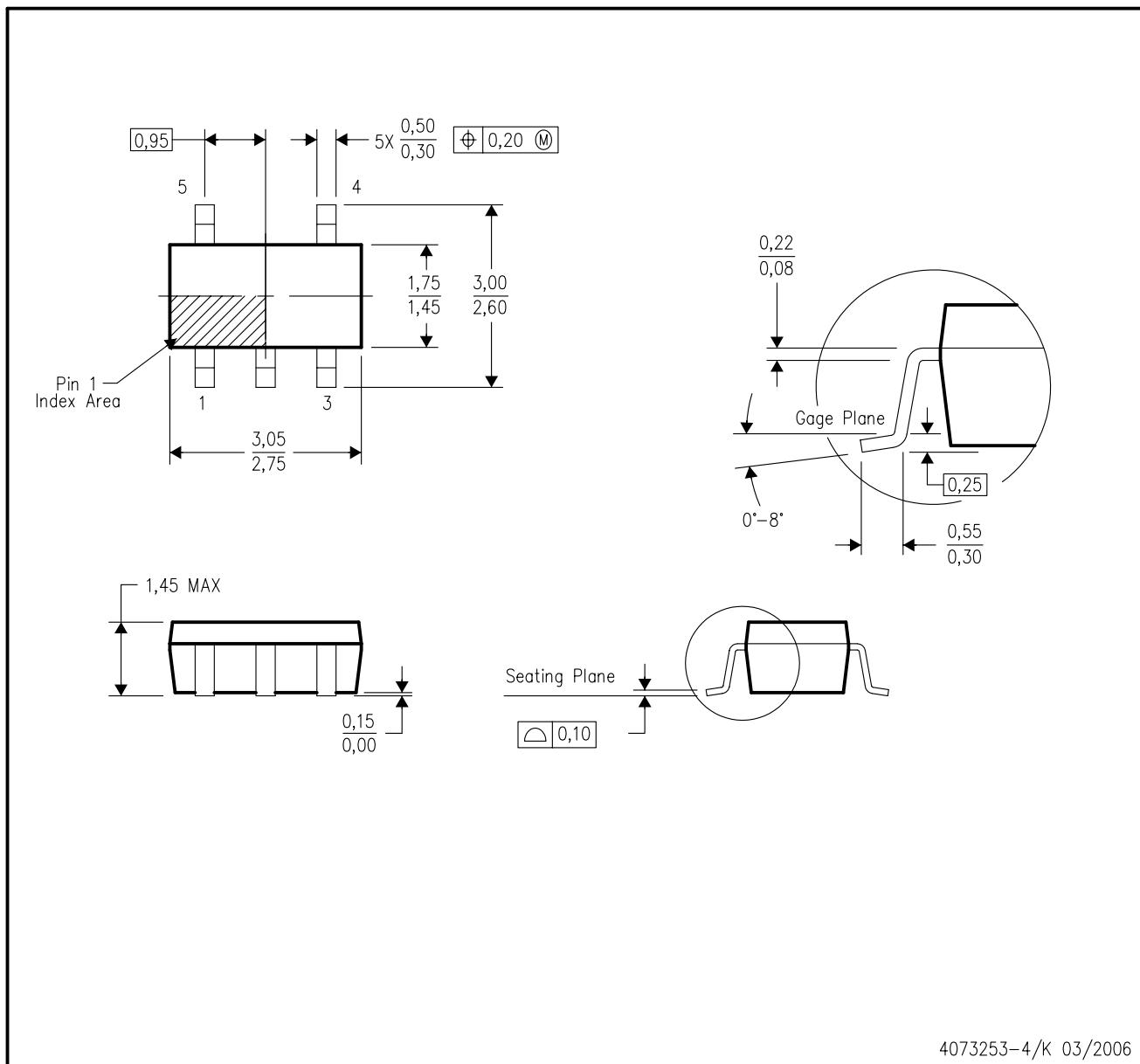
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## MECHANICAL DATA

DBV (R-PDSO-G5)

PLASTIC SMALL-OUTLINE PACKAGE



4073253-4/K 03/2006

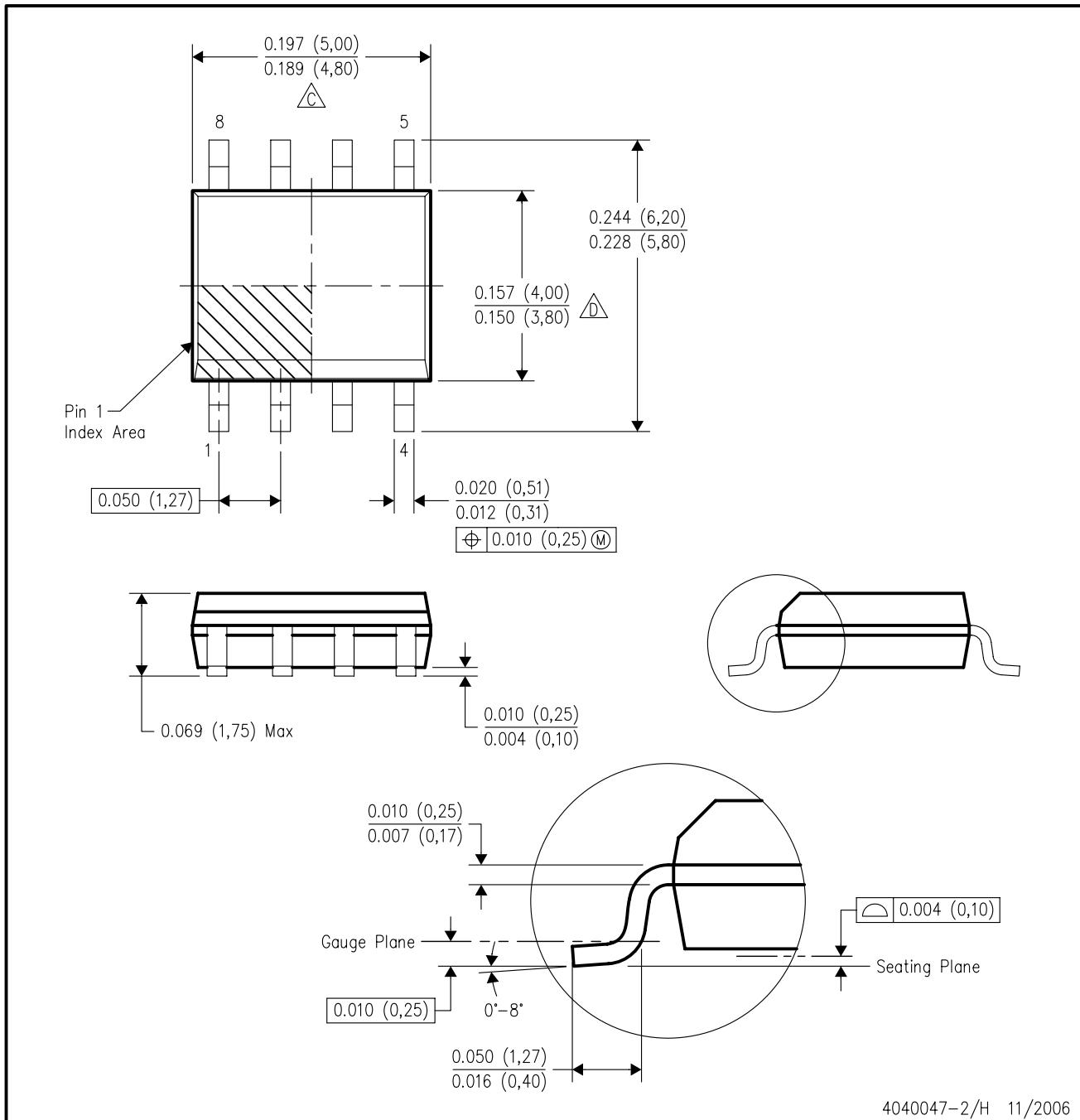
NOTES:

- All linear dimensions are in millimeters.
- This drawing is subject to change without notice.
- Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
- Falls within JEDEC MO-178 Variation AA.

## MECHANICAL DATA

### D (R-PDSO-G8)

### PLASTIC SMALL-OUTLINE PACKAGE



4040047-2/H 11/2006

NOTES: A. All linear dimensions are in inches (millimeters).

B. This drawing is subject to change without notice.

$\triangle$  C Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 (0,15) per end.

$\triangle$  D Body width does not include interlead flash. Interlead flash shall not exceed .017 (0,43) per side.

E. Reference JEDEC MS-012 variation AA.

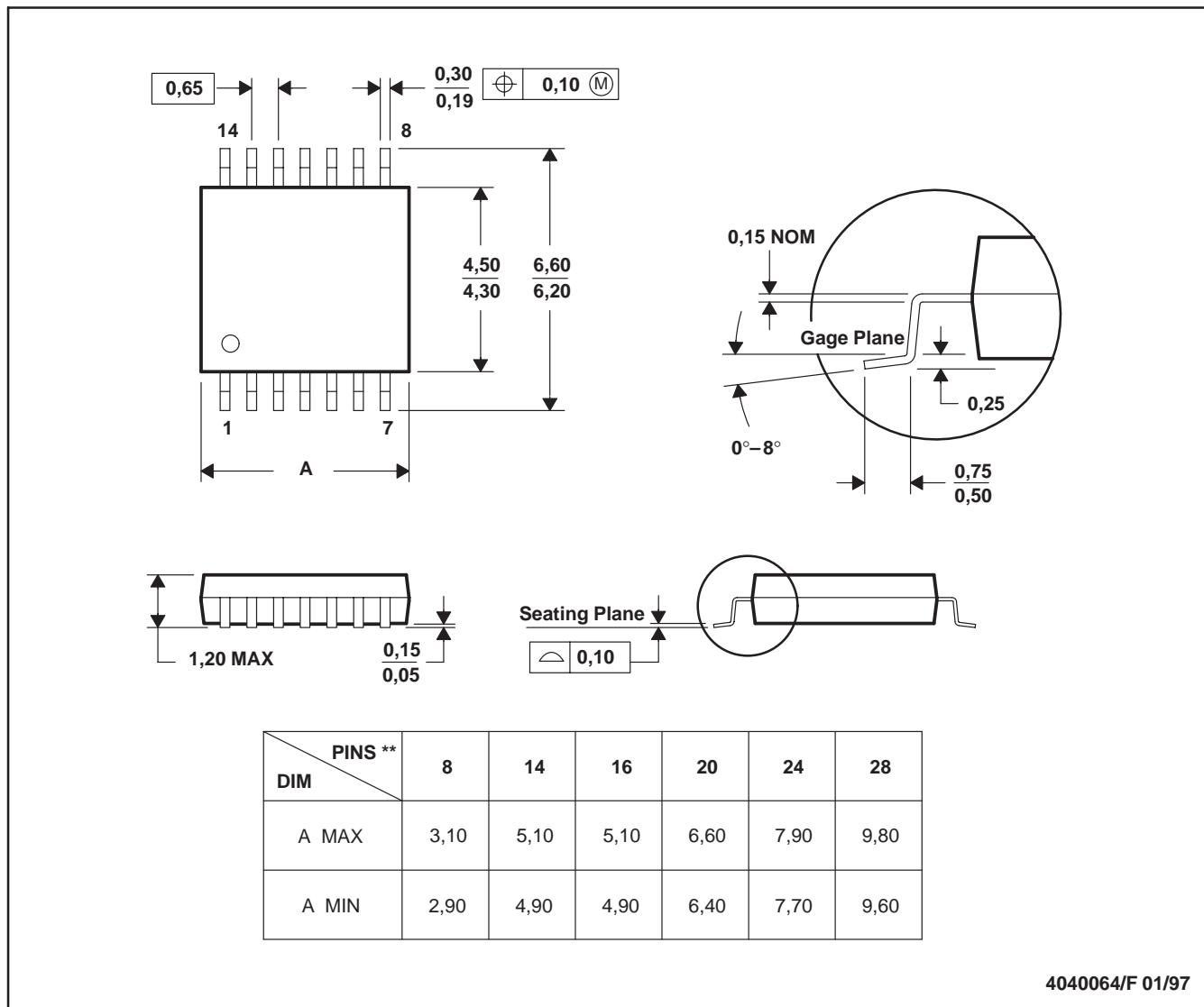
# MECHANICAL DATA

MTSS001C – JANUARY 1995 – REVISED FEBRUARY 1999

PW (R-PDSO-G\*\*)

14 PINS SHOWN

PLASTIC SMALL-OUTLINE PACKAGE



4040064/F 01/97

NOTES: A. All linear dimensions are in millimeters.  
 B. This drawing is subject to change without notice.  
 C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.  
 D. Falls within JEDEC MO-153

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RFID <a href="http://www.ti-rfid.com">www.ti-rfid.com</a>	Telephony <a href="http://www.ti.com/telephony">www.ti.com/telephony</a>
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