# LM2587 SIMPLE SWITCHER ${ }^{\circledR}$ 5A Flyback Regulator 

Check for Samples: LM2587

## FEATURES

- Requires Few External Components
- Family of Standard Inductors and Transformers
- NPN Output Switches 5.0A, can Stand Off 65V
- Wide Input Voltage Range: 4 V to 40 V
- Current-Mode Operation for Improved Transient Response, Line Regulation, and Current Limit
- 100 kHz Switching Frequency
- Internal Soft-Start Function Reduces In-Rush Current During Start-Up
- Output Transistor Protected by Current Limit, Under Voltage Lockout, and Thermal Shutdown
- System Output Voltage Tolerance of $\pm 4 \%$ Max Over Line and Load Conditions


## TYPICAL APPLICATIONS

- Flyback Regulator
- Multiple-Output Regulator
- Simple Boost Regulator
- Forward Converter


## DESCRIPTION

The LM2587 series of regulators are monolithic integrated circuits specifically designed for flyback, step-up (boost), and forward converter applications. The device is available in 4 different output voltage versions: $3.3 \mathrm{~V}, 5.0 \mathrm{~V}$, 12 V , and adjustable.
Requiring a minimum number of external components, these regulators are cost effective, and simple to use. Included in the datasheet are typical circuits of boost and flyback regulators. Also listed are selector guides for diodes and capacitors and a family of standard inductors and flyback transformers designed to work with these switching regulators.
The power switch is a 5.0A NPN device that can stand-off 65V. Protecting the power switch are current and thermal limiting circuits, and an undervoltage lockout circuit. This IC contains a 100 kHz fixedfrequency internal oscillator that permits the use of small magnetics. Other features include soft start mode to reduce in-rush current during start up, current mode control for improved rejection of input voltage and output load transients and cycle-by-cycle current limiting. An output voltage tolerance of $\pm 4 \%$, within specified input voltages and output load conditions, is ensured for the power supply system.

## Flyback Regulator



Figure 1.

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## Connection Diagrams



Figure 2. Bent, Staggered Leads 5-Lead TO-220 (NDH) Top View


Figure 4. 5-Lead TO-263 (KTT) Top View


Figure 3. Bent, Staggered Leads 5-Lead TO-220 (NDH) Side View


Figure 5. 5-Lead TO-263 (KTT) Side View


For Fixed Versions $3.3 \mathrm{~V}, \mathrm{R} 1=3.4 \mathrm{k}, \mathrm{R} 2=2 \mathrm{k} 5 \mathrm{~V}, \mathrm{R} 1=6.15 \mathrm{k}, \mathrm{R} 2=2 \mathrm{k} 12 \mathrm{~V}, \mathrm{R} 1=8.73 \mathrm{k}, \mathrm{R} 2=1 \mathrm{kFor}$ Adj. VersionR1 $=$ Short (0 $\Omega$ ), R2 $=$ Open

Figure 6. Block Diagram

## Test Circuits


$\mathrm{C}_{\mathrm{IN} 1}-100 \mu \mathrm{~F}, 25 \mathrm{~V}$ Aluminum Electrolytic $\mathrm{C}_{\mathrm{IN} 2}-0.1 \mu \mathrm{~F}$ CeramicT-22 $\mu \mathrm{H}, 1: 1$ Schott \#67141450D—1N5820Cout-680 $\mu \mathrm{F}, 16 \mathrm{~V}$ Aluminum Electrolytic $\mathrm{C}_{\mathrm{C}}-0.47 \mu \mathrm{~F}$ Ceramic $\mathrm{R}_{\mathrm{C}}-2 \mathrm{k}$

Figure 7. LM2587-3.3 and LM2587-5.0 Test Circuit

$\mathrm{C}_{\mathrm{IN} 1}-100 \mu \mathrm{~F}, 25 \mathrm{~V}$ Aluminum Electrolytic $\mathrm{C}_{\mathrm{IN} 2}-0.1 \mu \mathrm{~F}$ CeramicL-15 $\mu \mathrm{H}$, Renco \#RL-5472-5D-1N5820CouT-680 $\mu \mathrm{F}, 16 \mathrm{~V}$ Aluminum Electrolytic $\mathrm{C}_{\mathrm{C}}-0.47 \mu \mathrm{~F}$ Ceramic $\mathrm{R}_{\mathrm{C}}-2 \mathrm{kFor} 12 \mathrm{~V}$ Devices: $\mathrm{R}_{1}=$ Short ( $0 \Omega$ ) and $\mathrm{R}_{2}=$ Open For ADJ Devices: $\mathrm{R}_{1}=48.75 \mathrm{k}, \pm 0.1 \%$ and $\mathrm{R} 2=5.62 \mathrm{k}, \pm 1 \%$

Figure 8. LM2587-12 and LM2587-ADJ Test Circuit

## Flyback Regulator Operation

The LM2587 is ideally suited for use in the flyback regulator topology. The flyback regulator can produce a single output voltage, such as the one shown in Figure 9, or multiple output voltages. In Figure 9, the flyback regulator generates an output voltage that is inside the range of the input voltage. This feature is unique to flyback regulators and cannot be duplicated with buck or boost regulators.
The operation of a flyback regulator is as follows (refer to Figure 9): when the switch is on, current flows through the primary winding of the transformer, T1, storing energy in the magnetic field of the transformer. Note that the primary and secondary windings are out of phase, so no current flows through the secondary when current flows through the primary. When the switch turns off, the magnetic field collapses, reversing the voltage polarity of the primary and secondary windings. Now rectifier D1 is forward biased and current flows through it, releasing the energy stored in the transformer. This produces voltage at the output.
The output voltage is controlled by modulating the peak switch current. This is done by feeding back a portion of the output voltage to the error amp, which amplifies the difference between the feedback voltage and a 1.230 V reference. The error amp output voltage is compared to a ramp voltage proportional to the switch current (i.e., inductor current during the switch on time). The comparator terminates the switch on time when the two voltages are equal, thereby controlling the peak switch current to maintain a constant output voltage.


As shown in Figure 9, the LM2587 can be used as a flyback regulator by using a minimum number of external components. The switching waveforms of this regulator are shown in Figure 22. Typical Performance Characteristics observed during the operation of this circuit are shown in Figure 23.

Figure 9. 12V Flyback Regulator Design Example

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.
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## Absolute Maximum Ratings ${ }^{(1)(2)}$

| Input Voltage |  | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 45 \mathrm{~V}$ |
| :---: | :---: | :---: |
| Switch Voltage |  | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\text {SW }} \leq 65 \mathrm{~V}$ |
| Switch Current ${ }^{(3)}$ |  | Internally Limited |
| Compensation Pin Voltage |  | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\text {COMP }} \leq 2.4 \mathrm{~V}$ |
| Feedback Pin Voltage |  | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{FB}} \leq 2 \mathrm{~V}_{\mathrm{OUT}}$ |
| Storage Temperature Range |  | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature | (Soldering, 10 sec.$)$ | $260^{\circ} \mathrm{C}$ |
| Maximum Junction | Temperature ${ }^{(4)}$ | $150^{\circ} \mathrm{C}$ |
| Power Dissipation ${ }^{(4)}$ |  | Internally Limited |
| Minimum ESD Rating | $(\mathrm{C}=100 \mathrm{pF}, \mathrm{R}=1.5 \mathrm{k} \Omega)$ | 2 kV |

(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating ratings indicate conditions the device is intended to be functional, but device parameter specifications may not be ensured under these conditions. For ensured specifications and test conditions, see the Electrical Characteristics.
(2) If Military/Aerospace specified devices are required, please contact the TI Sales Office/ Distributors for availability and specifications.
(3) Note that switch current and output current are not identical in a step-up regulator. Output current cannot be internally limited when the LM2587 is used as a step-up regulator. To prevent damage to the switch, the output current must be externally limited to 5A. However, output current is internally limited when the LM2587 is used as a flyback regulator (see the Application Hints section for more information).
(4) The junction temperature of the device $\left(T_{J}\right)$ is a function of the ambient temperature $\left(T_{A}\right)$, the junction-to-ambient thermal resistance $\left(\theta_{\mathrm{JA}}\right)$, and the power dissipation of the device ( $\mathrm{P}_{\mathrm{D}}$ ). A thermal shutdown will occur if the temperature exceeds the maximum junction temperature of the device: $P_{D} \times \theta_{J A}+T_{A(M A X)} \geq T_{J(M A X)}$. For a safe thermal design, check that the maximum power dissipated by the device is less than: $P_{D} \leq\left[T_{J(M A X)}-T_{A(M A X)}\right] / \theta_{J A}$. When calculating the maximum allowable power dissipation, derate the maximum junction temperature-this ensures a margin of safety in the thermal design.

## Operating Ratings

| Supply Voltage | $4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 40 \mathrm{~V}$ |
| :--- | ---: |
| Output Switch Voltage | $0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{SW}} \leq 60 \mathrm{~V}$ |
| Output Switch Current | $\mathrm{I}_{\mathrm{SW}} \leq 5.0 \mathrm{~A}$ |
| Junction Temperature Range | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{J}} \leq+125^{\circ} \mathrm{C}$ |

## LM2587-3.3 Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathbb{I}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure ${ }^{(1)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {OUT }}$ | Output Voltage | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=400 \mathrm{~mA} \text { to } 1.75 \mathrm{~A} \end{aligned}$ | 3.3 | 3.17/3.14 | 3.43/3.46 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ $\Delta V_{I N}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=400 \mathrm{~mA} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\Delta \mathrm{V}_{\text {OUT }} /$ $\Delta \mathrm{I}_{\text {LOAD }}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{LOAD}}=400 \mathrm{~mA} \text { to } 1.75 \mathrm{~A} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 75 |  |  | \% |
| UNIQUE DEVICE PARAMETERS ${ }^{(2)}$ |  |  |  |  |  |  |
| $V_{\text {REF }}$ | Output Reference <br> Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 3.3 | 3.242/3.234 | 3.358/3.366 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 V | 2.0 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp Transconductance | $\begin{aligned} & \mathrm{I}_{\text {COMP }}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V} \end{aligned}$ | 1.193 | 0.678 | 2.259 | mmho |
| Avol | Error Amp Voltage Gain | $\begin{aligned} & \mathrm{V}_{\text {COMP }}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega^{(3)} \end{aligned}$ | 260 | 151/75 |  | V/V |

(1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2587 is used as shown in Figure 7 and Figure 8, system performance will be as specified by the system parameters.
(2) All room temperature limits are $100 \%$ production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
(3) A $1.0 \mathrm{M} \Omega$ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring $A_{V o l}$.

## LM2587-5.0 Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathbb{I N}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure $7^{(1)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {OUT }}$ | Output Voltage | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{LOAD}}=500 \mathrm{~mA} \text { to } 1.45 \mathrm{~A} \end{aligned}$ | 5.0 | 4.80/4.75 | 5.20/5.25 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ $\Delta V_{I N}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=500 \mathrm{~mA} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\begin{aligned} & \Delta \mathrm{V}_{\text {OUT/ }} \\ & \Delta I_{\text {LOAD }} \end{aligned}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=500 \mathrm{~mA} \text { to } 1.45 \mathrm{~A} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=750 \mathrm{~mA}$ | 80 |  |  | \% |
| UNIQUE DEVICE PARAMETERS ${ }^{(2)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Output Reference Voltage | Measured at Feedback Pin <br> $\mathrm{V}_{\text {COMP }}=1.0 \mathrm{~V}$ | 5.0 | 4.913/4.900 | 5.088/5.100 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V}$ to 40 V | 3.3 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp Transconductance | $\begin{aligned} & \mathrm{I}_{\text {COMP }}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{COMP}}=1.0 \mathrm{~V} \end{aligned}$ | 0.750 | 0.447 | 1.491 | mmho |
| Avol | Error Amp Voltage Gain | $\begin{aligned} & \mathrm{V}_{\text {COMP }}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega^{(3)} \end{aligned}$ | 165 | 99/49 |  | V/V |

(1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2587 is used as shown in Figure 7 and Figure 8, system performance will be as specified by the system parameters.
(2) All room temperature limits are $100 \%$ production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
(3) A $1.0 \mathrm{M} \Omega$ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring $A_{V o l}$.

## LM2587-12 Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure 8 ${ }^{(1)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {OUT }}$ | Output Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 12.0 | 11.52/11.40 | 12.48/12.60 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ $\Delta V_{\text {IN }}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \\ & \hline \end{aligned}$ | 20 |  | 100/200 | mV |
| $\Delta \mathrm{V}_{\text {OUT }} /$ $\Delta \mathrm{I}_{\text {LOAD }}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 90 |  |  | \% |
| UNIQUE DEVICE PARAMETERS ${ }^{(2)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Output Reference <br> Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 12.0 | 11.79/11.76 | 12.21/12.24 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 | 7.8 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp Transconductance | $\begin{aligned} & \mathrm{I}_{\text {COMP }}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V} \end{aligned}$ | 0.328 | 0.186 | 0.621 | mmho |
| Avol | Error Amp Voltage Gain | $\begin{aligned} & \mathrm{V}_{\text {COMP }}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\text {COMP }}=1.0 \mathrm{M} \Omega^{(3)} \end{aligned}$ | 70 | 41/21 |  | V/V |

(1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2587 is used as shown in Figure 7 and Figure 8, system performance will be as specified by the system parameters.
(2) All room temperature limits are 100\% production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
(3) A $1.0 \mathrm{M} \Omega$ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring $\mathrm{A}_{\text {vol }}$.

## LM2587-ADJ Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathbb{I N}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure $8^{(1)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {OUT }}$ | Output Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 12.0 | 11.52/11.40 | 12.48/12.60 | V |
| $\begin{aligned} & \Delta \mathrm{V}_{\text {OUT } / ~} \\ & \Delta \mathrm{~V}_{\text {IN }} \end{aligned}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\begin{aligned} & \Delta \mathrm{V}_{\text {OUT }} \\ & \left.\Delta\right\|_{\text {LOAD }} \end{aligned}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\text {IN }}=10 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 90 |  |  | \% |
| UNIQUE DEVICE PARAMETERS ${ }^{(2)}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Output Reference Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 1.230 | 1.208/1.205 | 1.252/1.255 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 V | 1.5 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp <br> Transconductance | $\begin{aligned} & \mathrm{I}_{\text {COMP }}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V} \end{aligned}$ | 3.200 | 1.800 | 6.000 | mmho |
| AvoL | Error Amp Voltage Gain | $\begin{aligned} & \mathrm{V}_{\text {COMP }}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega^{(3)} \end{aligned}$ | 670 | 400/200 |  | V/V |
| $\mathrm{I}_{B}$ | Error Amp Input Bias Current | $\mathrm{V}_{\text {COMP }}=1.0 \mathrm{~V}$ | 125 |  | 425/600 | nA |

(1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2587 is used as shown in Figure 7 and Figure 8, system performance will be as specified by the system parameters.
(2) All room temperature limits are $100 \%$ production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
(3) A $1.0 \mathrm{M} \Omega$ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring $\mathrm{A}_{\mathrm{vol}}$.

## All Output Voltage Versions Electrical Characteristics ${ }^{(1)}$

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Is | Input Supply Current | $\begin{aligned} & \text { (Switch Off) } \\ & \text { See } \end{aligned}$ | 11 |  | 15.5/16.5 | mA |
|  |  | $\mathrm{I}_{\text {SWITCH }}=3.0 \mathrm{~A}$ | 85 |  | 140/165 | mA |
| Vuv | Input Supply Undervoltage Lockout | $\mathrm{R}_{\text {LOAD }}=100 \Omega$ | 3.30 | 3.05 | 3.75 | V |
| $f_{0}$ | Oscillator Frequency | Measured at Switch Pin <br> $R_{\text {LOAD }}=100 \Omega$ <br> $\mathrm{V}_{\text {COMP }}=1.0 \mathrm{~V}$ | 100 | 85/75 | 115/125 | kHz |
| $\mathrm{f}_{\text {SC }}$ | Short-Circuit Frequency | Measured at Switch Pin <br> $R_{\text {LOAD }}=100 \Omega$ <br> $\mathrm{V}_{\text {FEEDBACK }}=1.15 \mathrm{~V}$ | 25 |  |  | kHz |
| $\mathrm{V}_{\text {EAO }}$ | Error Amplifier Output Swing | $\begin{array}{\|l\|} \hline \text { Upper Limit } \\ \text { See }^{(3)} \end{array}$ | 2.8 | 2.6/2.4 |  | V |
|  |  | $\begin{aligned} & \text { Lower Limit } \\ & \text { See }^{(2)} \end{aligned}$ | 0.25 |  | 0.40/0.55 | V |
| $\mathrm{I}_{\text {eao }}$ | Error Amp Output Current (Source or Sink) | See ${ }^{(4)}$ | 165 | 110/70 | 260/320 | $\mu \mathrm{A}$ |

(1) All room temperature limits are $100 \%$ production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
(2) To measure this parameter, the feedback voltage is set to a high value, depending on the output version of the device, to force the error amplifier output low. Adj: $\mathrm{V}_{\mathrm{FB}}=1.41 \mathrm{~V} ; 3.3 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=3.80 \mathrm{~V} ; 5.0 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=5.75 \mathrm{~V} ; 12 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=13.80 \mathrm{~V}$.
(3) To measure this parameter, the feedback voltage is set to a low value, depending on the output version of the device, to force the error amplifier output high. Adj: $\mathrm{V}_{\mathrm{FB}}=1.05 \mathrm{~V} ; 3.3 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=2.81 \mathrm{~V} ; 5.0 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=4.25 \mathrm{~V} ; 12 \mathrm{~V}: \mathrm{V}_{\mathrm{FB}}=10.20 \mathrm{~V}$.
(4) To measure the worst-case error amplifier output current, the LM2587 is tested with the feedback voltage set to its low value (specified in Note 7) and at its high value (specified in Note 8).

## All Output Voltage Versions Electrical Characteristics ${ }^{(1)}$ (continued)

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathbb{I N}}=5 \mathrm{~V}$.

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iss | Soft Start Current | $\begin{aligned} & \mathrm{V}_{\text {FEEDBACK }}=0.92 \mathrm{~V} \\ & \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V} \\ & \hline \end{aligned}$ | 11.0 | 8.0/7.0 | 17.0/19.0 | $\mu \mathrm{A}$ |
| D | Maximum Duty Cycle | $\begin{aligned} & \mathrm{R}_{\mathrm{LOAR}}=100 \Omega \\ & \mathrm{See}^{(3)} \end{aligned}$ | 98 | 93/90 |  | \% |
| $\mathrm{I}_{\mathrm{L}}$ | Switch Leakage Current | Switch Off $\mathrm{V}_{\text {SWITCH }}=60 \mathrm{~V}$ | 15 |  | 300/600 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {Sus }}$ | Switch Sustaining Voltage | $\mathrm{dV} / \mathrm{dT}=1.5 \mathrm{~V} / \mathrm{ns}$ |  | 65 |  | V |
| $\mathrm{V}_{\text {SAT }}$ | Switch Saturation Voltage | $\mathrm{I}_{\text {SWITCH }}=5.0 \mathrm{~A}$ | 0.7 |  | 1.1/1.4 | V |
| ICL | NPN Switch Current Limit |  | 6.5 | 5.0 | 9.5 | A |
| COMMON DEVICE PARAMETERS ${ }^{(5)}$ |  |  |  |  |  |  |
| $\theta_{\mathrm{JA}}$$\theta_{\mathrm{JA}}$$\theta_{\mathrm{JC}}$$\theta_{\text {JA }}$$\theta_{\mathrm{JA}}$$\theta_{\mathrm{JA}}$$\theta_{\mathrm{JC}}$ | Thermal Resistance | NDH Package, Junction to Ambient ${ }^{(6)}$ NDH Package, Junction to Ambient ${ }^{(7)}$ NDH Package, Junction to Case | $\begin{gathered} 65 \\ 45 \\ 25 \end{gathered}$ |  |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  | KTT Package, Junction to Ambient ${ }^{(8)}$ KTT Package, Junction to Ambient ${ }^{(9)}$ KTT Package, Junction to Ambient ${ }^{(10)}$ KTT Package, Junction to Case | $\begin{gathered} 56 \\ 35 \\ 26 \\ 2 \end{gathered}$ |  |  |  |

(5) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2587 is used as shown in Figure 7 and Figure 8, system performance will be as specified by the system parameters.
(6) Junction to ambient thermal resistance (no external heat sink) for the 5 lead TO-220 package mounted vertically, with $1 / 2$ inch leads in a socket, or on a PC board with minimum copper area.
(7) Junction to ambient thermal resistance (no external heat sink) for the 5 lead TO-220 package mounted vertically, with $1 / 2$ inch leads soldered to a PC board containing approximately 4 square inches of (1oz.) copper area surrounding the leads.
(8) Junction to ambient thermal resistance for the 5 lead TO-263 mounted horizontally against a PC board area of 0.136 square inches (the same size as the TO-263 package) of 1 oz . ( 0.0014 in . thick) copper.
(9) Junction to ambient thermal resistance for the 5 lead TO-263 mounted horizontally against a PC board area of 0.4896 square inches ( 3.6 times the area of the TO-263 package) of 1 oz . ( 0.0014 in . thick) copper.
(10) Junction to ambient thermal resistance for the 5 lead TO-263 mounted horizontally against a PC board copper area of 1.0064 square inches ( 7.4 times the area of the TO-263 package) of 1 oz . ( 0.0014 in . thick) copper. Additional copper area will reduce thermal resistance further. See the thermal model in Switchers Made Simple ${ }^{\circledR}$ software.
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Typical Performance Characteristics


Figure 10.


Figure 12.


Figure 14.


Figure 11.

Supply Current vs Switch Current


Figure 13.


Figure 15.

Typical Performance Characteristics (continued)

Switch Saturation


Figure 16.


Figure 18.


Figure 20.

Switch Transconductance
vs Temperature


Figure 17.


Figure 19.


Figure 21.

## Performance Characteristics

A


A: Switch Voltage, $10 \mathrm{~V} / \mathrm{divB}$ : Switch Current, $5 \mathrm{~A} / \mathrm{divC}$ : Output Rectifier Current, $5 \mathrm{~A} / \mathrm{divD}$ : Output Ripple Voltage, $100 \mathrm{mV} / \mathrm{div}$ AC-Coupled Horizontal: $\mathbf{2 \mu s} /$ div

Figure 22. Switching Waveforms


Figure 23. $\mathrm{V}_{\text {out }}$ Load Current Step Response

## TYPICAL FLYBACK REGULATOR APPLICATIONS

Figure 24 Figure 25 Figure 26 Figure 27 Figure 28 show six typical flyback applications, varying from single output to triple output. Each drawing contains the part number(s) and manufacturer(s) for every component except the transformer. For the transformer part numbers and manufacturers names, see the table in TRANSFORMER SELECTION (T). For applications with different output voltages-requiring the LM2587ADJ—or different output configurations that do not match the standard configurations, refer to the Switchers Made Simple software.


Figure 24. Single-Output Flyback Regulator


Figure 25. Single-Output Flyback Regulator


Figure 26. Single-Output Flyback Regulator


Figure 27. Dual-Output Flyback Regulator


Figure 28. Dual-Output Flyback Regulator


Figure 29. Triple-Output Flyback Regulator

## TRANSFORMER SELECTION (T)

Table 1 lists the standard transformers available for flyback regulator applications. Included in the table are the turns ratio(s) for each transformer, as well as the output voltages, input voltage ranges, and the maximum load currents for each circuit.

Table 1. Transformer Selection Table

| Applications | Figure 24 | Figure 25 | Figure 26 | Figure 27 | Figure 28 | Figure 29 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Transformers | T1 | T1 | T1 | T2 | T3 | T4 |
| $\mathrm{V}_{\text {IN }}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $8 \mathrm{~V}-16 \mathrm{~V}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $18 \mathrm{~V}-36 \mathrm{~V}$ | $18 \mathrm{~V}-36 \mathrm{~V}$ |
| $\mathrm{~V}_{\text {OUT1 }}$ | 3.3 V | 5 V | 12 V | 12 V | 12 V | 5 V |
| $\mathrm{l}_{\text {OUT1 }}$ (Max) | 1.8 A | 1.4 A | 1.2 A | 0.3 A | 1 A | 2.5 A |
| $\mathrm{~N}_{1}$ | 1 | 1 | 1 | 2.5 | 0.8 | 0.35 |
| $\mathrm{~V}_{\text {OUT2 }}$ |  |  |  | -12 V | -12 V | 12 V |
| $\mathrm{l}_{\text {OUT2 }}$ (Max) |  |  |  | 0.3 A | 1 A | 0.5 A |
| $\mathrm{~N}_{2}$ |  |  |  | 2.5 | 0.8 | 0.8 |
| $\mathrm{~V}_{\text {OUT3 }}$ |  |  |  |  |  | -12 V |
| lout3 (Max) |  |  |  |  |  | 0.5 A |
| $\mathrm{~N}_{3}$ |  |  |  |  | 0.8 |  |

Table 2. Transformer Manufacturer Guide

| Transformer <br> Type | Manufacturers' Part Numbers |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Coilcraft $^{(\mathbf{1 )}}$ | Coilcraft $^{(1)}$ | Pulse $^{(2)}$ | Renco $^{(3)}$ | Schott $^{(4)}$ |
|  |  | Surface Mount | Surface Mount |  |  |
| T1 | Q4434-B | Q4435-B | PE-68411 | RL-5530 | 67141450 |
| T2 | Q4337-B | Q4436-B | PE-68412 | RL-5531 | 67140860 |
| T3 | Q4343-B | - | PE-68421 | RL-5534 | 67140920 |

[^1]Table 2. Transformer Manufacturer Guide (continued)

| Transformer <br> Type | Manufacturers' Part Numbers |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Coilcraft $^{(1)}$ | Coilcraft $^{(1)}$ | Pulse $^{(2)}$ | Renco $^{(3)}$ | Schott $^{(4)}$ |
|  |  | Surface Mount | Surface Mount |  |  |
| T4 | Q4344-B | - | PE-68422 | RL-5535 | 67140930 |

## TRANSFORMER FOOTPRINTS

Figure 30, Figure 31, Figure 32, Figure 33, Figure 34, Figure 35, Figure 36, Figure 37, Figure 38 Figure 39, Figure 40, Figure 41, Figure 42, Figure 43, Figure 44, Figure 45, Figure 46, and Figure 47 show the footprints of each transformer, listed in Table 1.


Figure 30. Coilcraft Q4434-B (Top View)


Figure 32. Coilcraft Q4343-B (Top View)


Figure 34. Coilcraft Q4435-B (Surface Mount) (Top View)

T1


Figure 36. Pulse PE-68411 (Surface Mount) (Top View)


Figure 31. Coilcraft Q4337-B (Top View)


Figure 33. Coilcraft Q4344-B (Top View)


Figure 35. Coilcraft Q4436-B (Surface Mount) (Top View)


Figure 37. Pulse PE-68412 (Surface Mount) (Top View)


Figure 38. Pulse PE-68421 (Surface Mount) (Top View)

T1


Figure 40. Renco RL-5530 (Top View)


Figure 42. Renco RL-5534 (Top View)


Figure 44. Schott 67141450 (Top View)


Figure 46. Schott 67140920 (Top View)


Figure 39. Pulse PE-68422 (Surface Mount) (Top View)

T2


Figure 41. Renco RL-5531 (Top View)


Figure 43. Renco RL-5535 (Top View)


Figure 45. Schott 67140860 (Top View)


Figure 47. Schott 67140930 (Top View)

## Step-Up (Boost) Regulator Operation

Figure 48 shows the LM2587 used as a step-up (boost) regulator. This is a switching regulator that produces an output voltage greater than the input supply voltage.

A brief explanation of how the LM2587 Boost Regulator works is as follows (refer to Figure 48). When the NPN switch turns on, the inductor current ramps up at the rate of $\mathrm{V}_{\mathbb{I}} / \mathrm{L}$, storing energy in the inductor. When the switch turns off, the lower end of the inductor flies above $\mathrm{V}_{\mathbb{I N}}$, discharging its current through diode ( D ) into the output capacitor ( $\mathrm{C}_{\text {OUT }}$ ) at a rate of $\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}\right) / \mathrm{L}$. Thus, energy stored in the inductor during the switch on time is transferred to the output during the switch off time. The output voltage is controlled by adjusting the peak switch current, as described in the Flyback Regulator Operation section.


By adding a small number of external components (as shown in Figure 48), the LM2587 can be used to produce a regulated output voltage that is greater than the applied input voltage. The switching waveforms observed during the operation of this circuit are shown in Figure 49. Typical performance of this regulator is shown in Figure 50.

Figure 48. 12V Boost Regulator
Typical Performance Characteristics


A: Switch Voltage, 10 V/divB: Switch Current, 5 A/divC: Inductor Current, 5 A/divD: Output Ripple Voltage, $100 \mathrm{mV} / \mathrm{div}$, AC-Coupled
Horizontal: $2 \boldsymbol{\mu} /$ div
Figure 49. Switching Waveforms


Figure 50. $\mathrm{V}_{\text {out }}$ Response to Load Current Step

## Typical Boost Regulator Applications

Figure 51 and Figure 52 Figure 53 and Figure 54 show four typical boost applications)—one fixed and three using the adjustable version of the LM2587. Each drawing contains the part number(s) and manufacturer(s) for every component. For the fixed 12 V output application, the part numbers and manufacturers' names for the inductor are listed in a table in Figure 54. For applications with different output voltages, refer to the Switchers Made Simple software.


Figure 51. +5 V to $\mathbf{+ 1 2 V}$ Boost Regulator
Table 3 contains a table of standard inductors, by part number and corresponding manufacturer, for the fixed output regulator of Figure 51.

Table 3. Inductor Selection Table

| Coilcraft $^{(1)}$ | Pulse $^{(2)}$ | Renco $^{(3)}$ | Schott $^{(4)}$ |
| :---: | :---: | :---: | :---: |
| R4793-A | PE-53900 | RL-5472-5 | 67146520 |

(1) Coilcraft Inc.,: Phone: (800) 322-26451102 Silver Lake Road, Cary, IL 60013: Fax: (708) 639-1469
(2) Pulse Engineering Inc.,: Phone: (619) 674-810012220 World Trade Drive, San Diego, CA 92128: Fax: (619) 674-8262
(3) Renco Electronics Inc.,: Phone: (800) 645-582860 Jeffryn Blvd. East, Deer Park, NY 11729: Fax: (516) 586-5562
(4) Schott Corp.,: Phone: (612) 475-11731000 Parkers Lane Road, Wayzata, MN 55391: Fax: (612) 475-1786


Figure 52. $\mathbf{+ 1 2 V}$ to $\mathbf{+ 2 4 V}$ Boost Regulator


Figure 53. $\mathbf{+ 2 4 V}$ to $\mathbf{+ 3 6 V}$ Boost Regulator

*The LM2587 will require a heat sink in these applications. The size of the heat sink will depend on the maximum ambient temperature. To calculate the thermal resistance of the IC and the size of the heat sink needed, see the "Heat Sink/Thermal Considerations" section in Application Hints.

Figure 54. $\mathbf{+ 2 4 V}$ to $\mathbf{+ 4 8 V}$ Boost Regulator

## Application Hints



Figure 55. Boost Regulator

## PROGRAMMING OUTPUT VOLTAGE <br> (SELECTING $\mathbf{R}_{1}$ AND $\mathbf{R}_{2}$ )

Referring to the adjustable regulator in Figure 55, the output voltage is programmed by the resistors $R_{1}$ and $R_{2}$ by the following formula:
$V_{\text {OUT }}=V_{\text {REF }}\left(1+R_{1} / R_{2}\right) \quad$ where $V_{\text {REF }}=1.23 V$
Resistors $R_{1}$ and $R_{2}$ divide the output voltage down so that it can be compared with the 1.23 V internal reference. With $R_{2}$ between $1 k$ and $5 k, R_{1}$ is:

$$
\begin{equation*}
\mathrm{R}_{1}=\mathrm{R}_{2}\left(\mathrm{~V}_{\mathrm{OUT}} / \mathrm{V}_{\mathrm{REF}}-1\right) \quad \text { where } \mathrm{V}_{\mathrm{REF}}=1.23 \mathrm{~V} \tag{2}
\end{equation*}
$$

For best temperature coefficient and stability with time, use $1 \%$ metal film resistors.

## SHORT CIRCUIT CONDITION

Due to the inherent nature of boost regulators, when the output is shorted (see Figure 55), current flows directly from the input, through the inductor and the diode, to the output, bypassing the switch. The current limit of the switch does not limit the output current for the entire circuit. To protect the load and prevent damage to the switch, the current must be externally limited, either by the input supply or at the output with an external current limit circuit. The external limit should be set to the maximum switch current of the device, which is 5 A .
In a flyback regulator application (Figure 56), using the standard transformers, the LM2587 will survive a short circuit to the main output. When the output voltage drops to $80 \%$ of its nominal value, the frequency will drop to 25 kHz . With a lower frequency, off times are larger. With the longer off times, the transformer can release all of its stored energy before the switch turns back on. Hence, the switch turns on initially with zero current at its collector. In this condition, the switch current limit will limit the peak current, saving the device.
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## FLYBACK REGULATOR INPUT CAPACITORS

A flyback regulator draws discontinuous pulses of current from the input supply. Therefore, there are two input capacitors needed in a flyback regulator; one for energy storage and one for filtering (see Figure 56). Both are required due to the inherent operation of a flyback regulator. To keep a stable or constant voltage supply to the LM2587, a storage capacitor ( $\geq 100 \mu \mathrm{~F}$ ) is required. If the input source is a recitified DC supply and/or the application has a wide temperature range, the required rms current rating of the capacitor might be very large. This means a larger value of capacitance or a higher voltage rating will be needed of the input capacitor. The storage capacitor will also attenuate noise which may interfere with other circuits connected to the same input supply voltage.


Figure 56. Flyback Regulator
In addition, a small bypass capacitor is required due to the noise generated by the input current pulses. To eliminate the noise, insert a $1.0 \mu \mathrm{~F}$ ceramic capacitor between $\mathrm{V}_{\mathbb{I N}}$ and ground as close as possible to the device.

## SWITCH VOLTAGE LIMITS

In a flyback regulator, the maximum steady-state voltage appearing at the switch, when it is off, is set by the transformer turns ratio, N , the output voltage, $\mathrm{V}_{\mathrm{OUT}}$, and the maximum input voltage, $\mathrm{V}_{\mathrm{IN}_{\mathrm{N}}}(\mathrm{Max})$ :

$$
\begin{equation*}
\mathrm{V}_{\text {SW(OFF) }}=\mathrm{V}_{\mathbb{I N}}(\mathrm{Max})+\left(\mathrm{V}_{\text {OUT }}+\mathrm{V}_{F}\right) / \mathbb{N} \tag{3}
\end{equation*}
$$

where $\mathrm{V}_{\mathrm{F}}$ is the forward biased voltage of the output diode, and is 0.5 V for Schottky diodes and 0.8 V for ultra-fast recovery diodes (typically). In certain circuits, there exists a voltage spike, $\mathrm{V}_{\mathrm{LL}}$, superimposed on top of the steady-state voltage (see Figure 22, waveform A). Usually, this voltage spike is caused by the transformer leakage inductance and/or the output rectifier recovery time. To "clamp" the voltage at the switch from exceeding its maximum value, a transient suppressor in series with a diode is inserted across the transformer primary (as shown in the circuit on the front page and other flyback regulator circuits throughout the datasheet). The schematic in Figure 56 shows another method of clamping the switch voltage. A single voltage transient suppressor (the SA51A) is inserted at the switch pin. This method clamps the total voltage across the switch, not just the voltage across the primary.
If poor circuit layout techniques are used (see the CIRCUIT LAYOUT GUIDELINES section), negative voltage transients may appear on the Switch pin (pin 4). Applying a negative voltage (with respect to the IC's ground) to any monolithic IC pin causes erratic and unpredictable operation of that IC. This holds true for the LM2587 IC as well. When used in a flyback regulator, the voltage at the Switch pin (pin 4) can go negative when the switch turns on. The "ringing" voltage at the switch pin is caused by the output diode capacitance and the transformer leakage inductance forming a resonant circuit at the secondary(ies). The resonant circuit generates the "ringing" voltage, which gets reflected back through the transformer to the switch pin. There are two common methods to avoid this problem. One is to add an RC snubber around the output rectifier(s), as in Figure 56. The values of the resistor and the capacitor must be chosen so that the voltage at the Switch pin does not drop below -0.4 V . The resistor may range in value between $10 \Omega$ and $1 \mathrm{k} \Omega$, and the capacitor will vary from $0.001 \mu \mathrm{~F}$ to $0.1 \mu \mathrm{~F}$. Adding a snubber will (slightly) reduce the efficiency of the overall circuit.

The other method to reduce or eliminate the "ringing" is to insert a Schottky diode clamp between pins 4 and 3 (ground), also shown in Figure 56. This prevents the voltage at pin 4 from dropping below -0.4 V . The reverse voltage rating of the diode must be greater than the switch off voltage.


Figure 57. Input Line Filter

## OUTPUT VOLTAGE LIMITATIONS

The maximum output voltage of a boost regulator is the maximum switch voltage minus a diode drop. In a flyback regulator, the maximum output voltage is determined by the turns ratio, N , and the duty cycle, D , by the equation:

$$
\begin{equation*}
V_{\text {OUT }} \approx N \times V_{\mathbb{I N}} \times D /(1-D) \tag{4}
\end{equation*}
$$

The duty cycle of a flyback regulator is determined by the following equation:

$$
\begin{equation*}
D=\frac{V_{\text {OUT }}+V_{F}}{N\left(V_{\text {IN }}-V_{\text {SAT }}\right)+V_{\text {OUT }}+V_{F}} \approx \frac{V_{\text {OUT }}}{N\left(V_{\text {IN }}\right)+V_{\text {OUT }}} \tag{5}
\end{equation*}
$$

Theoretically, the maximum output voltage can be as large as desired-just keep increasing the turns ratio of the transformer. However, there exists some physical limitations that prevent the turns ratio, and thus the output voltage, from increasing to infinity. The physical limitations are capacitances and inductances in the LM2587 switch, the output diode(s), and the transformer-such as reverse recovery time of the output diode (mentioned above).

## NOISY INPUT LINE CONDITION)

A small, low-pass RC filter should be used at the input pin of the LM2587 if the input voltage has an unusual large amount of transient noise, such as with an input switch that bounces. The circuit in Figure 57 demonstrates the layout of the filter, with the capacitor placed from the input pin to ground and the resistor placed between the input supply and the input pin. Note that the values of $R_{I N}$ and $C_{I N}$ shown in the schematic are good enough for most applications, but some readjusting might be required for a particular application. If efficiency is a major concern, replace the resistor with a small inductor (say $10 \mu \mathrm{H}$ and rated at 100 mA ).

## STABILITY

All current-mode controlled regulators can suffer from an instability, known as subharmonic oscillation, if they operate with a duty cycle above $50 \%$. To eliminate subharmonic oscillations, a minimum value of inductance is required to ensure stability for all boost and flyback regulators. The minimum inductance is given by:

$$
\begin{equation*}
\mathrm{L}(\mathrm{Min})=\frac{2.92\left[\left(\mathrm{~V}_{\text {IN }}(\operatorname{Min})-\mathrm{V}_{\text {SAT }}\right) \times(2 \mathrm{D}(\mathrm{Max})-1)\right]}{1-\mathrm{D}(\mathrm{Max})}(\mu \mathrm{H}) \tag{6}
\end{equation*}
$$

where $\mathrm{V}_{\mathrm{SAT}}$ is the switch saturation voltage and can be found in the Characteristic Curves.


Figure 58. Circuit Board Layout

## CIRCUIT LAYOUT GUIDELINES

As in any switching regulator, layout is very important. Rapidly switching currents associated with wiring inductance generate voltage transients which can cause problems. For minimal inductance and ground loops, keep the length of the leads and traces as short as possible. Use single point grounding or ground plane construction for best results. Separate the signal grounds from the power grounds (as indicated in Figure 58). When using the Adjustable version, physically locate the programming resistors as near the regulator IC as possible, to keep the sensitive feedback wiring short.

## HEAT SINK/THERMAL CONSIDERATIONS

In many cases, no heat sink is required to keep the LM2587 junction temperature within the allowed operating range. For each application, to determine whether or not a heat sink will be required, the following must be identified:

1) Maximum ambient temperature (in the application).
2) Maximum regulator power dissipation (in the application).
3) Maximum allowed junction temperature $\left(125^{\circ} \mathrm{C}\right.$ for the LM2587). For a safe, conservative design, a temperature approximately $15^{\circ} \mathrm{C}$ cooler than the maximum junction temperature should be selected $\left(110^{\circ} \mathrm{C}\right)$.
4) LM2587 package thermal resistances $\theta_{\mathrm{JA}}$ and $\theta_{\mathrm{JC}}$ (given in the Electrical Characteristics).

Total power dissipated ( $\mathrm{P}_{\mathrm{D}}$ ) by the LM2587 can be estimated as follows:
Boost:

$$
P_{D}=0.15 \Omega \times\left(\frac{I_{L O A D}}{1-D}\right)^{2} \times D+\frac{I_{L O A D}}{50 \times(1-D)} \times D \times V_{I N}
$$

Flyback:

$$
\begin{align*}
\mathrm{P}_{\mathrm{D}}= & 0.15 \Omega \times\left(\frac{\mathrm{N} \times \Sigma \operatorname{l}_{\text {LOAD }}}{1-\mathrm{D}}\right)^{2} \times \mathrm{D} \\
& +\frac{N \times \Sigma I_{\text {LOAD }}}{50 \times(1-\mathrm{D})} \times \mathrm{D} \times \mathrm{V}_{I N} \tag{7}
\end{align*}
$$

$\mathrm{V}_{\text {IN }}$ is the minimum input voltage, $\mathrm{V}_{\text {OUT }}$ is the output voltage, N is the transformer turns ratio, D is the duty cycle, and $I_{\text {LOAD }}$ is the maximum load current (and $\sum I_{\text {LOAD }}$ is the sum of the maximum load currents for multiple-output flyback regulators). The duty cycle is given by:
Boost:

$$
D=\frac{V_{\text {OUT }}+V_{F}-V_{\text {IN }}}{V_{\text {OUT }}+V_{F}-V_{S A T}} \approx \frac{V_{\text {OUT }}-V_{\text {IN }}}{V_{\text {OUT }}}
$$

Flyback:

$$
\begin{equation*}
D=\frac{V_{\text {OUT }}+V_{F}}{N\left(V_{\text {IN }}-V_{S A T}\right)+V_{\text {OUT }}+V_{F}} \approx \frac{V_{\text {OUT }}}{N\left(V_{\text {IN }}\right)+V_{\text {OUT }}} \tag{8}
\end{equation*}
$$

where $\mathrm{V}_{\mathrm{F}}$ is the forward biased voltage of the diode and is typically 0.5 V for Schottky diodes and 0.8 V for fast recovery diodes. $\mathrm{V}_{\mathrm{SAT}}$ is the switch saturation voltage and can be found in the Characteristic Curves.
When no heat sink is used, the junction temperature rise is:

$$
\begin{equation*}
\Delta T_{J}=P_{D} \times \theta_{\mathrm{JA}} . \tag{9}
\end{equation*}
$$

Adding the junction temperature rise to the maximum ambient temperature gives the actual operating junction temperature:

$$
\begin{equation*}
\mathrm{T}_{\mathrm{J}}=\Delta \mathrm{T}_{\mathrm{J}}+\mathrm{T}_{\mathrm{A}} . \tag{10}
\end{equation*}
$$

If the operating junction temperature exceeds the maximum junction temperatue in item 3 above, then a heat sink is required. When using a heat sink, the junction temperature rise can be determined by the following:

$$
\begin{equation*}
\Delta T_{J}=P_{D} \times\left(\theta_{\mathrm{JC}}+\theta_{\text {Interface }}+\theta_{\text {Heat Sink }}\right) \tag{11}
\end{equation*}
$$

Again, the operating junction temperature will be:

$$
\begin{equation*}
\mathrm{T}_{J}=\Delta \mathrm{T}_{\mathrm{J}}+\mathrm{T}_{\mathrm{A}} \tag{12}
\end{equation*}
$$

As before, if the maximum junction temperature is exceeded, a larger heat sink is required (one that has a lower thermal resistance).
Included in the Switchers Made Simple design software is a more precise (non-linear) thermal model that can be used to determine junction temperature with different input-output parameters or different component values. It can also calculate the heat sink thermal resistance required to maintain the regulator junction temperature below the maximum operating temperature.
To further simplify the flyback regulator design procedure, TI is making available computer design software. Switchers Made Simple software is available on a ( $31 / 2^{\prime \prime}$ ) diskette for IBM compatible computers from a TI sales office in your area or the TI WEBENCH Design Center team.
http://www.ti.com/ww/en/analog/webench/index.shtml?DCMP=hpa_sva_webench\&HQS=webench-bb

## European Magnetic Vendor Contacts

Please contact the following addresses for details of local distributors or representatives:

## Coilcraft

## 21 Napier Place

Wardpark North Cumbernauld, Scotland G68 0LL Phone: +44 1236730595 Fax: +44 1236730627

## Pulse Engineering

## Dunmore Road

Tuam Co. Galway, Ireland Phone: +353 9324107 Fax: +353 9324459

## REVISION HISTORY

[^2] INSTRUMENTS
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## PACKAGING INFORMATION

| Orderable Device | Status (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead/Ball Finish <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM2587S-12/NOPB | ACTIVE | $\begin{array}{r} \text { DDPAK/ } \\ \text { TO-263 } \end{array}$ | KTT | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -12 P_{+} \end{aligned}$ | Samples |
| LM2587S-3.3/NOPB | ACTIVE | $\begin{array}{r} \text { DDPAK/ } \\ \text { TO-263 } \end{array}$ | KTT | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -3.3 \mathrm{P}_{+} \\ & \hline \end{aligned}$ | Samples |
| LM2587S-5.0 | NRND | $\begin{array}{r} \hline \text { DDPAK/ } \\ \text { TO-263 } \end{array}$ | KTT | 5 | 45 | TBD | Call TI | Call TI | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -5.0 \mathrm{P}_{+} \end{aligned}$ |  |
| LM2587S-5.0/NOPB | ACTIVE | $\begin{array}{r} \text { DDPAK/ } \\ \text { TO-263 } \\ \hline \end{array}$ | KTT | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -5.0 \mathrm{P}_{+} \\ & \hline \end{aligned}$ | Samples |
| LM2587S-ADJ | NRND | $\begin{array}{r} \text { DDPAK/ } \\ \text { TO-263 } \\ \hline \end{array}$ | KTT | 5 | 45 | TBD | Call TI | Call TI | -40 to 125 | LM2587S -ADJ P+ |  |
| LM2587S-ADJ/NOPB | ACTIVE | $\begin{aligned} & \text { DDPAK/ } \\ & \text { TO-263 } \end{aligned}$ | KTT | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & \text {-ADJ P+ } \end{aligned}$ | Samples |
| LM2587SX-12/NOPB | ACTIVE | $\begin{aligned} & \text { DDPAK/ } \\ & \text { TO-263 } \\ & \hline \end{aligned}$ | KTT | 5 | 500 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -12 P_{+} \\ & \hline \end{aligned}$ | Samples |
| LM2587SX-5.0/NOPB | ACTIVE | $\begin{gathered} \text { DDPAK/ } \\ \text { TO-263 } \end{gathered}$ | KTT | 5 | 500 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & -5.0 P_{+} \end{aligned}$ | Samples |
| LM2587SX-ADJ | NRND | $\begin{gathered} \text { DDPAK/ } \\ \text { TO-263 } \end{gathered}$ | KTT | 5 | 500 | TBD | Call TI | Call TI | -40 to 125 | LM2587S -ADJ P+ |  |
| LM2587SX-ADJ/NOPB | ACTIVE | $\begin{gathered} \text { DDPAK/ } \\ \text { TO-263 } \end{gathered}$ | KTT | 5 | 500 | Pb-Free (RoHS Exempt) | CU SN | Level-3-245C-168 HR | -40 to 125 | $\begin{aligned} & \text { LM2587S } \\ & \text {-ADJ P+ } \end{aligned}$ | Samples |
| LM2587T-12 | NRND | TO-220 | NDH | 5 |  | TBD | Call TI | Call TI | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & -12 \text { P+ }^{2} \end{aligned}$ |  |
| LM2587T-12/NOPB | ACTIVE | TO-220 | NDH | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-1-NA-UNLIM | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & -12 \mathrm{P}_{+} \\ & \hline \end{aligned}$ | Samples |
| LM2587T-3.3/NOPB | ACTIVE | TO-220 | NDH | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-1-NA-UNLIM | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & -3.3 \text { P+ } \end{aligned}$ | Samples |
| LM2587T-5.0/NOPB | ACTIVE | TO-220 | NDH | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-1-NA-UNLIM | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & -5.0 \mathrm{P}_{+} \end{aligned}$ | Samples |
| LM2587T-ADJ | NRND | TO-220 | NDH | 5 | 45 | TBD | Call TI | Call TI | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & \text {-ADJ P+ } \end{aligned}$ |  |
| LM2587T-ADJ/NOPB | ACTIVE | TO-220 | NDH | 5 | 45 | Pb-Free (RoHS Exempt) | CU SN | Level-1-NA-UNLIM | -40 to 125 | $\begin{aligned} & \text { LM2587T } \\ & \text {-ADJ P+ } \end{aligned}$ | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but Tl does not recommend using this part in a new design. PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device
${ }^{(2)}$ Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS \& no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.
TBD: The Pb-Free/Green conversion plan has not been defined
Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.
Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.
Green (RoHS \& no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed $0.1 \%$ by weight in homogeneous material)
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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## TAPE AND REEL INFORMATION



| *All dimensions are nominal |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> $\mathbf{W 1}(\mathbf{m m})$ | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | W <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| LM2587SX-12/NOPB | DDPAK/ <br> TO-263 | KTT | 5 | 500 | 330.0 | 24.4 | 10.75 | 14.85 | 5.0 | 16.0 | 24.0 | Q2 |
| LM2587SX-5.0/NOPB | DDPAK/ <br> TO-263 | KTT | 5 | 500 | 330.0 | 24.4 | 10.75 | 14.85 | 5.0 | 16.0 | 24.0 | Q2 |
| LM2587SX-ADJ | DDPAK/ <br> TO-263 | KTT | 5 | 500 | 330.0 | 24.4 | 10.75 | 14.85 | 5.0 | 16.0 | 24.0 | Q2 |
| LM2587SX-ADJ/NOPB | DDPAK/ <br> TO-263 | KTT | 5 | 500 | 330.0 | 24.4 | 10.75 | 14.85 | 5.0 | 16.0 | 24.0 | Q2 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM2587SX-12/NOPB | DDPAK/TO-263 | KTT | 5 | 500 | 367.0 | 367.0 | 45.0 |
| LM2587SX-5.0/NOPB | DDPAK/TO-263 | KTT | 5 | 500 | 367.0 | 367.0 | 45.0 |
| LM2587SX-ADJ | DDPAK/TO-263 | KTT | 5 | 500 | 367.0 | 367.0 | 45.0 |
| LM2587SX-ADJ/NOPB | DDPAK/TO-263 | KTT | 5 | 500 | 367.0 | 367.0 | 45.0 |

## NDH0005D




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[^2]:    - Changed layout of National Data Sheet to TI format24

