



## INTEGRATED PHOTO FLASH CHARGER AND IGBT DRIVER

### FEATURES

- Highly Integrated Solution to Reduce Components
- Integrated 50-V Power Switch,  $R_{(ON)} = 200\text{ m}\Omega$  Typical
- Integrated IGBT Driver
- High Efficiency
- Programmable Peak Current, 0.95 A ~ 1.8 A
- Input Voltage of 1.8 V to 12 V
- Optimized Control Loop for Fast Charge Time
- Sensing All Trigger From Primary Side
- 10-Pin MSOP/16-Pin QFN Package
- Protection
  - MAX On Time
  - Over  $V_{DS}$  Shutdown
  - Thermal Monitor

### APPLICATIONS

- Digital Still Cameras (DSC)
- Optical Film Cameras
- Mobile Phones With Camera
- PDAs With Camera

### DESCRIPTION

This device offers a complete solution for charging a photo flash capacitor from battery input, and subsequently discharging the capacitor to the xenon tube. The device has an integrated power switch, IGBT driver, and control logic blocks for charge applications. Compared with discrete solutions, the device significantly reduces the component count, shrinks the solution size, and eases design complexity. Additional advantages are fast charging time and high efficiency due to the optimized PWM control algorithm.

Other provisions of the device includes four options for determining a different target voltage, programmable peak current, thermal disable monitor, input signal for charge enable, flash enable, and an output signal for charge completion status.

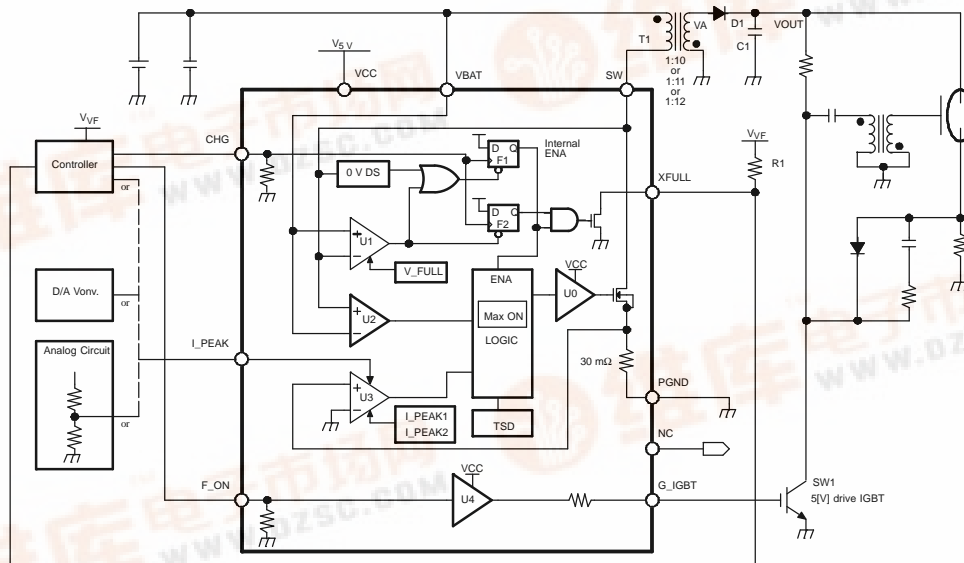


Figure 1. Typical Application Circuit

PRODUCT PREVIEW





These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### ORDERING INFORMATION

T <sub>A</sub>	TARGET VOLTAGE at PRIMARY SIDE	PACKAGE MARKING	PACKAGE	PART NUMBER
-35°C to 85°C	29	BKV	16-pin QFN	TPS65552ARGT
-35°C to 85°C	29	BMA	10-pin MSOP	TPS65552ADGQ

### ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted) <sup>(1)</sup>

		UNIT
V <sub>SS</sub>	Supply voltage	VCC
		VBAT
V <sub>(SW)</sub>	Switch terminal voltage	-0.6 V to 6 V
	Switch current between SW and PGND, ISW	-0.6 V to 13 V
		3 A
V <sub>I</sub>	Input voltage of CHG, I_PEAK, F_ON	-0.6 V to 50 V
T <sub>stg</sub>	Storage temperature	-0.3 V to V <sub>CC</sub>
T <sub>J</sub>	Maximum junction temperature	-40°C to 150°C
		125°C

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### RECOMMENDED OPERATING CONDITIONS

		MIN	NOM	MAX	UNIT
V <sub>SS</sub>	Supply voltage, VCC	4.5		5.5	V
	Supply voltage, VBAT	1.8		12	V
V <sub>(SW)</sub>	Switch terminal voltage,	-0.3		45	V
	Switch current between SW and PGND			2	A
	Operating free-air temperature range	-35		85	°C
V <sub>IH</sub>	High-level digital input voltage at CHG and F_ON	2.4			V
V <sub>IL</sub>	Low-level digital input voltage at CHG and F_ON			0.6	V

### DISSIPATION RATINGS

PACKAGE	R <sub>θJA</sub> <sup>(1)</sup>	POWER RATING T <sub>A</sub> < 25°C	POWER RATING T <sub>A</sub> = 70°C	POWER RATING T <sub>A</sub> = 85°C
MSOP	49.08 °C/W	2.04 W	1.12 W	815 mW
QFN	47.40 °C/W	2.11 W	1.16 W	844 mW

(1) The thermal resistance, R<sub>θJA</sub>, is based on a soldered PowerPAD™ on a 2S2P JEDEC board using thermal vias.

## ELECTRICAL CHARACTERISTICS

$T_A = 25^\circ\text{C}$ ,  $V_{BAT} = 4.2\text{ V}$ ,  $V_{CC} = 5\text{ V}$ ,  $V_{(SW)} = 4.2\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
$R_{(ONL)}$	ON resistance of XFULL		1.5	3	$k\Omega$	
$V_{(PKH)}^{(1)}$	Upper threshold voltage of I_PEAK	2.4			V	
$V_{(PKL)}^{(1)}$	Lower threshold voltage of I_PEAK			0.6	V	
$I_{CC1}$	Supply current from VBAT		27		$\mu\text{A}$	
$I_{CC2}$	Supply current from VCC		2.5	5	mA	
$I_{CC3}$	Supply current from VCC and VBAT			1	$\mu\text{A}$	
$I_{lk1}$	Leakage current of SW terminal			2	$\mu\text{A}$	
$I_{lk2}$	Leakage current of XFULL terminal	$V_{(XFULL)} = 5\text{ V}$		1	$\mu\text{A}$	
$R_{(ONSW)}$	SW ON resistance between SW and PGND	$I_{(SW)} = 1\text{ A}$	0.3	1	$\Omega$	
$R_{(IGBT1)}$	G_IGBT pullup resistance	$V_{(G\_IGBT)} = 0\text{ V}$	5	10	$\Omega$	
$R_{(IGBT2)}$	G_IGBT pulldown resistance	$V_{(G\_IGBT)} = 5\text{ V}$	25	51	$\Omega$	
$I_{(PEAK1)}$	Upper peak of $I_{(SW)}$	$V_{(L\_IPEAK)} = 3\text{ V}$	1.58	1.68	1.78	A
$I_{(PEAK2)}$	Lower peak of $I_{(SW)}$	$V_{(L\_IPEAK)} = 0\text{ V}$	0.77	0.87	0.97	A
$V_{(FULL)}$	Charge completion detect voltage at $V_{(SW)}$	TPS65552A	28.7	29	29.3	V
$V_{(ZERO)}$	Zero current detection at $V_{(SW)}$		1	20	60	mV
$T_{(SD)}^{(1)}$	Thermal shutdown temperature		150	160	170	$^\circ\text{C}$
	Over $V_{DS}$ detection at $V_{(SW)}$		0.95	1.2	1.45	V
$t_{MAX}$	MAX ON time		50	80	120	$\mu\text{s}$
$R_{(INPD)}$	Pulldown resistance of CHG, F_ON	$V_{CHG} = V_{(F\_ON)} = 4.2\text{ V}$		100		$k\Omega$

(1) Specified by design.

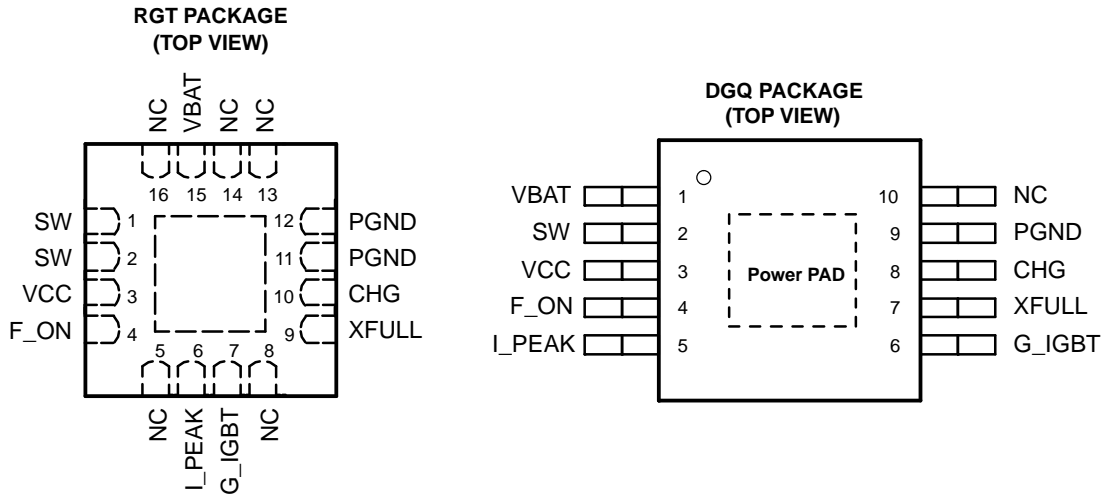
## SWITCHING CHARACTERISTICS

$T_A = 25^\circ\text{C}$ ,  $V_{BAT} = 4.2\text{ V}$ ,  $V_{CC} = 5\text{ V}$ ,  $V_{(SW)} = 4.2\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
$t_{PD}^{(1)}$	Propagation delay					
		$F\_ON\uparrow\downarrow - G\_IGBT\uparrow\downarrow$		50		ns
		SW ON after $V_{(SW)}$ dips from $V_{(ZERO)}$		45		ns
		SW OFF after $I_{(SW)}$ exceeds $I_{(PEAK)}$		270		ns
		XFULL $\downarrow$ after $V_{(SW)}$ exceeds $V_{(FULL)}$		300		ns
		SW ON after CHG $\uparrow$		20		ns
	SW OFF after CHG $\downarrow$		20		ns	

(1) Specified by design.

**PIN ASSIGNMENT**



NC – No internal connection

**TERMINAL FUNCTIONS**

PIN NUMBER		SIGNAL	I/O	DESCRIPTION
RGT	DGQ			
1, 2	2	SW	O	Primary side switch
3	3	VCC	I	Power supply voltage
4	4	F_ON	I	G_IGBT control input
5, 8, 13, 16	–	NC		No connection (internally open)
6	5	I_PEAK	I	Peak current control input
7	6	G_IGBT	O	IGBT gate driver output
9	7	XFULL	O	Charge completion output
10	8	CHG	I	Charge control input
11, 12	9	PGND		Power ground
14	10	NC		No connection (used by TI, should be open pin)
15	1	VBAT	I	Battery voltage input

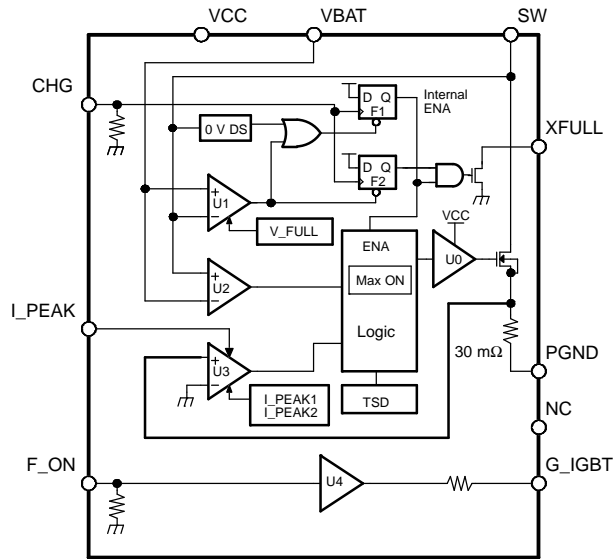


Figure 2. Functional Block Diagram

I/O Equivalent Circuits

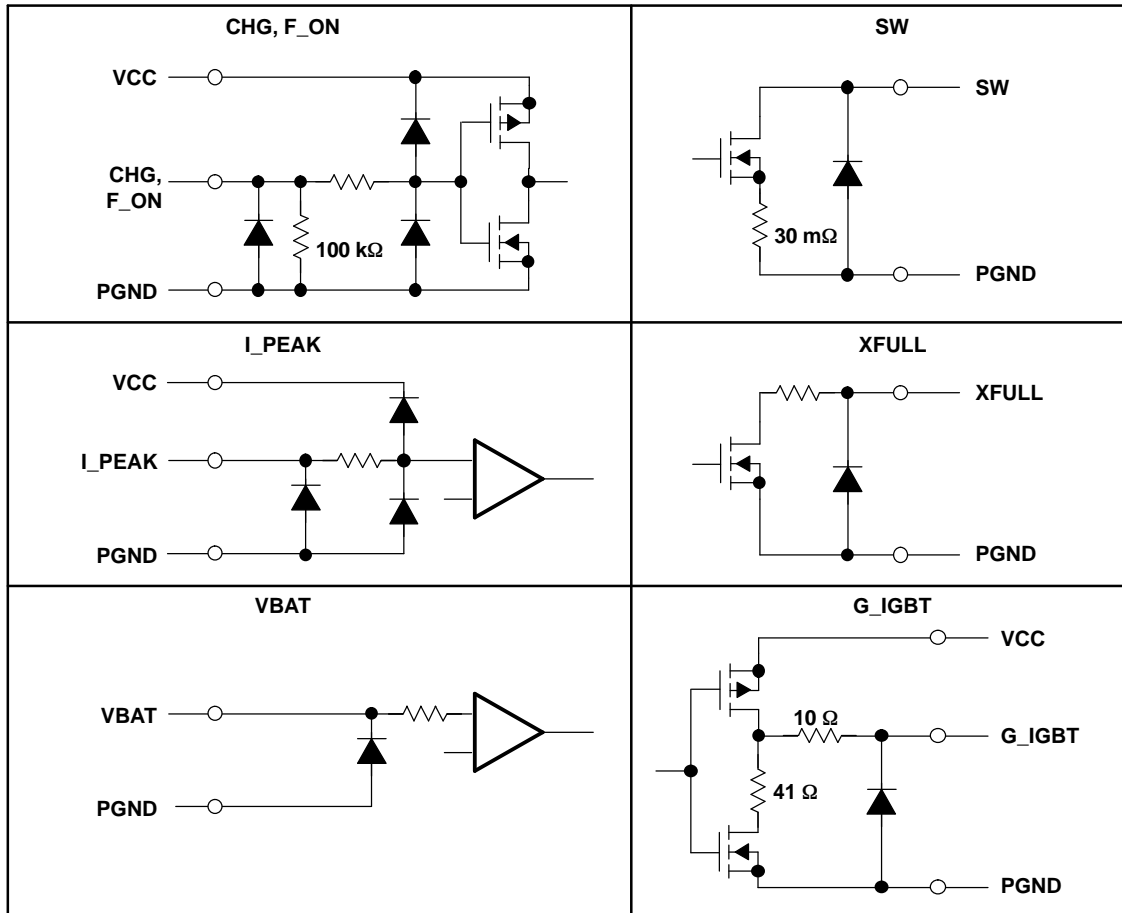


Figure 3. I/O Equivalent Circuits

## PRINCIPLES OF OPERATION

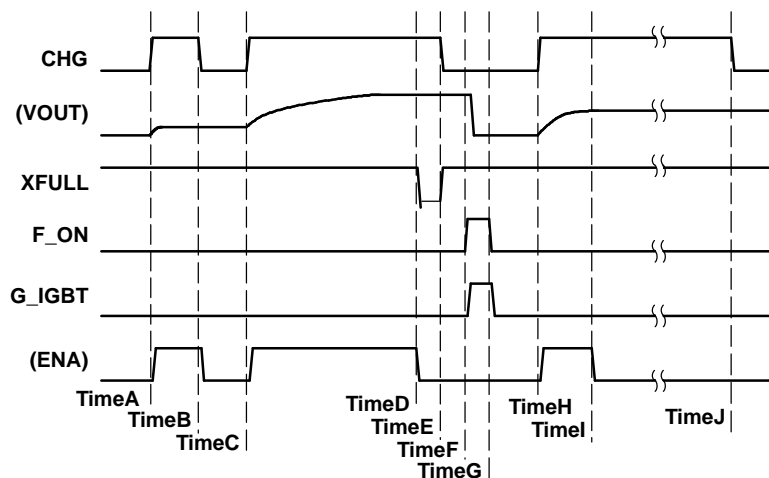


Figure 4. Whole Operation Sequence Chart

### Start/Stop Charging

TPS65552A has one internal enable latch, F1, that holds a charge (*ON/OFF* status) of the device. See Figure 2.

The only way to *start* charging is to input  $\text{CHG}\uparrow$  (see time A/C/H in Figure 4). Each time  $\text{CHG}\uparrow$  is reached, the TPS65552A starts charging.

There are three trigger events to *stop* charging:

1. Forced *stop* by inputting  $\text{CHG} = \text{L}$  from the controller (see timeB in Figure 4).
2. Automatic *stop* by detecting full charge.  $\text{VOUT}$  reaches the target value (see TimeD in Figure 4).
3. Protected *stop* by over  $V_{\text{DS}}$  detection (see TimeI in Figure 4).

### Indicate Charging Status

When the charging operation is completed, the TPS65552A drives the charge completion indicator pin, XFULL, to GND. XFULL is an open-drain type output. When connecting the indicator LED to XFULL, the LED lights are on when fully charged. The controller detects the status of the device as a logic signal when connecting a pullup resistor, R1 (see Figure 1).

XFULL enables the controller to detect the over  $V_{\text{DS}}$  protection status using software time. If over  $V_{\text{DS}}$  protection occurs, XFULL never goes L during  $\text{CHG} = \text{H}$ , provided that the timer that starts at  $\text{CHG}\uparrow$  stops at  $\text{XFULL}\uparrow$ , and times out within a designed period of maximum charging times. The controller can detect over  $V_{\text{DS}}$  at time out.

The device starts charging at *timeH*, and over  $V_{\text{DS}}$  protection occurs at TimeI (see Figure 4). At timeI, XFULL stays H, and the controller detects over  $V_{\text{DS}}$  protection when the timer ends at timeJ. In this event, the controller inputs  $\text{CHG} = \text{L}$  to terminate the operation.

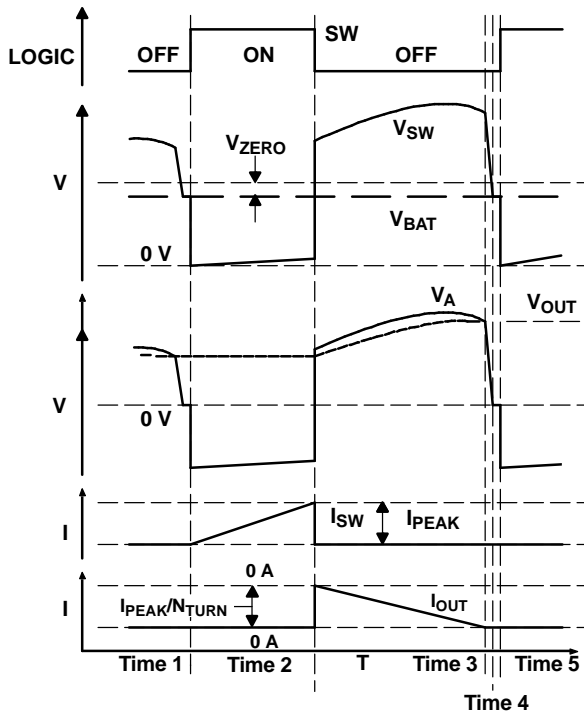


Figure 5. Timing Diagram at One Switching Cycle

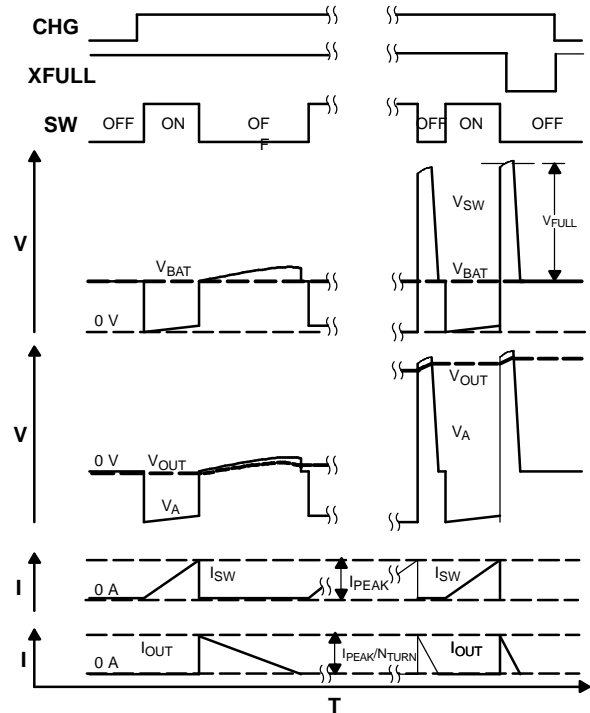


Figure 6. Timing Diagram at Beginning/Ending

## Control Charging

The TPS65552A provides three comparators to control charging. Figure 2 shows the block diagram of TPS65552A and Figure 5 shows one timing diagram switching cycle. Note that emphasis is placed on Time1 and Time3 of the waveform in Figure 5.

While SW is ON (Time1 to Time2 in Figure 5), U3 monitors current flow through integrated power-MOSFET from SW to PGND. When  $I_{(SW)}$  exceeds  $I_{(PEAK)}$ , SW turns OFF (Time2 in Figure 5).

When SW turns OFF (Time2 in Figure 5), the magnetic energy in the transformer starts discharging. Meanwhile, U2 monitors the kickback voltage at the SW terminal. As the energy is discharging, the kickback voltage is increasing according to the increase of  $V_{OUT}$  (Time2 to Time3 in Figure 5). When almost all energy is discharged, the system cannot continue rectification via the diode, and the charging current of  $I_{OUT}$  goes to zero (Times3 in Figure 5). After rectification stops, the small amount of energy left in the transformer is released via the parasitic path, and the kickback voltage reaches zero (Time3 to Time4 in Figure 5). During this period, U2 makes SW turn ON when  $(V_{(SW)} - V_{BAT})$  dips from  $V_{(ZERO)}$  (Time5 in Figure 5). In the actual circuit, the period between Time4 and Time5 in Figure 5 is small or does not appear dependent on the delay time of the U2 detection to SW ON.

U1 also monitors the kickback voltage. When  $(V_{(SW)} - V_{BAT})$  exceeds  $V_{(FULL)}$ , TPS65552A stops charging (see Figure 6).

In Figure 5 and Figure 6, ON time is always the same period in every switching. The ON time is calculated by Equation 1. This equation is not dependent on output voltage.

$$t_{ON} = L \frac{I_{PEAK}}{V_{BAT}} \quad (1)$$

However, OFF time is dependant on output voltage. As the output voltage gets higher, the OFF time gets shorter (see Equation 2).

$$t_{OFF} = N\_TURN \times L \frac{I_{PEAK}}{V_{OUT}} \tag{2}$$

### Reference Voltage

The TPS65552A does not have its own reference voltage circuit inside, and the TPS65552A uses the VCC input voltage as a reference to detect  $I_{(PEAK)}$ ,  $V_{(ZERO)}$ , and  $V_{(FULL)}$ . Therefore, voltage input at VCC is approximately 5 V.

VCC differs from 5 V by system limitations. [Table 1](#) shows the dependence of each function of TPS65552A to VCC.

**Table 1. VCC Dependence of TPS65552A**

PARAMETER		EQUATION	VCC		
			4.5	5	5.5
$I_{(PEAK1)}$		$0.52 \times VCC - 0.92$	1.42	1.68	1.94
$I_{(PEAK2)}$		$0.24 \times VCC - 0.33$	0.75	0.87	0.99
$V_{(FULL)}$	TPS65552A	$5.8 \times VCC$	26.1	29.0	31.9
	over $V_{DS}$	$0.24 \times VCC$	1.08	1.2	1.32

### Termination Voltage Setting

To obtain a different termination voltage, transformers of different turn ratio are required. [Table 2](#) shows the matrix of termination voltage and the turn ratio of the transformer. The table only shows a *ONE to integer* ratio while there are no limitations for a turn ratio of the transformer in a real application circuit, example 1:10.5 (= 10:105).

**Table 2. Termination Voltage Setting Table**

	TPS65552A
	29 [V]
1:10	290
1:11	319
1:12	348



## Programming Peak Current

The TPS65552A provides a method to program  $I_{(PEAK)}$  through the input voltage of the I\_PEAK terminal. [Figure 7](#) shows how to program  $I_{(PEAK)}$ .

I\_PEAK input is treated as a logic input, when its voltage is below  $V_{(PKL)}$  (0.6 V) and above  $V_{(PKH)}$  (2.4 V). Between  $V_{(PKL)}$  and  $V_{(PKH)}$ , I\_PEAK input is treated as an analog input. Using this characteristic,  $I_{(PEAK)}$  can be set by the logic signal or by an analog input.

Typical usages of this function are:

1. Charging  $I_{(PEAK)}$  depends on the battery voltage. Large  $I_{(PEAK)}$  for an adequate battery, small  $I_{(PEAK)}$  for a poor battery.
2. Reducing  $I_{(PEAK)}$  when zooming lens (motor works); this avoids shutdown of the battery with a large current output.

In [Figure 1](#), three optional connections to I\_PEAK are shown.

1. Use the controller to treat I\_PEAK as the logic input pin. This option is the easiest.
2. Use a D/A converter to force  $I_{(PEAK)}$  to follow analog information, such as battery voltage.
3. Use an analog circuit to achieve the same results as the D/A converter.

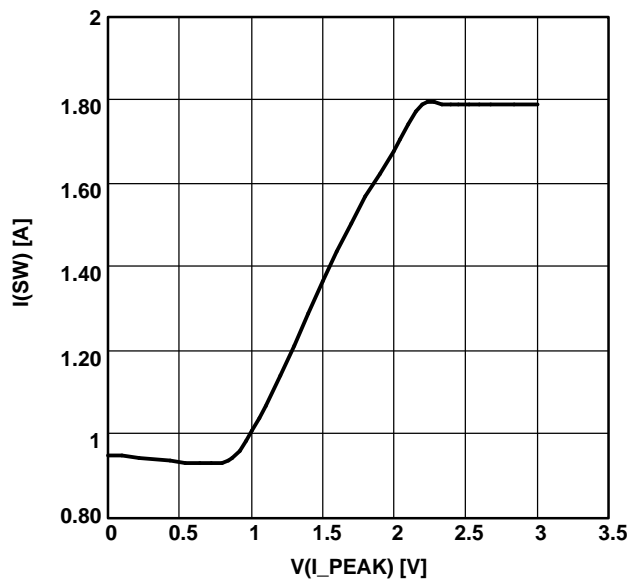


Figure 7. I\_PEAK vs  $I_{(sw)}$

## IGBT Driver Control

The IGBT driver provided by the TPS65552A is a simple buffer in the logical table. [Table 3](#) shows the function (see [Figure 4](#)).

Table 3. IGBT Driver Function Table

F_ON	G_IGBT
L	L
H	H

# TPS65552A

SLVS567–JULY 2005

## Protections

TPS65552A provides three protections: thermal shutdown, max on time, and overvoltage at power SW.

### Thermal Shutdown

When TPS65552A overheats, all functions stop. The only way to recover is to wait for the TPS65552A to cool down. This protection is not through *SHUTDOWN*, so the TPS65552A restarts charging if CHG stays H during the whole overheated period.

### MAX ON Time

To prevent a condition such as pulling current from a poor power source (i.e., an almost empty battery), the TPS65552A provides a maximum *ON* time protection. If the *ON* time exceeds  $t_{MAX}$ , the TPS555x is forced *OFF* regardless of  $I_{(PEAK)}$  detection.

### Overvoltage at Power SW

To avoid the stress of power dissipation, the TPS65552A provides an overvoltage monitor function at the SW terminal. If this protection occurs, the overvoltage status is latched (see [Figure 4](#) and its descriptions).

This function also protects short-circuit of the secondary side. In the short-circuit state of the secondary side, almost 100% of the battery voltage is supplied to SW, which stresses the device.

## PCB Information

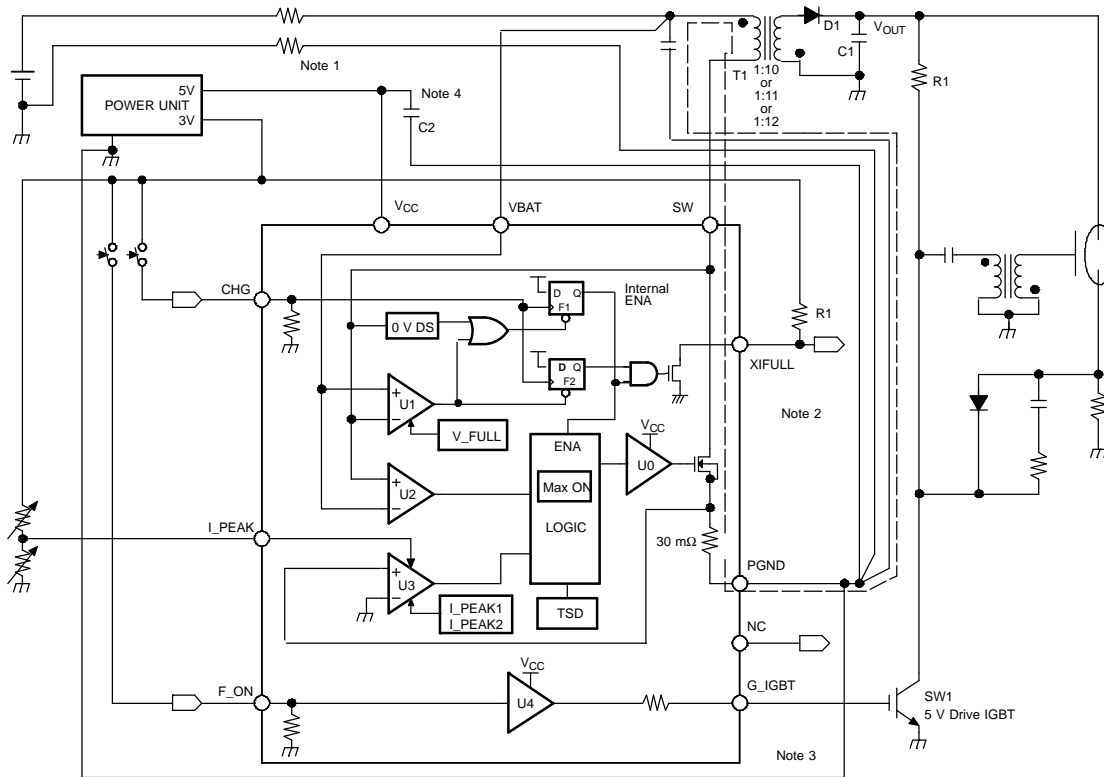


Figure 8. PCB Design Guideline

Figure 8 shows key points when designing a PCB.

1. In many DSC designs, parasitic resistance that cannot be ignored, exists on the power line path from the battery to the primary side turn of the transformer. The TPS65552A has one ground point connection inside the IC at the PGND PAD. So, the PCB layout should also keep a one-point ground connection at the PGND terminal of TPS65552A.
2. The loop indicated by dotted-lines is laid out as small as possible to reduce the open area of the loop.
3. The TPS65552A uses the VCC input as a reference voltage. Considering Note 1, the ground of the *power unit* that sources VCC is connected to PGND.
4. Regarding Note 3, the bypass capacitor, C2, is required to avoid grounding noise.

### Additional Technical Information

TI provides an application note for this device. For more technical information, please find the application note on the TI Web site or consult your sales contact. Literature number [SLVA197](#).

The application note provides the following information.

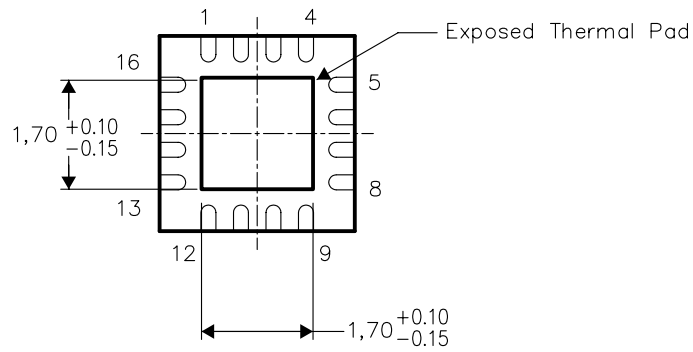
1. Recommended external parts
2. PCB layout
3. Detailed operation theory
4. Calculation of the efficiency
5. Key points to design your system

THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB), the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to a ground plane or special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, Quad Flatpack No-Lead Logic Packages, Texas Instruments Literature No. SCBA017. This document is available at [www.ti.com](http://www.ti.com).

The exposed thermal pad dimensions for this package are shown in the following illustration.



Bottom View

NOTE: All linear dimensions are in millimeters

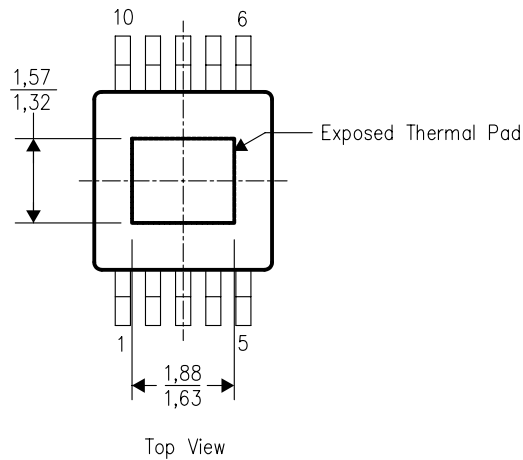
Exposed Thermal Pad Dimensions

THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. When the thermal pad is soldered directly to the printed circuit board (PCB), the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to a ground plane or special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at [www.ti.com](http://www.ti.com).

The exposed thermal pad dimensions for this package are shown in the following illustration.



NOTE: All linear dimensions are in millimeters

Exposed Thermal Pad Dimensions

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Interface	<a href="http://interface.ti.com">interface.ti.com</a>	Digital Control	<a href="http://www.ti.com/digitalcontrol">www.ti.com/digitalcontrol</a>
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