



Low Noise, Rail-to-Rail Precision Op Amp

February 2000

FEATURES

- Rail-to-Rail Input and Output
- 100% Tested Low Voltage Noise:
3.2nV/√Hz Typ at 1kHz
4.5nV/√Hz Max at 1kHz
- Offset Voltage: 60μV Max
- Low V_{OS} Drift: 0.2μV/°C Typ
- Low Input Bias Current: 20nA Max
- Wide Supply Range: 3V to ±15V
- High A_{VOL} : 4V/μV Min, $R_L = 1k$
- High CMRR: 109dB Min
- High PSRR: 108dB Min
- Gain Bandwidth Product: 7.2MHz
- Slew Rate: 2.5V/μs
- Operating Temperature Range: -40°C to 85°C

APPLICATIONS

- Low Noise Signal Processing
- Microvolt Accuracy Threshold Detection
- Strain Gauge Amplifiers
- Tape Head Preamplifiers
- Direct Coupled Audio Gain Stages
- Infrared Detectors

DESCRIPTION

The LT[®]1677 features the lowest noise performance available for a rail-to-rail operational amplifier: 3.2nV/√Hz wideband noise, 1/f corner frequency of 13Hz and 70nV peak-to-peak 0.1Hz to 10Hz noise. Low noise is combined with outstanding precision: 20μV offset voltage and 0.2μV/°C drift, 130dB common mode and power supply rejection and 7.2MHz gain bandwidth product. The common mode range exceeds the power supply by 100mV.

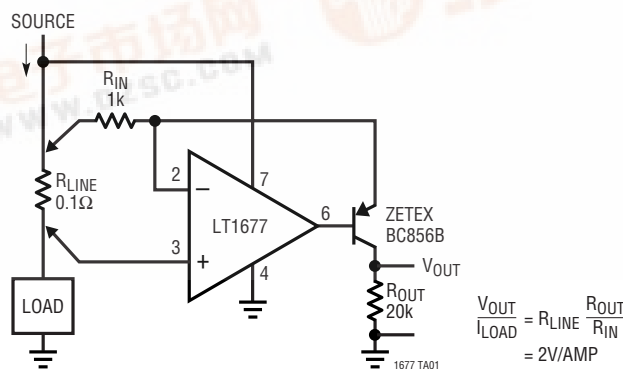
The voltage gain of the LT1677 is extremely high, especially with a single supply: 20 million driving a 1k load.

In the design, processing and testing of the device, particular attention has been paid to the optimization of the entire distribution of several key parameters. Consequently, the specifications of even the lowest cost grade have been spectacularly improved compared to competing rail-to-rail amplifiers.

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TYPICAL APPLICATION

Precision High Side Current Sense



ELECTRICAL CHARACTERISTICS

$T_A = 25^\circ\text{C}$, $V_S = \pm 15\text{V}$, $V_{CM} = V_O = 0\text{V}$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS (Note 6)	MIN	TYP	MAX	UNITS
i_n	Input Noise Current Density	$f_0 = 10\text{Hz}$ $f_0 = 1\text{kHz}$		1.2 0.3		$\text{pA}/\sqrt{\text{Hz}}$ $\text{pA}/\sqrt{\text{Hz}}$
V_{CM}	Input Voltage Range		± 15.1	± 15.2		V
R_{IN}	Input Resistance	Common Mode		2		$\text{G}\Omega$
C_{IN}	Input Capacitance	$V_S = \pm 2.5\text{V}$		3.8 4.2		pF pF
CMRR	Common Mode Rejection Ratio	$V_{CM} = -13.3\text{V}$ to 14.0V $V_{CM} = \pm 15.1\text{V}$	109 74	130 95		dB dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 1.7\text{V}$ to $\pm 18\text{V}$ $V_S = 2.7\text{V}$ to 40V , $V_{CM} = V_O = 1.7\text{V}$	106 108	130 125		dB dB
A_{VOL}	Large-Signal Voltage Gain	$R_L \geq 10\text{k}$, $V_O = \pm 14\text{V}$ $R_L \geq 1\text{k}$, $V_O = \pm 13.5\text{V}$ $R_L \geq 600\Omega$, $V_O = \pm 10\text{V}$	7 4 0.4	25 20 0.7		$\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$
		$V_{CC} = 5\text{V}$ or 3V , $V_{EE} = 0\text{V}$, $V_{CM} = 1.7\text{V}$, R_L to GND, $V_{OUT} = 0.5\text{V}$ to: $R_L \geq 10\text{k}$, $V_{CC} - 0.5\text{V}$ $R_L \geq 1\text{k}$, $V_{CC} - 0.7\text{V}$	2 1.5	10 4		$\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$
V_{OL}	Output Voltage Swing Low	Above V_{EE} $I_{SINK} = 0.1\text{mA}$ $I_{SINK} = 2.5\text{mA}$ $I_{SINK} = 10\text{mA}$		80 110 300	170 250 500	mV mV mV
V_{OH}	Output Voltage Swing High	Below V_{CC} $I_{SOURCE} = 0.1\text{mA}$ $I_{SOURCE} = 2.5\text{mA}$ $I_{SOURCE} = 10\text{mA}$		110 190 500	170 300 700	mV mV mV
I_{SC}	Output Short-Circuit Current (Note 3)		25	35		mA
SR	Slew Rate	$R_L \geq 10\text{k}$ (Note 9)	1.7	2.5		$\text{V}/\mu\text{s}$
GBW	Gain Bandwidth Product	$f_0 = 100\text{kHz}$	4.5	7.2		MHz
THD	Total Harmonic Distortion	$R_L = 2\text{k}$, $A_V = 1$, $f_0 = 1\text{kHz}$, $V_O = 10\text{V}_{P-P}$		0.0006		%
t_S	Settling Time	10V Step 0.1%, $A_V = +1$ 10V Step 0.01%, $A_V = +1$		5 6		μs μs
R_O	Open-Loop Output Resistance Closed-Loop Output Resistance	$I_{OUT} = 0$ $A_V = 100$, $f = 10\text{kHz}$		80 1		Ω Ω
I_S	Supply Current			2.75	3.5	mA

LT1677

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the temperature range of $0^{\circ}\text{C} < T_A < 70^{\circ}\text{C}$. $V_S = \pm 15\text{V}$, $V_{CM} = V_O = 0\text{V}$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS (Note 6)	MIN	TYP	MAX	UNITS
V_{OS}	Input Offset Voltage	● $V_{CM} = 14.0\text{V to } 14.8\text{V}$		30	120	μV
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		180	550	μV
		●		1.8	6	mV
$\frac{\Delta V_{OS}}{\Delta \text{Temp}}$	Average Input Offset Drift	● SO-8		0.40	2	$\mu\text{V}/^{\circ}\text{C}$
		● N8 (Note 10)		0.20	0.5	$\mu\text{V}/^{\circ}\text{C}$
I_B	Input Bias Current	● $V_{CM} = 14.0\text{V to } 14.8\text{V}$		± 3	± 35	nA
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		0.19	0.6	μA
		●	-2	-0.43		μA
I_{OS}	Input Offset Current	● $V_{CM} = 14.0\text{V to } 14.8\text{V}$		2	20	nA
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		90	220	nA
		●		90	350	nA
V_{CM}	Input Voltage Range	●	-15		14.8	V
CMRR	Common Mode Rejection Ratio	● $V_{CM} = -13.3\text{V to } 14.0\text{V}$	106	126		dB
		● $V_{CM} = -15\text{V to } 14.8\text{V}$	73	93		dB
PSRR	Power Supply Rejection Ratio	● $V_S = \pm 1.7\text{V to } \pm 18\text{V}$	104	127		dB
		● $V_S = 2.8\text{V to } 40\text{V}$, $V_{CM} = V_O = 1.7\text{V}$	106	122		dB
A_{VOL}	Large-Signal Voltage Gain	● $R_L \geq 10\text{k}$, $V_O = \pm 14\text{V}$	4	20		$\text{V}/\mu\text{V}$
		● $R_L \geq 1\text{k}$, $V_O = \pm 13.5\text{V}$	2	10		$\text{V}/\mu\text{V}$
		● $R_L \geq 600\Omega$, $V_O = \pm 10\text{V}$	0.3	0.5		$\text{V}/\mu\text{V}$
		● $V_{CC} = 5\text{V or } 3\text{V}$, $V_{EE} = 0\text{V}$, $V_{CM} = 1.7\text{V}$, $V_{OUT} = 0.4\text{V to:}$ ● $R_L \geq 10\text{k}$, $V_{CC} - 0.5\text{V}$ ● $R_L \geq 1\text{k}$, $V_{CC} - 0.7\text{V}$	3 0.5	8 4		$\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$
V_{OL}	Output Voltage Swing Low	● Above V_{EE}				
		● $I_{SINK} = 0.1\text{mA}$		85	200	mV
		● $I_{SINK} = 2.5\text{mA}$		160	320	mV
V_{OH}	Output Voltage Swing High	● Below V_{CC}				
		● $I_{SOURCE} = 0.1\text{mA}$		140	200	mV
		● $I_{SOURCE} = 2.5\text{mA}$		230	350	mV
I_{SC}	Output Short-Circuit Current (Note 3)	●	20	27		mA
		●				
SR	Slew Rate	● $R_L \geq 10\text{k}$ (Note 9)	1.5	2.3		$\text{V}/\mu\text{s}$
GBW	Gain Bandwidth Product	● $f_0 = 100\text{kHz}$		6.2		MHz
I_S	Supply Current	●		3.0	3.9	mA

ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the temperature range of $-40^{\circ}\text{C} < T_A < 85^{\circ}\text{C}$. $V_S = \pm 15\text{V}$, $V_{CM} = V_O = 0\text{V}$ unless otherwise noted. (Note 5)

SYMBOL	PARAMETER	CONDITIONS (Note 6)	MIN	TYP	MAX	UNITS
V_{OS}	Input Offset Voltage	● $V_{CM} = 14.0\text{V to } 14.7\text{V}$		45	180	μV
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		200	650	μV
		●		2	6.5	mV
$\frac{\Delta V_{OS}}{\Delta \text{Temp}}$	Average Input Offset Drift	● SO-8		0.40	2.0	$\mu\text{V}/^{\circ}\text{C}$
		● N8 (Note 10)		0.20	0.5	$\mu\text{V}/^{\circ}\text{C}$
I_B	Input Bias Current	● $V_{CM} = 14.0\text{V to } 14.7\text{V}$		± 7	± 50	nA
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		0.25	0.75	μA
		●	-2.3	-0.45		μA
I_{OS}	Input Offset Current	● $V_{CM} = 14.0\text{V to } 14.7\text{V}$		6	40	nA
		● $V_{CM} = -13.3\text{V to } -15\text{V}$		100	250	nA
		●		100	400	nA
V_{CM}	Input Voltage Range	●	-15		14.7	V
CMRR	Common Mode Rejection Ratio	● $V_{CM} = -13.3\text{V to } 14.0\text{V}$	105	124		dB
		● $V_{CM} = -15\text{V to } 14.7\text{V}$	72	91		dB
PSRR	Power Supply Rejection Ratio	● $V_S = \pm 1.7\text{V to } \pm 18\text{V}$	103	125		dB
		● $V_S = 3.1\text{V to } 40\text{V}$, $V_{CM} = V_O = 1.7\text{V}$	105	120		dB
A_{VOL}	Large-Signal Voltage Gain	● $R_L \geq 10\text{k}$, $V_O = \pm 14\text{V}$	3	17		$\text{V}/\mu\text{V}$
		● $R_L \geq 1\text{k}$, $V_O = \pm 13.5\text{V}$	1.5	8		$\text{V}/\mu\text{V}$
		● $R_L \geq 600\Omega$, $V_O = \pm 10\text{V}$	0.2	0.35		$\text{V}/\mu\text{V}$
		● $V_{CC} = 5\text{V or } 3\text{V}$, $V_{EE} = 0\text{V}$, $V_{CM} = 1.7\text{V}$, $V_{OUT} = 0.5\text{V to:}$ ● $R_L \geq 10\text{k}$, $V_{CC} - 0.5\text{V}$ ● $R_L \geq 1\text{k}$, $V_{CC} - 0.7\text{V}$	2	15		$\text{V}/\mu\text{V}$
V_{OL}	Output Voltage Swing Low	● Above V_{EE}		90	230	mV
		● $I_{SINK} = 0.1\text{mA}$		175	350	mV
		● $I_{SINK} = 2.5\text{mA}$ ● $I_{SINK} = 10\text{mA}$		450	650	mV
V_{OH}	Output Voltage Swing High	● Below V_{CC}		150	250	mV
		● $I_{SOURCE} = 0.1\text{mA}$		250	375	mV
		● $I_{SOURCE} = 2.5\text{mA}$ ● $I_{SOURCE} = 10\text{mA}$		600	850	mV
I_{SC}	Output Short-Circuit Current (Note 3)	●	18	25		mA
SR	Slew Rate	● $R_L \geq 10\text{k}$ (Note 9)	1.2	2.0		$\text{V}/\mu\text{s}$
GBW	Gain Bandwidth Product	● $f_0 = 100\text{kHz}$		5.8		MHz
I_S	Supply Current	●		3.1	4.0	mA

Note 1: Absolute Maximum Ratings are those values beyond which the life of the device may be impaired.

Note 2: The inputs are protected by back-to-back diodes. Current limiting resistors are not used in order to achieve low noise. If differential input voltage exceeds $\pm 1.4\text{V}$, the input current should be limited to 25mA. If the common mode range exceeds either rail, the input current should be limited to 10mA.

Note 3: A heat sink may be required to keep the junction temperature below absolute maximum.

Note 4: The LT1677C and LTC1677I are guaranteed functional over the Operating Temperature Range of -40°C to 85°C .

Note 5: The LT1677C is guaranteed to meet specified performance from 0°C to 70°C . The LT1677C is designed, characterized and expected to

meet specified performance from -40°C to 85°C but is not tested or QA sampled at these temperatures. The LT1677I is guaranteed to meet the extended temperature limits.

Note 6: Typical parameters are defined as the 60% yield of parameter distributions of individual amplifier; i.e., out of 100 LT1677s, typically 60 op amps will be better than the indicated specification.

Note 7: See the test circuit and frequency response curve for 0.1Hz to 10Hz tester in the Applications Information section of the LT1677 data sheet.

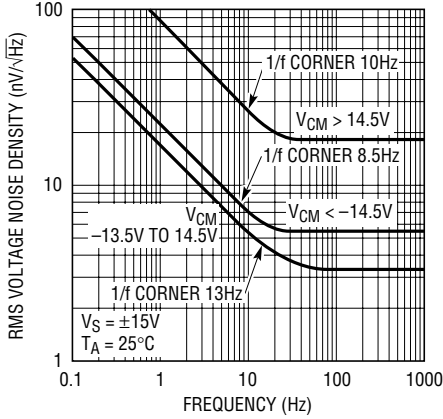
Note 8: Noise is 100% tested.

Note 9: Slew rate is measured in $A_V = -1$; input signal is $\pm 7.5\text{V}$, output measured at $\pm 2.5\text{V}$.

Note 10: This parameter is not 100% tested.

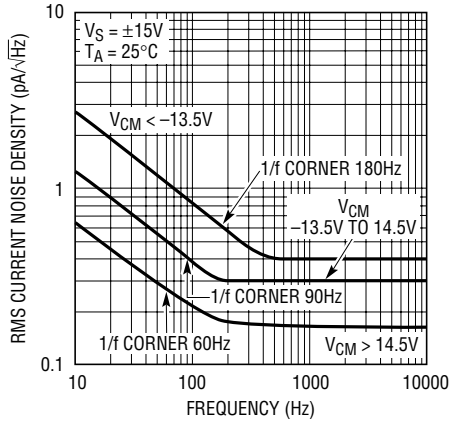
TYPICAL PERFORMANCE CHARACTERISTICS

Voltage Noise vs Frequency



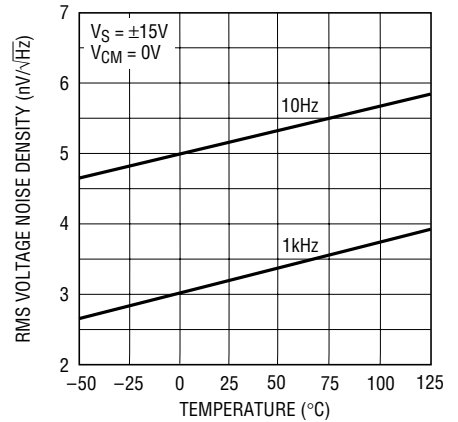
1677 G03

Current Noise vs Frequency



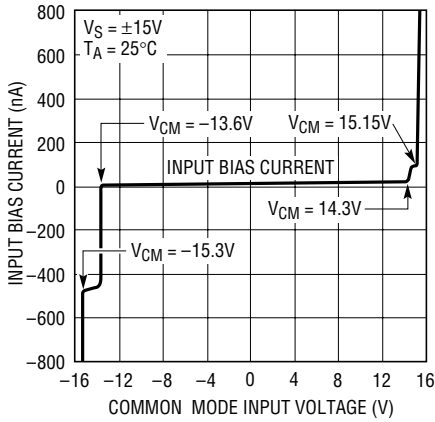
1677 G04

Voltage Noise vs Temperature



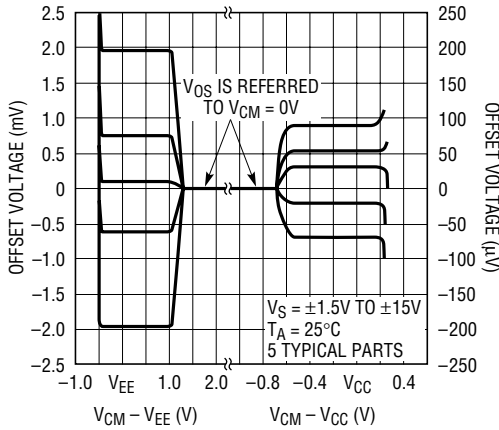
1677 G05

Input Bias Current Over the Common Mode Range



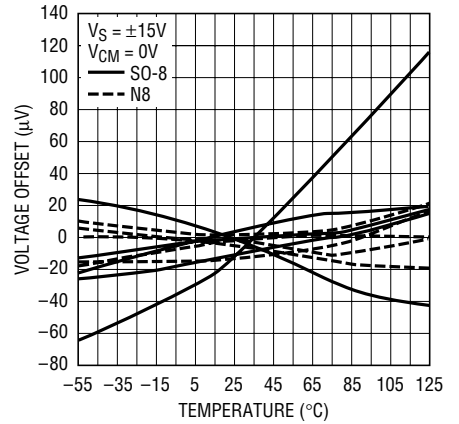
1677 G06

Offset Voltage Shift vs Common Mode



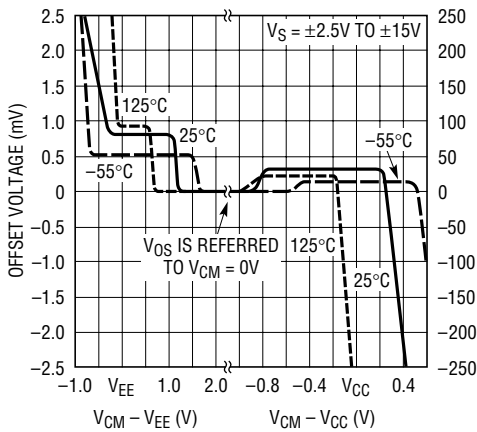
1677 G08

VOS vs Temperature of Representative Units



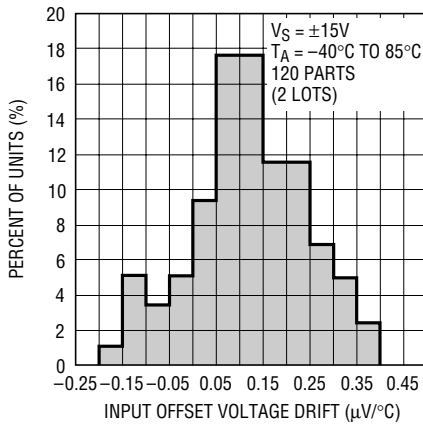
1677 G11

Common Mode Range vs Temperature



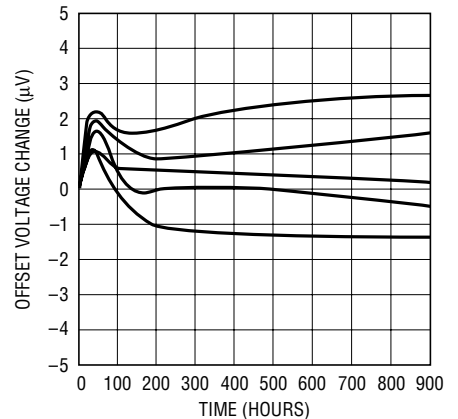
1677 G09

Distribution of Input Offset Voltage Drift (N8)



1677 G02

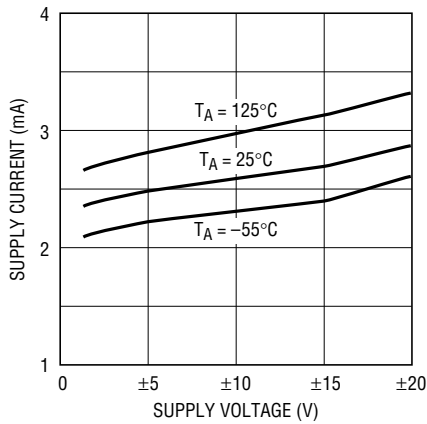
Long-Term Stability of Four Representative Units



1677 G13

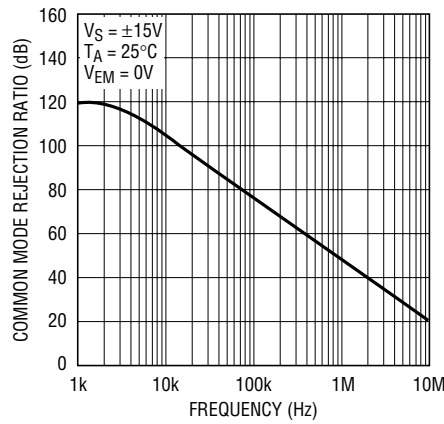
TYPICAL PERFORMANCE CHARACTERISTICS

Supply Current vs Supply Voltage



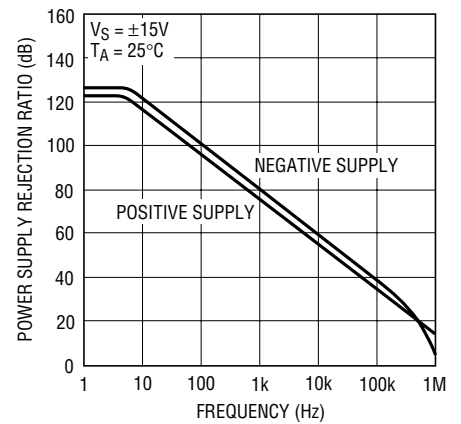
1677 G28

Common Mode Rejection Ratio vs Frequency



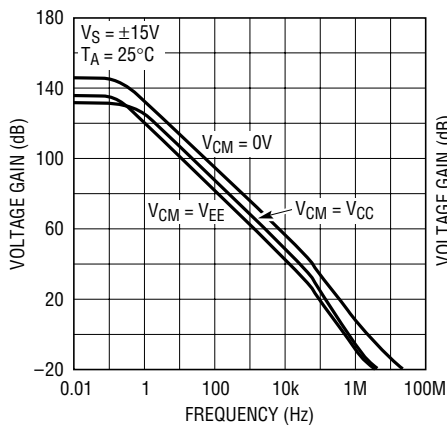
1677 G14

Power Supply Rejection Ratio vs Frequency



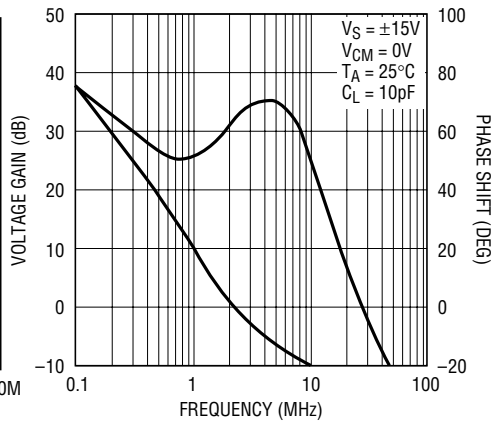
1677 G15

Voltage Gain vs Frequency



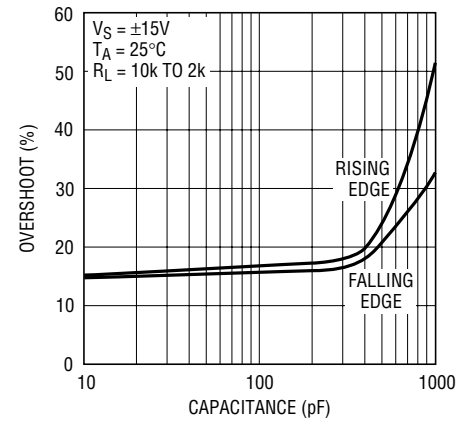
1677 G16

Gain, Phase Shift vs Frequency



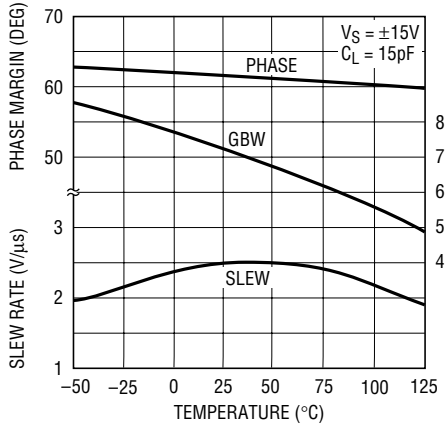
1677 G17

Overshoot vs Load Capacitance



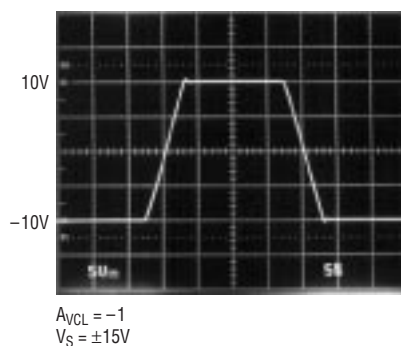
1677 G30

PM, GBWP, SR vs Temperature

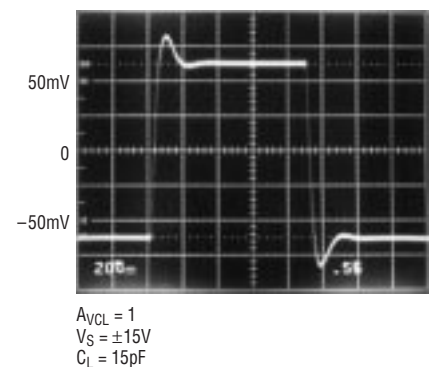


1677 G29

Large-Signal Transient Response

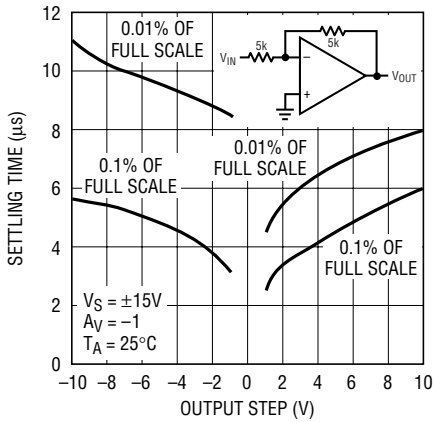


Small-Signal Transient Response



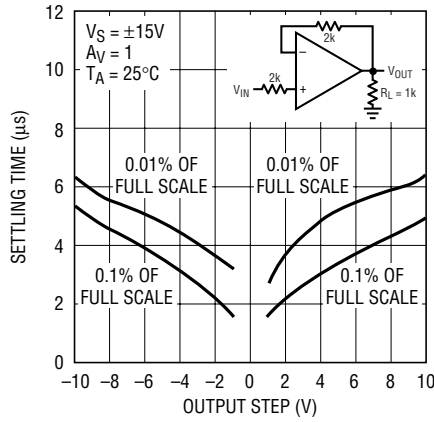
TYPICAL PERFORMANCE CHARACTERISTICS

Settling Time vs Output Step (Inverting)



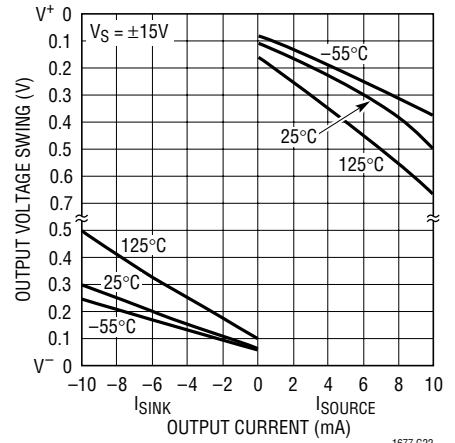
1677 G32

Settling Time vs Output Step (Noninverting)



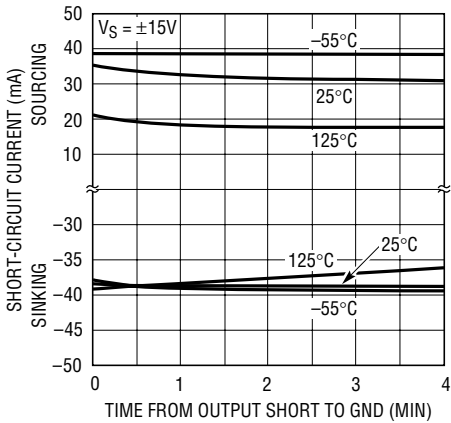
1677 G33

Output Voltage Swing vs Load Current



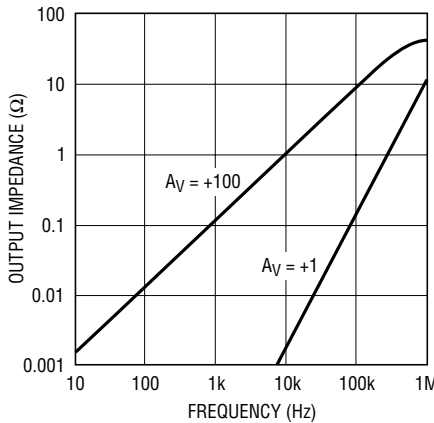
1677 G22

Output Short-Circuit Current vs Time



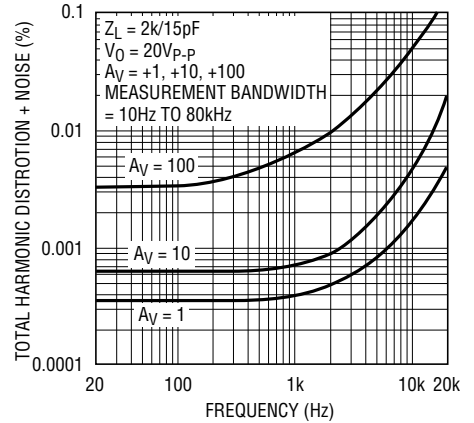
1677 G23

Closed-Loop Output Impedance vs Frequency



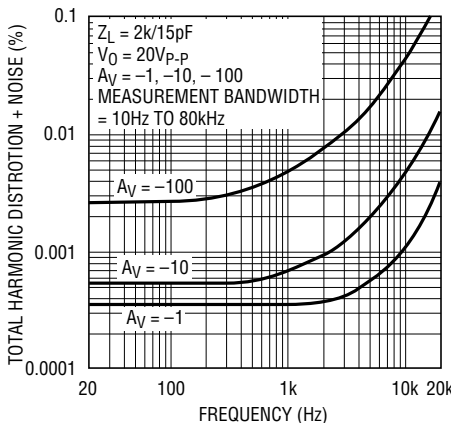
1677 G31

Total Harmonic Distortion and Noise vs Frequency for Noninverting Gain



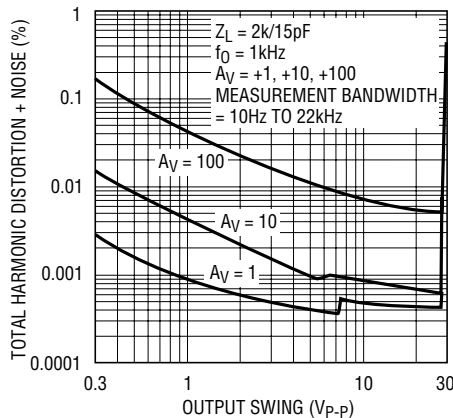
1677 G24

Total Harmonic Distortion and Noise vs Frequency for Inverting Gain



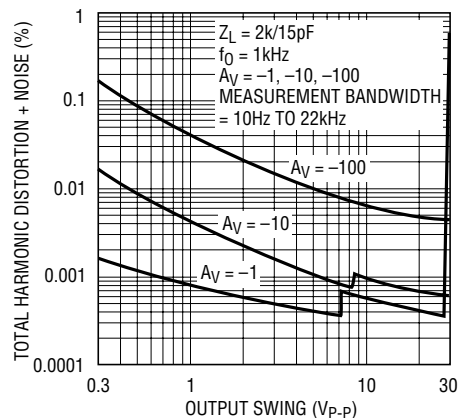
1677 G25

Total Harmonic Distortion and Noise vs Output Amplitude for Noninverting Gain



1677 G26

Total Harmonic Distortion and Noise vs Output Amplitude for Inverting Gain



1677 G27

APPLICATIONS INFORMATION

General

The LT1677 series devices may be inserted directly into OP-07, OP-27, OP-37 and sockets with or without removal of external compensation or nulling components. In addition, the LT1677 may be fitted to 741 sockets with the removal or modification of external nulling components.

Rail-to-Rail Operation

To take full advantage of an input range that can exceed the supply, the LT1677 is designed to eliminate phase reversal. Referring to the photographs shown in Figure 1, the LT1677 is operating in the follower mode ($A_V = +1$) at a single 3V supply. The output of the LT1677 clips cleanly and recovers with no phase reversal. This has the benefit of preventing lock-up in servo systems and minimizing distortion components.

Offset Voltage Adjustment

The input offset voltage of the LT1677 and its drift with temperature are permanently trimmed at wafer testing to a low level. However, if further adjustment of V_{OS} is necessary, the use of a 10k Ω nulling potentiometer will not degrade drift with temperature. Trimming to a value other than zero creates a drift of $(V_{OS}/300)\mu V/^\circ C$, e.g., if V_{OS} is adjusted to 300 μV , the change in drift will be 1 $\mu V/^\circ C$ (Figure 2).

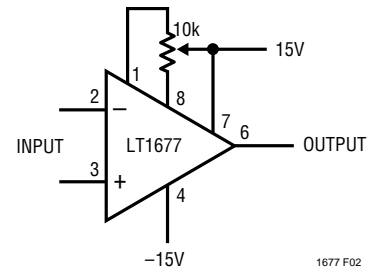


Figure 2. Standard Adjustment

The adjustment range with a 10k Ω pot is approximately $\pm 2.5mV$. If less adjustment range is needed, the sensitivity and resolution of the nulling can be improved by using a smaller pot in conjunction with fixed resistors. The example has an approximate null range of $\pm 200\mu V$ (Figure 3).

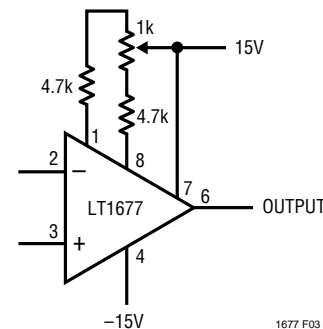


Figure 3. Improved Sensitivity Adjustment

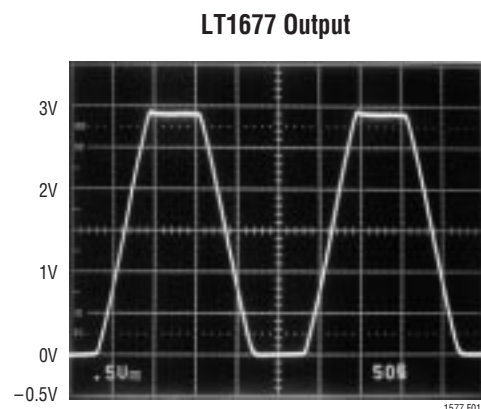
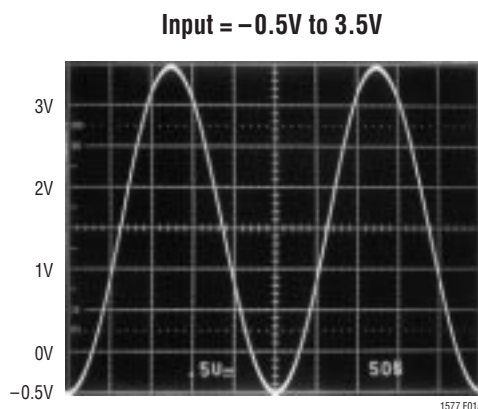


Figure 1. Voltage Follower with Input Exceeding the Supply Voltage ($V_S = 3V$)

APPLICATIONS INFORMATION

Offset Voltage and Drift

Thermocouple effects, caused by temperature gradients across dissimilar metals at the contacts to the input terminals, can exceed the inherent drift of the amplifier unless proper care is exercised. Air currents should be minimized, package leads should be short, the two input leads should be close together and maintained at the same temperature.

The circuit shown to measure offset voltage is also used as the burn-in configuration for the LT1677, with the supply voltages increased to $\pm 20V$ (Figure 4).

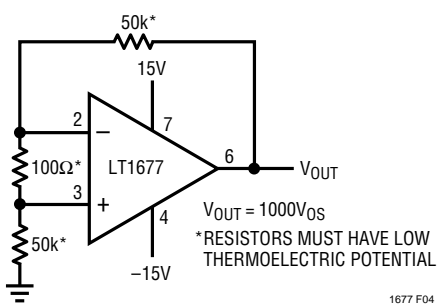


Figure 4. Test Circuit for Offset Voltage and Offset Voltage Drift with Temperature

Unity-Gain Buffer Application

When $R_F \leq 100\Omega$ and the input is driven with a fast, large-signal pulse ($>1V$), the output waveform will look as shown in the pulsed operation diagram (Figure 5).

During the fast feedthrough-like portion of the output, the input protection diodes effectively short the output to the input and a current, limited only by the output short-circuit protection, will be drawn by the signal generator. With $R_F \geq 500\Omega$, the output is capable of handling the current requirements ($I_L \leq 20mA$ at 10V) and the amplifier stays in its active mode and a smooth transition will occur.

As with all operational amplifiers when $R_F > 2k$, a pole will be created with R_F and the amplifier's input capacitance,

creating additional phase shift and reducing the phase margin. A small capacitor (20pF to 50pF) in parallel with R_F will eliminate this problem.

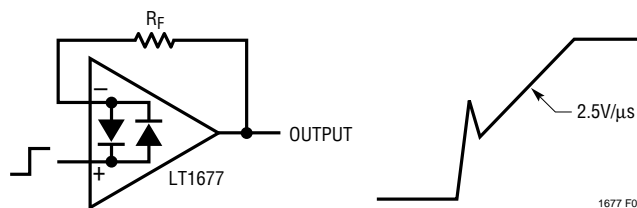


Figure 5. Pulsed Operation

Noise Testing

The 0.1Hz to 10Hz peak-to-peak noise of the LT1677 is measured in the test circuit shown (Figure 6a). The frequency response of this noise tester (Figure 6b) indicates that the 0.1Hz corner is defined by only one zero. The test time to measure 0.1Hz to 10Hz noise should not exceed ten seconds, as this time limit acts as an additional zero to eliminate noise contributions from the frequency band below 0.1Hz.

Measuring the typical 70nV peak-to-peak noise performance of the LT1677 requires special test precautions:

1. The device should be warmed up for at least five minutes. As the op amp warms up, its offset voltage changes typically $3\mu V$ due to its chip temperature increasing $10^\circ C$ to $20^\circ C$ from the moment the power supplies are turned on. In the ten-second measurement interval these temperature-induced effects can easily exceed tens of nanovolts.
2. For similar reasons, the device must be well shielded from air currents to eliminate the possibility of thermoelectric effects in excess of a few nanovolts, which would invalidate the measurements.
3. Sudden motion in the vicinity of the device can also "feedthrough" to increase the observed noise.

APPLICATIONS INFORMATION

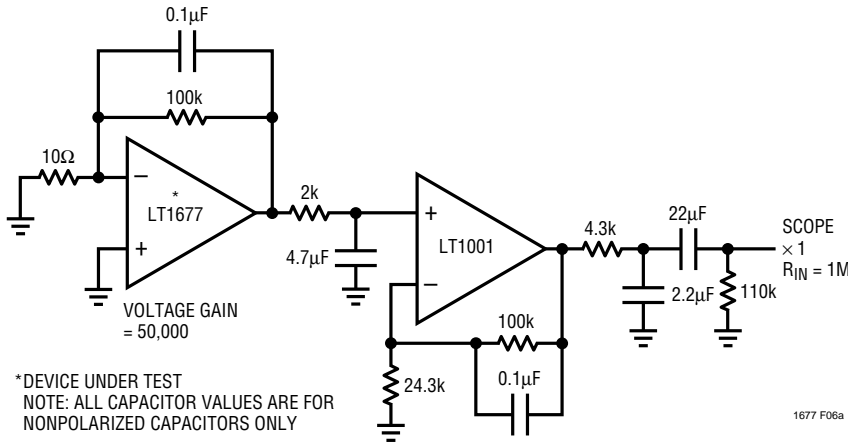


Figure 6a. 0.1Hz to 10Hz Noise Test Circuit

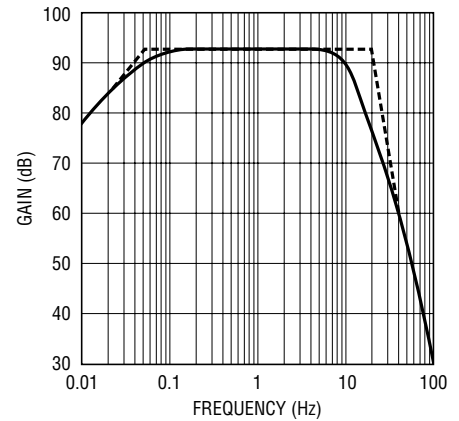


Figure 6b. 0.1Hz to 10Hz Peak-to-Peak Noise Tester Frequency Response

Current noise is measured in the circuit shown in Figure 7 and calculated by the following formula:

$$i_n = \left[\frac{(\epsilon_{no})^2 - (130\text{nV} \cdot 101)^2}{(1\text{M}\Omega)(101)} \right]^{1/2}$$

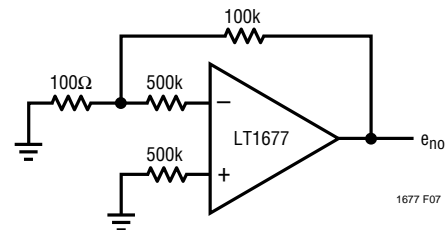


Figure 7

The LT1677 achieves its low noise, in part, by operating the input stage at 120µA versus the typical 10µA of most other op amps. Voltage noise is inversely proportional while current noise is directly proportional to the square root of the input stage current. Therefore, the LT1677's current noise will be relatively high. At low frequencies, the low 1/f current noise corner frequency (≈90Hz) minimizes current noise to some extent.

In most practical applications, however, current noise will not limit system performance. This is illustrated in the Total Noise vs Source Resistance plot (Figure 8) where:

$$\text{Total Noise} = [(voltage\ noise)^2 + (current\ noise \cdot R_S)^2 + (resistor\ noise)^2]^{1/2}$$

Three regions can be identified as a function of source resistance:

- (i) $R_S \leq 400\Omega$. Voltage noise dominates
- (ii) $400\Omega \leq R_S \leq 50\text{k}$ at 1kHz } Resistor noise dominates
- $400\Omega \leq R_S \leq 8\text{k}$ at 10Hz }

- (iii) $R_S > 50\text{k}$ at 1kHz } Current noise dominates
- $R_S > 8\text{k}$ at 10Hz }

Clearly the LT1677 should not be used in region (iii), where total system noise is at least six times higher than the

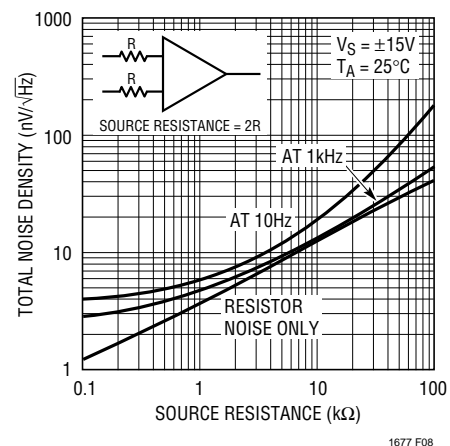


Figure 8. Total Noise vs Source Resistance

LT1677

APPLICATIONS INFORMATION

voltage noise of the op amp, i.e., the low voltage noise specification is completely wasted. In this region the LT1792 or LT1793 is the best choice.

Rail-to-Rail Input

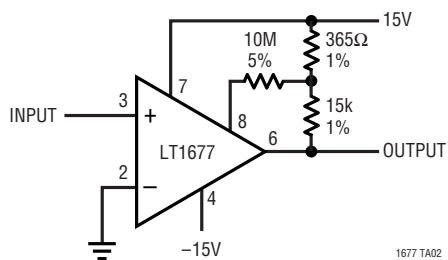
The LT1677 has the lowest voltage noise, offset voltage and highest gain when compared to any rail-to-rail op amp. The input common mode range for the LT1677 can exceed the supplies by at least 100mV. As the common mode voltage approaches the positive rail ($V_{CC} - 0.7V$), the tail current for the input pair (Q1, Q2) is reduced, which prevents the input pair from saturating (refer to the Simplified Schematic). The voltage drop across the load

resistors R_{C1} , R_{C2} is reduced to less than 200mV, degrading the slew rate, bandwidth voltage noise, offset voltage and input bias current (the cancellation is shut off).

When the input common mode range goes below 1.5V above the negative rail, the NPN input pair (Q1, Q2) shuts off and the PNP input pair (Q8, Q9) turns on. The offset voltage, input bias current, voltage noise and bandwidth are also degraded. The graph of Offset Voltage vs Common Mode Range shows where the knees occur by displaying the change in offset voltage. The change-over points are temperature dependent, see Common Mode Range vs Temperature.

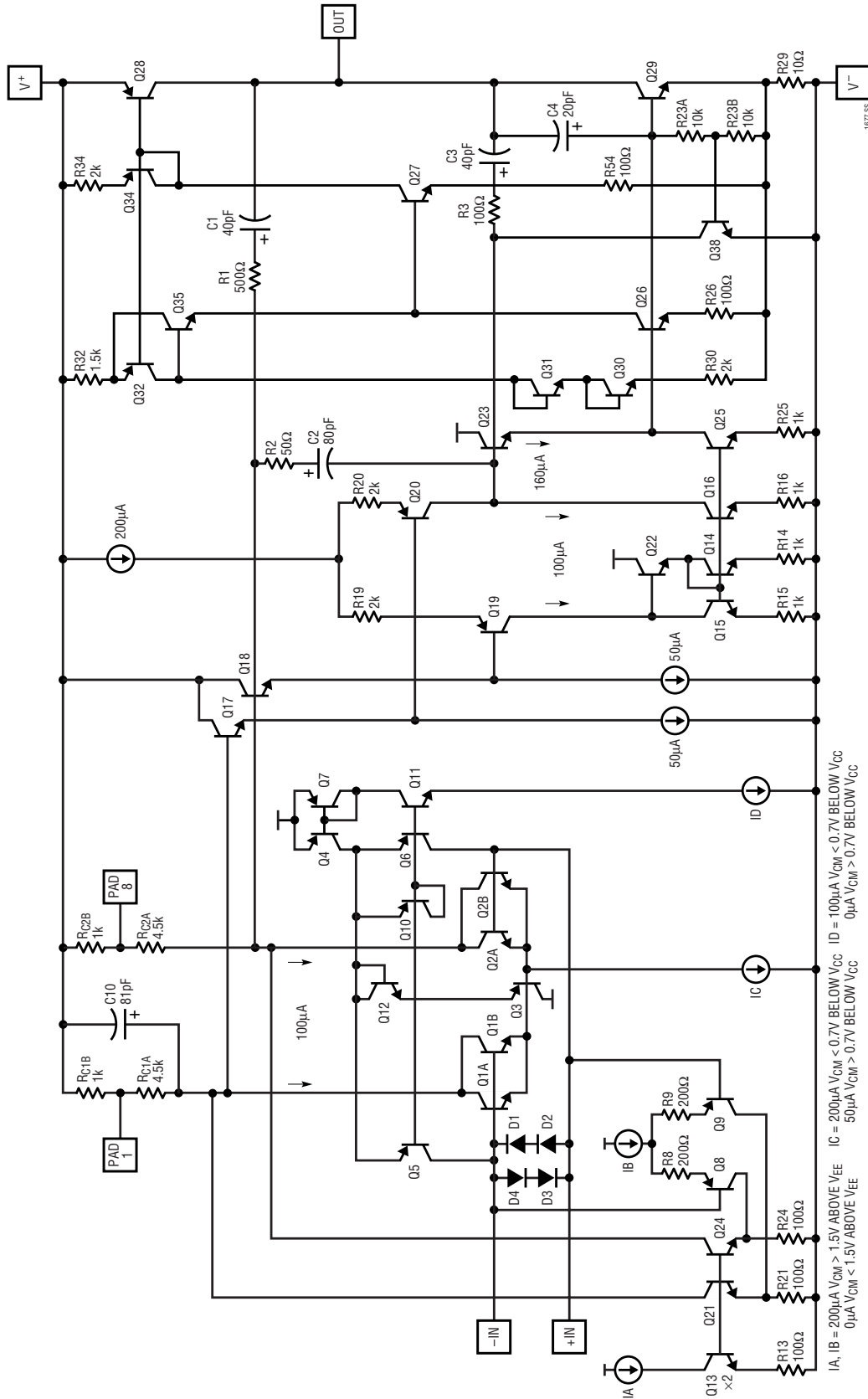
TYPICAL APPLICATION

Microvolt Comparator with Hysteresis



POSITIVE FEEDBACK TO ONE OF THE NULLING TERMINALS
CREATES APPROXIMATELY $5\mu V$ OF HYSTERESIS. OUTPUT
CAN SINK 16mA
INPUT OFFSET VOLTAGE IS TYPICALLY CHANGED LESS THAN
 $5\mu V$ DUE TO THE FEEDBACK

SIMPLIFIED SCHEMATIC

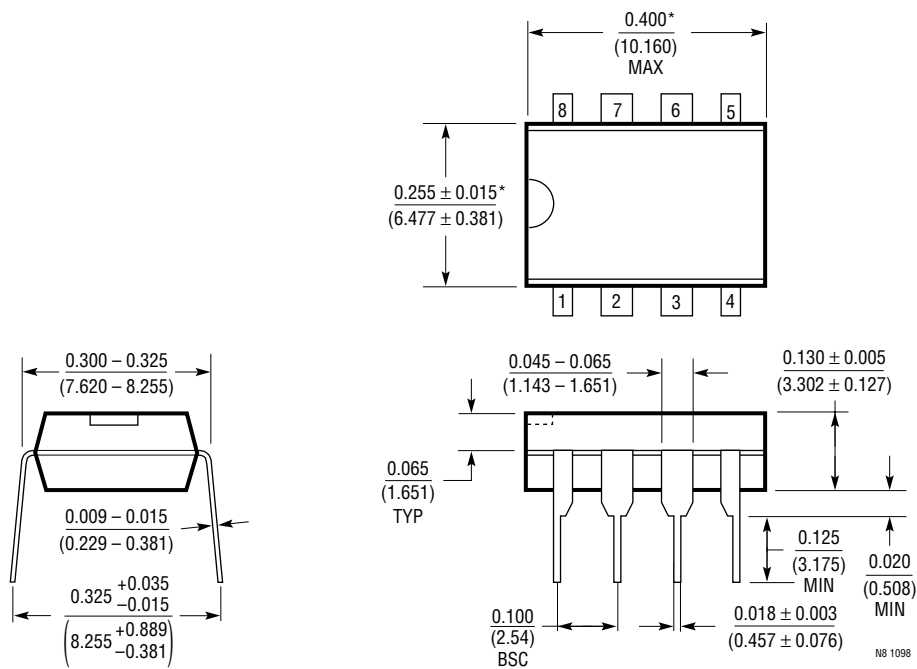


LT1677

PACKAGE DESCRIPTION

Dimensions in inches (millimeters) unless otherwise noted.

N8 Package 8-Lead PDIP (Narrow 0.300) (LTC DWG # 05-08-1510)



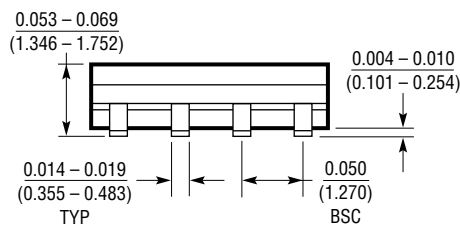
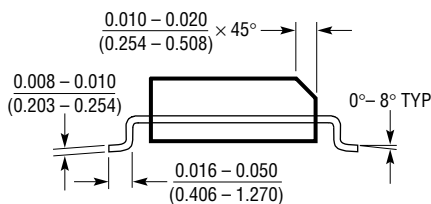
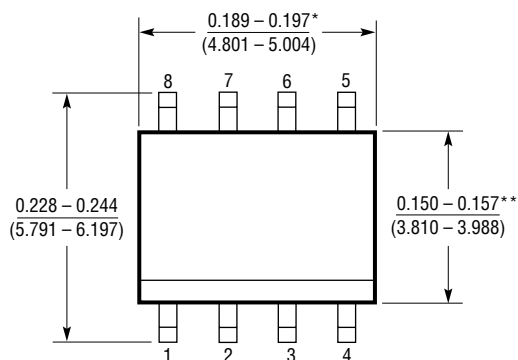
*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)

N8 1098

PACKAGE DESCRIPTION

Dimensions in inches (millimeters) unless otherwise noted.

S8 Package
8-Lead Plastic Small Outline (Narrow 0.150)
 (LTC DWG # 05-08-1610)



*DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

**DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

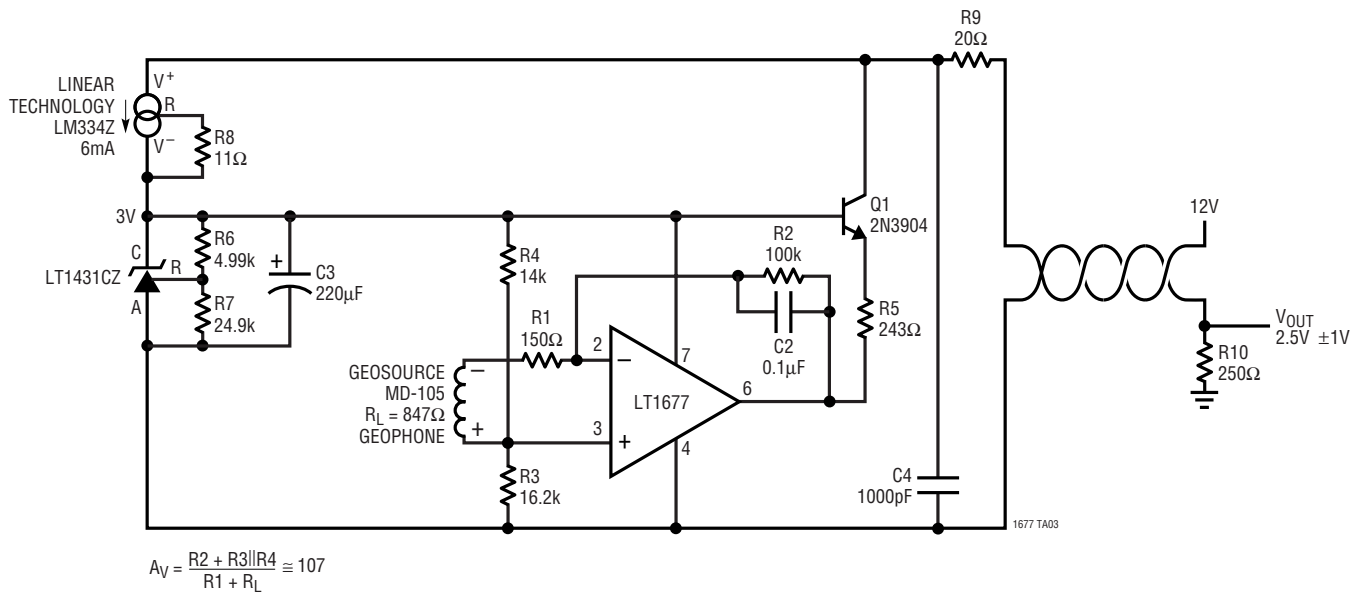
LT1677

TYPICAL APPLICATION

This 2-wire remote Geophone preamp operates on a current-loop principle and so has good noise immunity. Quiescent current is $\approx 10\text{mA}$ for a V_{OUT} of 2.5V . Excitation will cause AC currents about this point of $\approx \pm 4\text{mA}$ for a V_{OUT} of $\approx \pm 1\text{V}$ max. The op amp is configured for a voltage

gain of ~ 107 . Components R5 and Q1 convert the voltage into a current for transmission back to R10, which converts it into a voltage again. The LM334 and 2N3904 are not temperature compensated so the DC output contains temperature information.

2-Wire Remote Geophone Preamp



RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1028	Ultralow Noise Precision Op Amp	Lowest Noise $0.85\text{nV}/\sqrt{\text{Hz}}$
LT1115	Ultralow Noise, Low distortion Audio Op Amp	0.002% THD, Max Noise $1.2\text{nV}/\sqrt{\text{Hz}}$
LT1124/LT1125	Dual/Quad Low Noise, High Speed Precision Op Amps	Similar to LT1007
LT1126/LT1127	Dual/Quad Decompensated Low Noise, High Speed Precision Op Amps	Similar to LT1037
LT1498/LT1499	10MHz, $5\text{V}/\mu\text{s}$, Dual/Quad Rail-to-Rail Input and Output Op Amps	Precision C-Load™ Stable
LT1792	Low Noise, Precision JFET Input Op Amp	$4.2\text{nV}/\sqrt{\text{Hz}}$, $10\text{fA}/\sqrt{\text{Hz}}$
LT1793	Low Noise, Picoampere Bias Current Op Amp	$6\text{nV}/\sqrt{\text{Hz}}$, $1\text{fA}/\sqrt{\text{Hz}}$
LT1884	Dual Rail-to-Rail Output Picoamp Input Precision Op Amp	2.2MHz Bandwidth, $1.2\text{V}/\mu\text{s}$ SR

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