# **Micropower Fixed Frequency PWM Step-Up DC-DC Converter**

The NCP1400A series are micropower step-up DC to DC converters that are specifically designed for powering portable equipment from one or two cell battery packs. These devices are designed to start-up with a cell voltage of 0.8 V and operate down to less than 0.2 V. With only four external components, this series allows a simple means to implement highly efficient converters that are capable of up to 100 mA of output current.

Each device consists of an on-chip fixed frequency oscillator, pulse width modulation controller, phase compensated error amplifier that ensures converter stability with discontinuous mode operation, soft-start, voltage reference, driver, and power MOSFET switch with current limit protection. Additionally, a chip enable feature is provided to power down the converter for extended battery life.

The NCP1400A device series are available in the TSOP-5 package with five standard regulated output voltages. Additional voltages that range from 1.8 V to 4.9 V in 100 mV steps can be manufactured.

- Extremely Low Start-Up Voltage of 0.8 V
- Operation Down to Less than 0.2 V
- Only Four External Components for Simple Highly Efficient Converters
- Up to 100 mA Output Current Capability
- Fixed Frequency Pulse Width Modulation Operation
- Phase Compensated Error Amplifier for Stable Converter Operation
- Chip Enable Power Down Capability for Extended Battery Life

#### **Typical Applications**

- Cellular Telephones
- Pagers
- Personal Digital Assistants
- Electronic Games
- Digital Cameras
- Camcorders
- Handheld Instruments



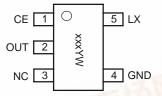
# ON Semiconductor

http://onsemi.com



TSOP-5 **SN SUFFIX CASE 483** 

### **PIN CONNECTIONS AND** MARKING DIAGRAM



xxx = Marking = Year

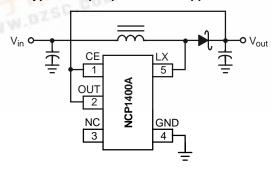
= Work Week

(Top View)

#### ORDERING INFORMATION

See detailed ordering and shipping information in the ordering information section on page 2 of this data sheet.

#### Typical Step-Up Converter Application





#### **ORDERING INFORMATION**

Device	Output Voltage	Switching Frequency	Marking	Package	Shipping
NCP1400ASN19T1	1.9 V		DAI		
NCP1400ASN27T1	2.7 V		DAA		
NCP1400ASN30T1	3.0 V	180 KHz	DAB	TSOP-5	3000 Units on 7 Inch Reel
NCP1400ASN33T1	3.3 V		DAJ		
NCP1400ASN50T1	5.0 V		DAD		

NOTE: The ordering information lists five standard output voltage device options. Additional devices with output voltage ranging from 1.8 V to 5.0 V in 100 mV increments can be manufactured. Contact your ON Semiconductor representative for availability.

#### **ABSOLUTE MAXIMUM RATINGS**

Rating	Symbol	Value	Unit
Power Supply Voltage (Pin 2)	V <sub>OUT</sub>	-0.3 to 6.0	V
Input/Output Pins LX (Pin 5) LX Peak Sink Current	V <sub>LX</sub> I <sub>LX</sub>	-0.3 to 6.0 400	V mA
CE (Pin 1) Input Voltage Range Input Current Range	V <sub>CE</sub> I <sub>CE</sub>	-0.3 to 6.0 -150 to 150	V mA
Thermal Resistance Junction to Air	$R_{ heta JA}$	250	°C/W
Operating Ambient Temperature Range (Note 2.)	T <sub>A</sub>	-40 to +85	°C
Operating Junction Temperature Range	TJ	-40 to +125	°C
Storage Temperature Range	T <sub>stg</sub>	-55 to +150	°C

#### NOTES:

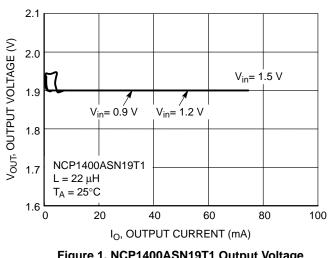
- This device series contains ESD protection and exceeds the following tests: Human Body Model 2.0 kV per MIL-STD-883, Method 3015.
   Machine Model Method 200 V.
- 2. The maximum package power dissipation limit must not be exceeded.

$$P_D = \frac{T_{J(max)} - T_A}{R_{\theta}JA}$$

### **ELECTRICAL CHARACTERISTICS** (For all values $T_{\Delta} = 25^{\circ}$ C, unless otherwise noted.)

Characteristic	Symbol	Min	Тур	Max	Unit
OSCILLATOR	•	•		•	•
Frequency (V <sub>OUT</sub> = V <sub>SET</sub> x 0.96, Note 3.)	fosc	144	180	216	kHz
Frequency Temperature Coefficient (T <sub>A</sub> = -40°C to 85°C)	Δf	-	0.11	_	%/°C
Maximum PWM Duty Cycle (V <sub>OUT</sub> = V <sub>SET</sub> x 0.96)	D <sub>MAX</sub>	68	75	82	%
Minimum Start-up Voltage (I <sub>O</sub> = 0 mA)	V <sub>start</sub>	-	0.8	0.95	V
Minimum Start-up Voltage Temperature Coefficient (T <sub>A</sub> = -40°C to 85°C)	$\Delta V_{start}$	-	-1.6	_	mV/°C
Minimum Operation Hold Voltage (I <sub>O</sub> = 0 mA)	V <sub>hold</sub>	0.3	-	-	V
Soft–Start Time (V <sub>OUT</sub> > 0.8 V)	t <sub>SS</sub>	0.5	2.0	_	ms
LX (PIN 5)	1	I		I	<u> </u>
LX Pin On–State Sink Current (V <sub>LX</sub> = 0.4 V)	I <sub>LX</sub>				mA
Device Suffix:		00	00		
19T1 27T1		80 100	90 125	_	
30T1		100	130	_	
33T1		100	135	_	
50T1		100	160	_	
Voltage Limit (V <sub>OUT</sub> = V <sub>CE</sub> = V <sub>SET</sub> x 0.96, V <sub>LX</sub> "L" Side)	V <sub>LXLIM</sub>	0.65	0.8	1.0	V
Off–State Leakage Current ( $V_{LX} = 5.0 \text{ V}$ , $T_A = -40^{\circ}\text{C}$ to $85^{\circ}\text{C}$ )	I <sub>LKG</sub>	_	0.5	1.0	μΑ
CE (PIN 1)					
CE Input Voltage (V <sub>OUT</sub> = V <sub>SET</sub> x 0.96)					V
High State, Device Enabled	V <sub>CE(high)</sub>	0.9	_	_	
Low State, Device Disabled	V <sub>CE(low)</sub>	_	_	0.3	
CE Input Current (Note 4.)					mA
High State, Device Enabled (V <sub>OUT</sub> = V <sub>CE</sub> = 5.0 V)	I <sub>CE(high)</sub>	-0.5	0	0.5	
Low State, Device Disabled (V <sub>OUT</sub> = 5.0 V, V <sub>CE</sub> = 0 V)	I <sub>CE(low)</sub>	-0.5	0.15	0.5	
TOTAL DEVICE		I		I	T ,,
Output Voltage ( $V_{in} > 0.8 \text{ V}$ , $I_{O} = 4.0 \text{ mA}$ ) Device Suffix:	V <sub>OUT</sub>				V
19T1		1.853	1.9	1.948	
27T1		2.633	2.7	2.768	
30T1		2.925	3.0	3.075	
33T1		3.218	3.3	3.383	
50T1		4.875	5.0	5.125	
Output Voltage Temperature Coefficient ( $T_A = -40^{\circ}C$ to +85°C) Device Suffix:	$\Delta V_{OUT}$				ppm/°C
19T1		_	100	_	
27T1		_	100	_	
30T1		_	100	_	
33T1		_	100	_	
50T1		-	150	_	
Operating Current 2 (V <sub>OUT</sub> = V <sub>CE</sub> = V <sub>SET</sub> +0.5 V, Note 3.)	I <sub>DD2</sub>	_	7.0	15	μΑ
Off–State Current ( $V_{OUT} = 5.0 \text{ V}$ , $V_{CE} = 0 \text{ V}$ , $T_A = -40^{\circ}\text{C}$ to +85°C, Note 4.)	I <sub>OFF</sub>	-	0.6	1.5	μΑ
Operating Current 1 ( $V_{OUT} = V_{CE} = V_{SET} \times 0.96$ , $f_{OSC} = 180 \text{ kHz}$ ) Device Suffix:	I <sub>DD1</sub>				μΑ
19T1		_	23	50	
27T1		_	32	60	
30T1		_	37	60	
33T1		_	37	60	
50T1			70	100	1

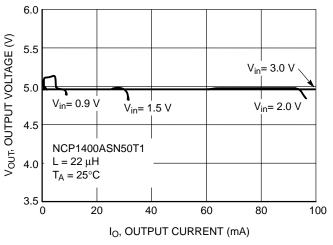
<sup>3.</sup>  $V_{SET}$  means setting of output voltage. 4. CE pin is integrated with an internal 10 M $\Omega$  pull–up resistor.



3.4 V<sub>OUT</sub>, OUTPUT VOLTAGE (V) 3.2  $V_{in}$ = 2.0 V3.0 V<sub>in</sub>= 1.2 V V<sub>in</sub>= 1.5 V V<sub>in</sub>= 0.9 V 2.8 NCP1400ASN30T1  $L=22~\mu H$ 2.6  $T_A = 25^{\circ}C$ 2.4 0 20 40 60 80 100 I<sub>O</sub>, OUTPUT CURRENT (mA)

Figure 1. NCP1400ASN19T1 Output Voltage vs. Output Current

Figure 2. NCP1400ASN30T1 Output Voltage vs. Output Current



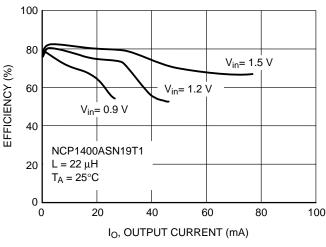
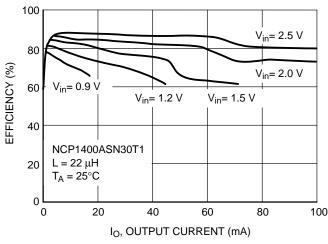


Figure 3. NCP1400ASN50T1 Output Voltage vs. Output Current

Figure 4. NCP1400ASN19T1 Efficiency vs.
Output Current



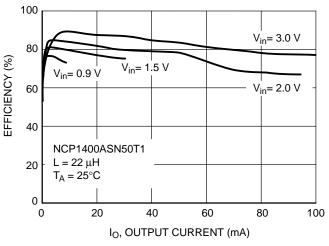
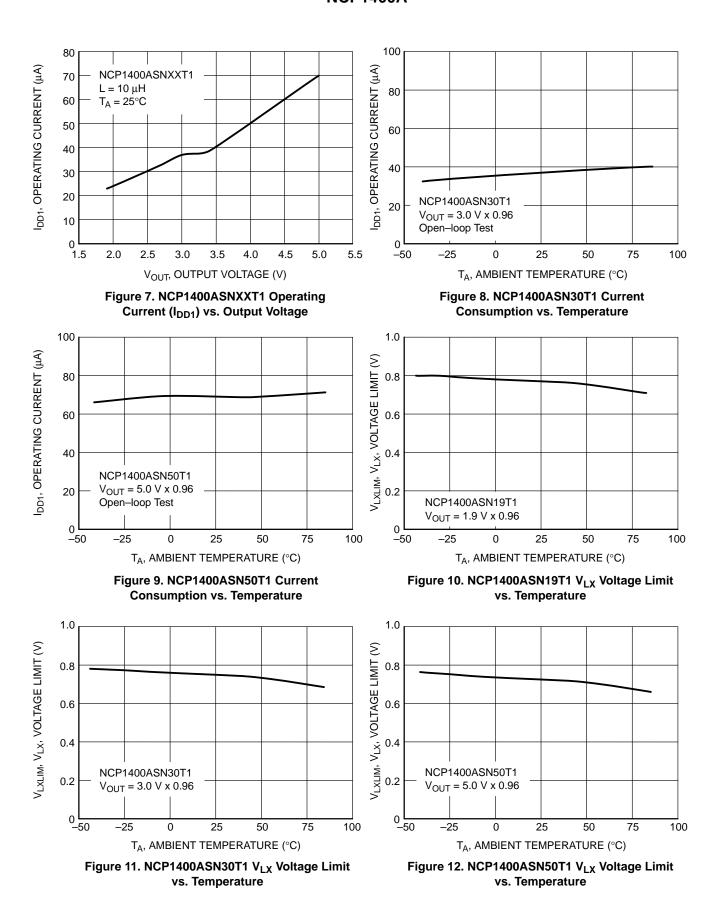


Figure 5. NCP1400ASN30T1 Efficiency vs.
Output Current

Figure 6. NCP1400ASN50T1 Efficiency vs.
Output Current



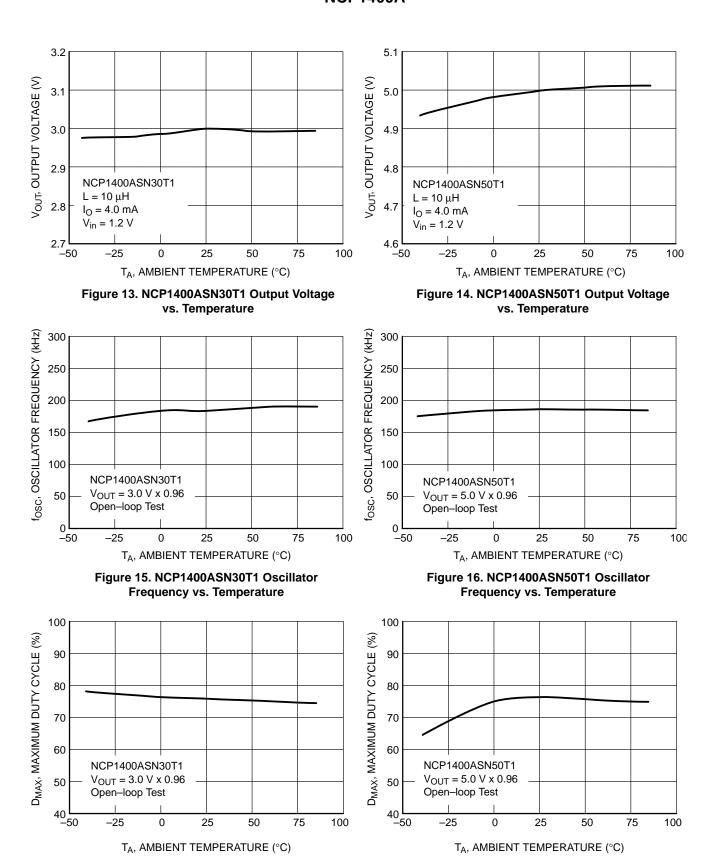
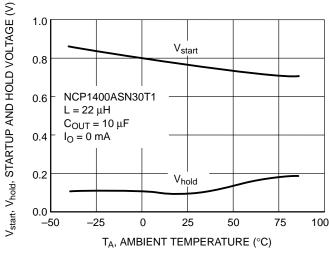


Figure 17. NCP1400ASN30T1 Maximum Duty Cycle vs. Temperature

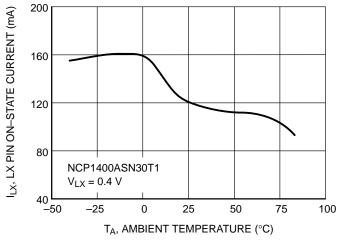
Figure 18. NCP1400ASN50T1 Maximum Duty Cycle vs. Temperature



 $V_{start}$ NCP1400ASN50T1  $L = 22 \mu H$  $C_{OUT} = 10 \mu F$  $I_0 = 0 \text{ mA}$  $V_{hold}$ Vhold, Vstart, 0.0 -50 -25 0 25 50 75 100 TA, AMBIENT TEMPERATURE (°C)

Figure 19. NCP1400ASN30T1 Startup/Hold Voltage vs. Temperature

Figure 20. NCP1400ASN50T1 Startup/Hold Voltage vs. Temperature



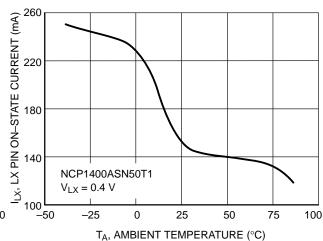
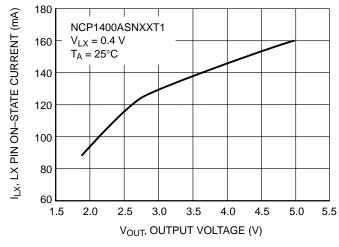


Figure 21. NCP1400ASN30T1 LX Pin On–State Current vs. Temperature

Figure 22. NCP1400ASN50T1 LX Pin On–State Current vs. Temperature



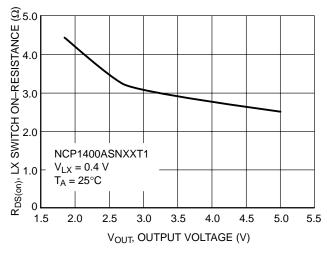
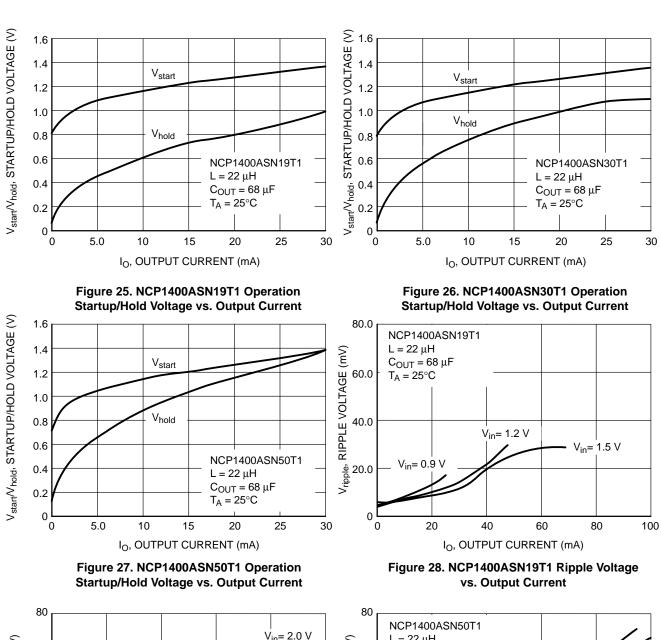


Figure 23. NCP1400ASNXXT1 LX Pin On–State Current vs. Output Voltage

Figure 24. NCP1400ASNXXT1 LX Switchon Resistance vs. Output Voltage



 $V_{in}$ = 2.0 VVripple, RIPPLE VOLTAGE (mV)  $V_{in}$ = 1.5 V60 V<sub>in</sub>= 1.5 V 40 NCP1400ASN30T1  $V_{in} = 0.9 V$  $L = 22 \mu H$ 20  $C_{OUT} = 68 \mu F$  $T_A = 25^{\circ}C$ 0 60 100 I<sub>O</sub>, OUTPUT CURRENT (mA)

Figure 29. NCP1400ASN30T1 Ripple Voltage vs. Output Current

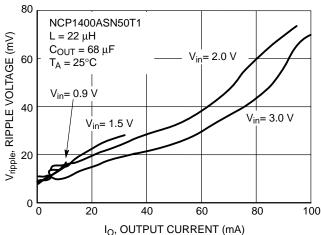
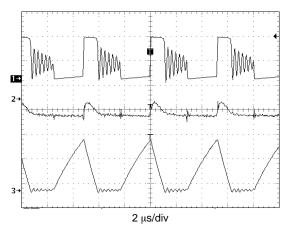


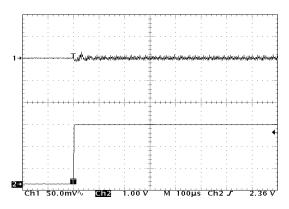
Figure 30. NCP1400ASN50T1 Ripple Voltage vs. Output Current



 $V_{OUT}$  = 3.0 V,  $V_{in}$  = 1.2 V,  $I_{O}$  = 10 mA., L = 22  $\mu H,\,C_{OUT}$  = 68  $\mu F$ 

- 1.  $V_{LX}$ , 2.0 V/div
- 2.  $V_{OUT}$ , 20 mV/div, AC coupled
- 3. I<sub>L</sub>, 100 mA/div

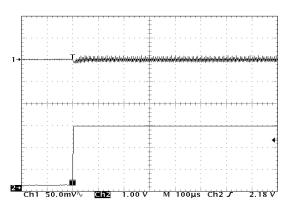
Figure 31. Operating Waveforms (Medium Load)



 $V_{in}$  = 1.2 V, L = 22  $\mu H$ 

- 1.  $V_{OUT} = 1.9 \text{ V (AC coupled)}, 50 \text{ mV/div}$
- 2.  $I_0 = 3.0 \text{ mA}$  to 30 mA

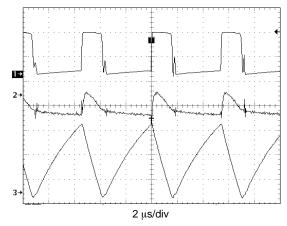
Figure 33. NCP1400ASN19T1 Load Transient Response



 $V_{in}$  = 1.5 V, L = 22  $\mu H$ 

- 1.  $V_{OUT} = 3.0 \text{ V (AC coupled)}, 50 \text{ mV/div}$
- 2.  $I_0 = 3.0 \text{ mA}$  to 30 mA

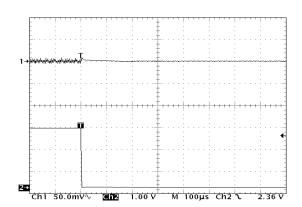
Figure 35. NCP1400ASN30T1 Load Transient Response



 $V_{OUT}$  = 3.0 V,  $V_{in}$  = 1.2 V,  $I_{O}$  = 25 mA., L = 22  $\mu H,\,C_{OUT}$  = 68  $\mu F$ 

- 1. V<sub>LX</sub>, 2.0 V/div
- 2. V<sub>OUT</sub>, 20 mV/div, AC coupled
- 3. I<sub>L</sub>, 100 mA/div

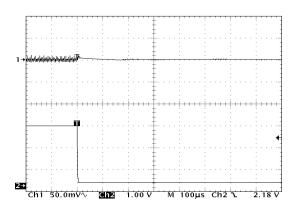
Figure 32. Operating Waveforms (Heavy Load)



 $V_{in}$  = 1.2 V, L = 22  $\mu H$ 

- 1.  $V_{OUT} = 1.9 \text{ V (AC coupled)}, 50 \text{ mV/div}$
- 2.  $I_0 = 30 \text{ mA to } 3.0 \text{ mA}$

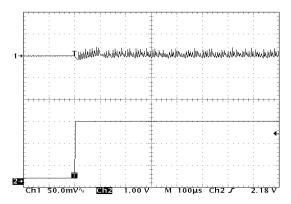
Figure 34. NCP1400ASN19T1 Load Transient Response



 $V_{in}$  = 1.5 V, L = 22  $\mu H$ 

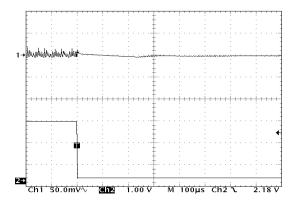
- 1.  $V_{OUT} = 3.0 \text{ V (AC coupled)}, 50 \text{ mV/div}$
- 2.  $I_0 = 30 \text{ mA to } 3.0 \text{ mA}$

Figure 36. NCP1400ASN30T1 Load Transient Response



- $$\begin{split} &V_{in}=1.5~\text{V, L}=22~\mu\text{H}\\ &1.~V_{OUT}=5.0~\text{V (AC coupled), 50 mV/div}\\ &2.~I_{O}=3.0~\text{mA to 30 mA} \end{split}$$

Figure 37. NCP1400ASN50T1 **Load Transient Response** 



- $$\begin{split} &V_{in}=1.5 \text{ V, L}=22 \text{ }\mu\text{H}\\ &1. &V_{OUT}=5.0 \text{ V (AC coupled), 50 mV/div}\\ &2. &I_{O}=30 \text{ mA to } 3.0 \text{ mA} \end{split}$$

Figure 38. NCP1400ASN50T1 **Load Transient Response** 

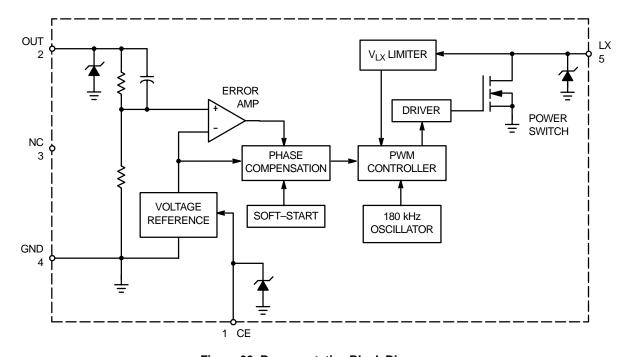


Figure 39. Representative Block Diagram

#### PIN FUNCTION DESCRIPTION

Pin #	Symbol	Pin Description	
1	CE	Chip Enable Pin (1) The chip is enabled if a voltage equal to or greater than 0.9 V is applied. (2) The chip is disabled if a voltage less than 0.3 V is applied. (3) The chip is enabled if this pin is left floating.	
2	OUT	Output voltage monitor pin and also the power supply for the device.	
3	NC	No internal connection to this pin.	
4	GND	Ground pin.	
5	LX	External inductor connection pin to power switch drain.	

#### **DETAILED OPERATING DESCRIPTION**

#### Operation

The NCP1400A series are monolithic power switching regulators optimized for applications where power drain must be minimized. These devices operate as fixed frequency, voltage mode boost regulator and is designed to operate in the discontinuous conduction mode. Potential applications include low powered consumer products and battery powered portable products.

The NCP1400A series are low noise fixed frequency voltage–mode PWM DC–DC converters, and consist of soft–start circuit, feedback resistor, reference voltage, oscillator, loop compensation network, PWM control circuit, current limit circuit and power switch. Due to the on–chip feedback resistor and loop compensation network, the system designer can get the regulated output voltage from 1.8 V to 5.0 V with a small number of external components. The quiescent current is typically 32  $\mu A$  (VOUT = 2.7 V), and can be further reduced to about 1.5  $\mu A$  when the chip is disabled (VCE < 0.3 V).

#### **Soft Start**

There is a soft start circuit in NCP1400A. When power is applied to the device, the soft start circuit pumps up the output voltage to approximately 1.5 V at a fixed duty cycle, the level at which the converter can operate normally. What is more, the start—up capability with heavy loads is also improved.

#### Oscillator

The oscillator frequency is internally set to 180 kHz at an accuracy of  $\pm 20\%$  and with low temperature coefficient of 0.11%/°C. Figure 15 and 16 illustrate oscillator frequency versus temperature.

### Regulated Converter Voltage (VOUT)

The  $V_{OUT}$  is set by an internal feedback resistor network. This is trimmed to a selected voltage from 1.8 V to 5.0 V range in 100 mV steps with an accuracy of  $\pm 2.5\%$ .

#### Compensation

The device is designed to operate in discontinuous conduction mode. An internal compensation circuit was designed to guarantee stability over the full input/output voltage and full output load range. Stability cannot be guaranteed in continuous conduction mode.

#### **Current Limit**

The NCP1400A series utilizes cycle-by-cycle current limiting as a means of protecting the output switch MOSFET from overstress and preventing the small value inductor from saturation. Current limiting is implemented by monitoring the output MOSFET current build-up during conduction, and upon sensing an overcurrent conduction immediately turning off the switch for the duration of the oscillator cycle.

The voltage across the output MOSFET is monitored and compared against a reference by the VLX limiter. When the threshold is reached, a signal is sent to the PWM controller block to terminate the output switch conduction. The current limit threshold is typically set at 350 mA.

#### **Enable/Disable Operation**

The NCP1400A series offer IC shutdown mode by chip enable pin (CE pin) to reduce current consumption. An internal pull–up resistor tied the CE pin to OUT pin by default, i.e., user can float the pin CE for permanent "On". When voltage at pin CE is equal or greater than 0.9 V, the chip will be enabled, which means the regulator is in normal operation. When voltage at pin CE is less than 0.3 V, the chip is disabled, which means IC is shutdown.

Important: DO NOT apply a voltage between 0.3 V to 0.9 V to pin CE as this voltage will place the IC into an undefined state and the IC may drain excessive current from the supply.

#### **APPLICATION CIRCUIT INFORMATION**

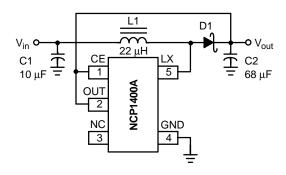


Figure 40. Typical Step-Up Converter Application

#### Step-up Converter Design Equations

General step-up DC-DC converter designed to operate in discontinuous conduction mode can be defined by:

Calculation	Equation
D	t <sub>on</sub> t
I <sub>PK</sub>	$\frac{V_{in}t_{on}}{L}$
Io	$\frac{(V_{in})^{2}(t_{on})^{2}f}{2L(V_{out} + V_{F} - V_{in})}$

#### NOTES:

D – Duty cycle

I<sub>PK</sub> - Peak inductor current

I<sub>O</sub> – Desired dc output current

Vin - Nominal operating dc input voltage

Vout - Desired dc output voltage

V<sub>F</sub> – Diode forward voltage

Assume saturation voltage of the internal FET switch is negligible.

#### **External Component Selection**

#### Inductor

Inductance values between 18  $\mu H$  and 27  $\mu H$  are the best suitable values for NCP1400A. In general, smaller inductance values can provide larger peak inductor current and output current capability, and lower conversion efficiency, and vice versa. Select an inductor with smallest possible ESR, usually less than 1.0  $\Omega$  to minimize loss. It is necessary to choose an inductor with saturation current greater than the peak current which the inductor will encounter in the application.

#### Diode

The diode is the largest source of loss in DC-DC converters. The most importance parameters which affect

their efficiency are the forward voltage drop,  $V_F$ , and the reverse recovery time, trr. The forward voltage drop creates a loss just by having a voltage across the device while a current flowing through it. The reverse recovery time generates a loss when the diode is reverse biased, and the current appears to actually flow backwards through the diode due to the minority carriers being swept from the P–N junction. A schottky diode with the following characteristics is recommended:

Small forward voltage,  $V_F < 0.3 \text{ V}$ 

Small reverse leakage current

Fast reverse recovery time/switching speed

Rated current larger than peak inductor current,

 $I_{rated} > I_{PK}$ 

Reverse voltage larger than output voltage.

 $V_{reverse} > V_{out}$ 

#### **Input Capacitor**

The input capacitor (optional) can stabilize the input voltage and minimize peak current ripple from the source. The value of the capacitor depends on the impedance of the input source used. Small ESR (Equivalent Series Resistance) Tantalum or ceramic capacitor with value of  $10~\mu F$  should be suitable.

#### **Output Capacitor**

The output capacitor is used for sustaining the output voltage when the internal MOSFET is switched on and smoothing the ripple voltage. Low ESR capacitor should be used to reduce output ripple voltage. In general, a 47  $\mu F$  to 68  $\mu F$  low ESR (0.15  $\Omega$  to 0.30  $\Omega$ ) Tantalum capacitor should be appropriate. For applications where space is a critical factor, two parallel 22  $\mu F$  low profile SMD ceramic capacitors can be used.

An evaluation board of NCP1400A has been made in the small size of 23 mm x 20 mm and is shown in Figures 41 and 42. Please contact your ON Semiconductor representative

for availability. The evaluation board schematic diagram, the artwork and the silkscreen of the surface mount PCB are shown below:

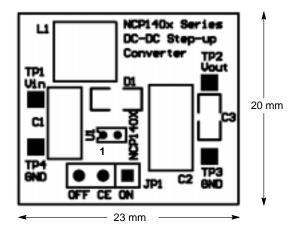


Figure 41. NCP1400A PWM Step-up DC-DC Converter Evaluation Board Silkscreen

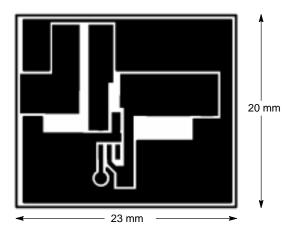


Figure 42. NCP1400A PWM Step-up DC-DC Converter Evaluation Board Artwork (Component Side)

#### **Components Supplier**

Parts	Supplier	Part Number	Description	Phone
Inductor, L1	Sumida Electric Co. Ltd.	CD54-220K	Inductor 22 μH/1.11 A	(852) 2880–6688
Schottky Diode, D1	ON Semiconductor Corp.	MBR0520LT1	Schottky Power Rectifier	(852) 2689–0088
Output Capacitor, C2	KEMET Electronics Corp.	T494D686K010AS	Low ESR Tantalum Capacitor 68 μF/10 V	(852) 2305–1168
Input Capacitor, C1	KEMET Electronics Corp.	T491C106K016AS	Low Profile Tantalum Capacitor 10 μF/16 V	(852) 2305–1168

#### **PCB Layout Hints**

#### Grounding

One point grounding should be used for the output power return ground, the input power return ground, and the device switch ground to reduce noise as shown in Figure 43, e.g.: C2 GND, C1 GND, and U1 GND are connected at one point in the evaluation board. The input ground and output ground traces must be thick enough for current to flow through and for reducing ground bounce.

#### **Power Signal Traces**

Low resistance conducting paths should be used for the power carrying traces to reduce power loss so as to improve efficiency (short and thick traces for connecting the inductor L can also reduce stray inductance), e.g.: short and thick traces listed below are used in the evaluation board:

- 1. Trace from TP1 to L1
- 2. Trace from L1 to Lx pin of U1
- 3. Trace from L1 to anode pin of D1
- 4. Trace from cathode pin of D1 to TP2

#### **Output Capacitor**

The output capacitor should be placed close to the output terminals to obtain better smoothing effect on the output ripple.

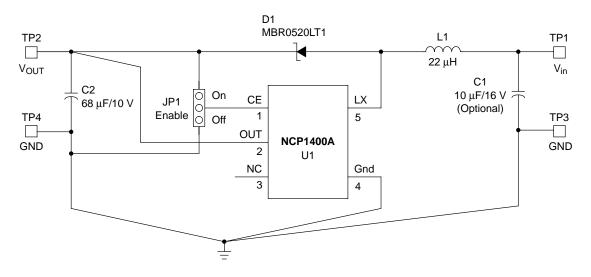
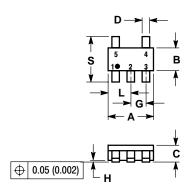
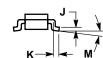


Figure 43. NCP1400A Evaluation Board Schematic Diagram

## **PACKAGE DIMENSIONS**

TSOP-5 **SN SUFFIX** CASE 483-01 ISSUE A





- NOTES:
  1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
  2. CONTROLLING DIMENSION: MILLIMETER.
  3. MAXIMUM LEAD THICKNESS INCLUDES LEAD FINISH THICKNESS. MINIMUM LEAD THICKNESS IS THE MINIMUM THICKNESS OF BASE MATERIAL.

	MILLIN	IETERS	INC	HES
DIM	MIN	MAX	MIN	MAX
Α	2.90	3.10	0.1142	0.1220
В	1.30	1.70	0.0512	0.0669
C	0.90	1.10	0.0354	0.0433
D	0.25	0.50	0.0098	0.0197
G	0.85	1.00	0.0335	0.0413
Н	0.013	0.100	0.0005	0.0040
J	0.10	0.26	0.0040	0.0102
K	0.20	0.60	0.0079	0.0236
L	1.25	1.55	0.0493	0.0610
M	0 °	10°	0°	10°
S	2.50	3.00	0.0985	0.1181

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