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### 2-Phase Stepper-Motor Driver

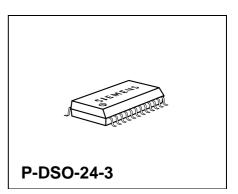
# TLE 4726

**Bipolar IC** 

#### Overview

### Features

- 2 × 0.75 A / 50 V outputs
- Integrated driver, control logic and current control (chopper)
- Fast free-wheeling diodes
- Low standby-current drain
- Full, half, quarter, mini step



Туре	Ordering Code	Package
TLE 4726 G	Q67006-A9297	P-DSO-24-3

### Description

TLE 4726 is a bipolar, monolithic IC for driving bipolar stepper motors, DC motors and other inductive loads that operate on constant current. The control logic and power output stages for two bipolar windings are integrated on a single chip which permits switched current control of motors with 0.75 A per phase at operating voltages up to 50 V.

The direction and value of current are programmed for each phase via separate control inputs. A common oscillator generates the timing for the current control and turn-on with phase offset of the two output stages. The two output stages in a full-bridge configuration have integrated, fast free-wheeling diodes and are free of crossover current. The logic is supplied either separately with 5 V or taken from the motor supply voltage by way of a series resistor and an integrated Z-diode. The device can be driven directly by a microprocessor with the possibility of all modes from full step through half step to mini step.

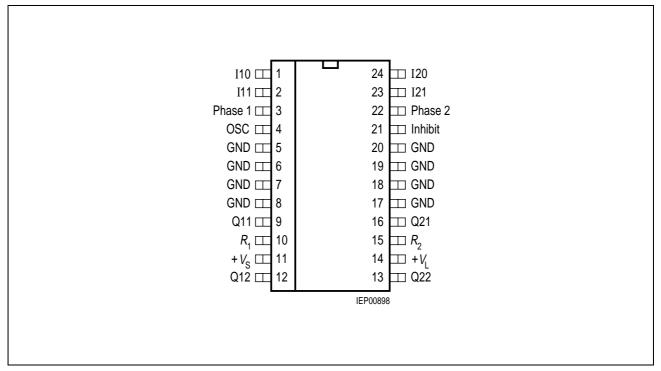


Figure 1 Pin Configuration (top view)

### Pin Definitions and Functions

Pin No.	Functio	on						
1, 2, 23, 24	<b>Digital</b> particul			<b>), IX1</b> for the mag	nitude of the <b>current</b> of the			
	IX1	IX0	Phase Current	Example of Motor Status	_			
	Н	Н	0	No current	_			
	Н	L	1/3 I <sub>max</sub>	Hold	typical $I_{max}$ with			
	L	Н	2/3 I <sub>max</sub>	Set	$R_{\text{sense}} = 1 \ \Omega$ : 750 mA			
	L	L	I <sub>max</sub>	Accelerate	_			
3	•	ntial the	phase curr	0	phase winding 1. On 1 to Q12, on L-potential in			
5, 6, 7, 8, 17, 18, 19, 20	Ground	<b>l</b> ; all pi	ns are conne	ected internally.				
4	<b>Oscilla</b> 2.2 nF.	tor; wo	rks at appro	x. 25 kHz if this p	in is wired to ground across			
10	Resisto	<b>or</b> <i>R</i> <sub>1</sub> fc	r sensing th	e current in phase	e 1.			
9, 12	Push-p diodes.	ull out	puts Q11, C	<b>212</b> for phase 1 w	ith integrated free-wheeling			
11		electrol	tic capacito	-	as possible to the IC, with a in parallel with a ceramic			
14	a series block to	s resiste groun	or. A Z-diode	e of approx. 7 V is	V or connect to + $V_{\rm S}$ across s integrated. In both cases ble electrolytic capacitor of 100 nF.			
13, 16	Push-p diodes.	ull out	puts Q22, 0	<b>221</b> for phase 2 w	ith integrated free-wheeling			
15	Resiste	<b>or</b> <i>R</i> <sub>2</sub> fc	r sensing th	e current in phase	e 2.			
21		•			by low potential on this pin. tantially.			
22	H-poter	This reduces the current consumption substantially. <b>Input phase 2</b> ; controls the current flow through phase winding 2. On H-potential the phase current flows from Q21 to Q22, on L potential in the reverse direction.						

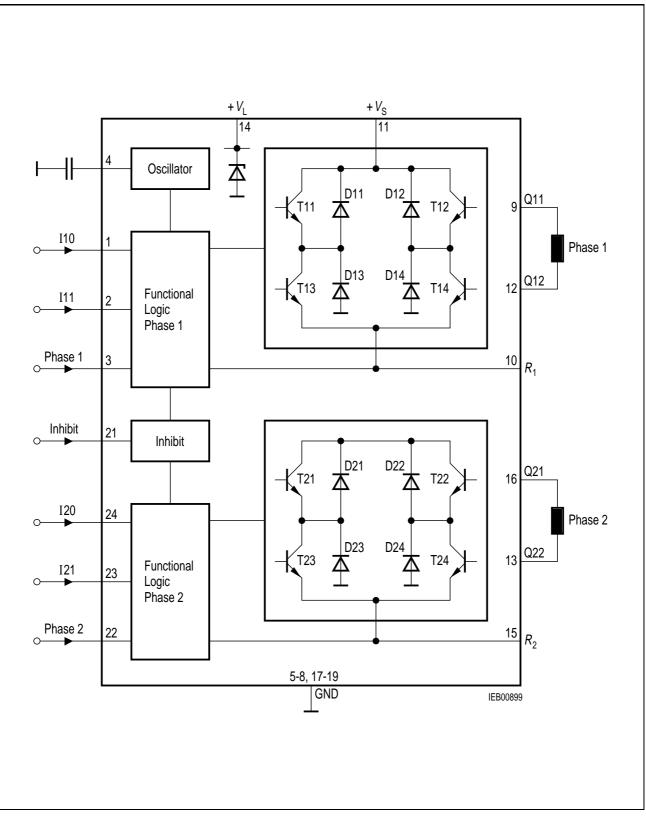


Figure 2 Block Diagram

### **Absolute Maximum Ratings**

### $T_{\rm A}$ = - 40 to 125 °C

Parameter	Symbol	Limit	Values	Unit	Remarks
		min.	max.		
Supply voltage	Vs	0	52	V	_
Logic supply voltage	$V_{L}$	0	6.5	V	Z-diode
Z-current of V <sub>L</sub>	IL	-	50	mA	-
Output current	IQ	- 1	1	А	-
Ground current	I <sub>GND</sub>	- 2	2	А	-
Logic inputs	V <sub>lxx</sub>	- 6	V <sub>L</sub> + 0.3	V	<i>I</i> <sub>XX</sub> ; Phase 1, 2; Inhibit
$R_1, R_2$ , oscillator input voltage	$V_{\rm RX,}$ $V_{\rm OSC}$	- 0.3	V <sub>L</sub> + 0.3	V	-
Junction temperature	$egin{array}{c} T_{\mathrm{j}} \ T_{\mathrm{j}} \end{array}$	-	125 150	°C °C	– max. 1,000 h
Storage temperature	T <sub>stg</sub>	- 50	125	°C	_

### **Operating Range**

Parameter	Symbol	Limit	Values	Unit	Remarks
		min.	max.		
Supply voltage	Vs	5	50	V	-
Logic supply voltage	VL	4.5	6.5	V	without series resistor
Case temperature	T <sub>C</sub>	- 25	110	°C	measured on pin 5 $P_{diss} = 2 W$
Output current	I <sub>Q</sub>	- 800	800	mA	-
Logic inputs	V <sub>IXX</sub>	- 5	VL	V	I <sub>XX</sub> ; Phase 1, 2; Inhibit

### **Thermal Resistances**

Junction ambient	R <sub>th ja</sub>	_	75	K/W	P-DSO-24-3
Junction ambient (soldered on a	$R_{\rm thja}$	_	50	K/W	P-DSO-24-3
35 μm thick					
20 cm <sup>2</sup> PC boar					
copper area)					
Junction case	$R_{\rm thjc}$	_	15	K/W	measured on
					pin 5
					P-DSO-24-3

### Characteristics

 $V_{\rm S}$  = 40 V;  $V_{\rm L}$  = 5 V; - 25 °C  $\leq T_{\rm j} \leq$  125 °C

Parameter	Symbol	Limit Values			Unit	Test Condition
		min. typ. max.				

### **Current Consumption**

from + $V_{\rm S}$	Is	_	0.2	0.5	mA	$V_{\rm inh} = L$
from + $V_{\rm S}$	I <sub>S</sub>	-	16	20	mA	$V_{\text{inh}} = H$ $I_{\text{Q1/2}} = 0, I_{\text{XX} = L}$
	-				_	$I_{Q1/2} = 0, I_{XX = L}$
from + $V_{L}$	IL	-	1.7	3	mA	$V_{\rm inh} = L$
from + $V_{\rm L}$	IL	—	18	25	mΑ	$V_{\rm inh} = H$
						$I_{Q1/2} = 0, I_{XX = L}$

### Characteristics (cont'd)

 $V_{\rm S}$  = 40 V;  $V_{\rm L}$  = 5 V; - 25 °C  $\leq T_{\rm I} \leq$  125 °C

Parameter Symbol		L	imit Va	lues	Unit	<b>Test Condition</b>
		min.	typ.	max.		
Oscillator		1		-		
Output charging current	I <sub>OSC</sub>	-	110	-	μA	-
Charging threshold	VOSCL	_	1.3	_	V	_
Discharging threshold	V <sub>OSCH</sub>	-	2.3	-	V	_
Frequency	$f_{OSC}$	18	25	40	kHz	$C_{\rm OSC}$ = 2.2 nF

### Phase Current Selection Current Limit Threshold

No current	V <sub>sense n</sub>	_	0	_	mV	IX0 = H; IX1 = H
Hold	$V_{sense h}$	200	250	300	mV	IX0 = L; IX1 = H
Setpoint	V <sub>sense s</sub>	420	540	680	mV	IX0 = H; IX1 = L
Accelerate	$V_{\rm sense}$ a	700	825	950	mV	IX0 = L; IX1 = L

### Logic Inputs

 $(I_{X1}; I_{X0}; Phase x)$ 

Threshold	$V_{\parallel}$	1.4	_	2.3	V	-
	-	(H→L)		(L→H)		
L-input current	$I_{\rm IL}$	- 10	-	—	μA	$V_{ } = 1.4 \text{ V}$
L-input current	$I_{  }$	- 100	-	—	μA	$V_{\rm I} = 0  \rm V$
H-input current	I <sub>IH</sub>	_	_	10	μA	$V_{1} = 5 V$

### Characteristics (cont'd)

 $V_{\rm S} = 40$  V;  $V_{\rm I} = 5$  V;  $-25 \,{}^{\circ}{\rm C} \le T_{\rm I} \le 125 \,{}^{\circ}{\rm C}$ 

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		

### Standby Cutout (inhibit)

Threshold	V <sub>Inh</sub>	2	3	4	V	-
Threshold	(L→H) V <sub>Inh</sub>	1.7	2.3	2.9	V	_
Hysteresis	(H→L) V <sub>Inhhy</sub>	0.3	0.7	1.1	V	_

### Internal Z-Diode

Z-voltage	V <sub>LZ</sub>	6.5	7.4	8.2	V	<i>I</i> <sub>L</sub> = 50 mA
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### **Power Outputs**

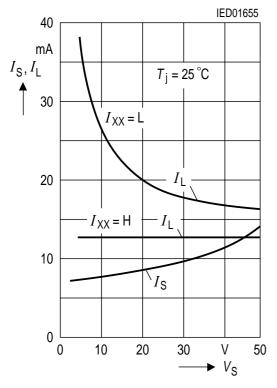
### Diode Transistor Sink Pair (D13, T13; D14, T14; D23, T23; D24, T24)

Saturation voltage	V .	_	0.3	0.6	V	$I_{\rm Q} = -0.5  {\rm A}$
•	v satl			1	V	$I_{\rm Q} = -0.75 \text{A}$
Saturation voltage	V satl		0.5	1	V,	34
Reverse current	I <sub>RI</sub>	-	—	300	μA	$V_{\rm Q} = 40 \text{ V}$
Forward voltage	$V_{FI}$	-	0.9	1.3	V	$I_{\rm Q} = 0.5  {\rm A}$
Forward voltage	$V_{FI}$	-	1	1.4	V	<i>I</i> <sub>Q</sub> = 0.75 A

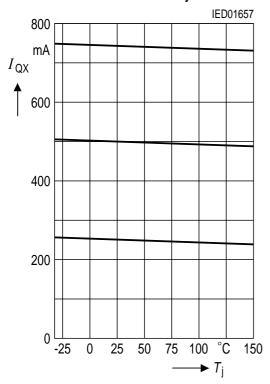
### Diode Transistor Source Pair (D11, T11; D12, T12; D21, T21; D22, T22)

Saturation voltage	V <sub>satuC</sub>	_	0.9	1.2	V	<i>I</i> <sub>Q</sub> = 0.5 A;
Saturation voltage	V		0.3	0.7	V	charge $I_{\Omega} = 0.5 \text{ A};$
Saturation voltage	V <sub>satuD</sub>	_	0.5	0.7	v	discharge
Saturation voltage	$V_{satuC}$	-	1.1	1.4	V	I <sub>Q</sub> = 0.75 A;
	17		0.5		.,	charge
Saturation voltage	V <sub>satuD</sub>	-	0.5	1	V	$I_{\rm Q} = 0.75 \text{ A};$ discharge
Reverse current	I <sub>Ru</sub>	_	_	300	μA	$V_{\rm Q} = 0  \rm V$
Forward voltage	$V_{Fu}$	_	1	1.3	V	$I_{Q} = -0.5 \text{ A}$
Forward voltage	$V_{Fu}$	-	1.1	1.4	V	$I_{\rm Q} = -0.75  {\rm A}$
Diode leakage current	I <sub>SL</sub>	—	1	2	mA	$I_{\rm F} = -0.75  {\rm A}$

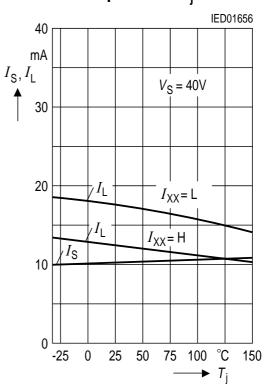
Quiescent Current  $I_{\rm S}, I_{\rm L}$  versus Supply Voltage  $V_{\rm S}$ 



# Output Current $I_{QX}$ versus Junction Temperature $T_i$



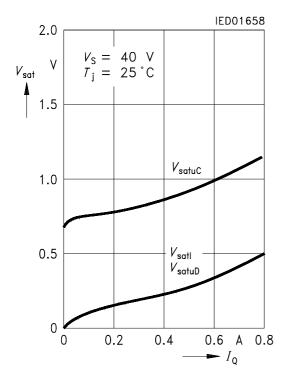
Quiescent Current  $I_{\rm S}$ ,  $I_{\rm L}$  versus Junction Temperature  $T_{\rm j}$ 



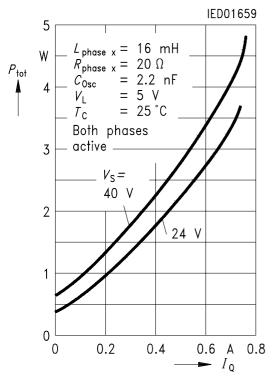
### **Operating Condition:**

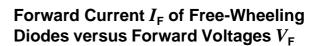
 $\begin{array}{ll} V_{\rm L} &= 5 \ {\rm V} \\ V_{\rm lnh} &= {\rm H} \\ C_{\rm OSC} &= 2.2 \ {\rm nF} \\ R_{\rm sense} &= 1 \ \Omega \\ {\rm Load:} \ {\rm L} = 10 \ {\rm mH} \\ R = 2.4 \ \Omega \\ f_{\rm phase} &= 50 \ {\rm Hz} \\ {\rm mode:} \ {\rm full step} \end{array}$ 

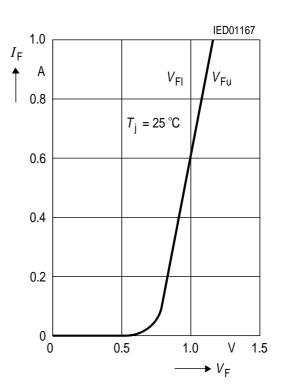
# Output Saturation Voltages $V_{sat}$ versus Output Current $I_{Q}$



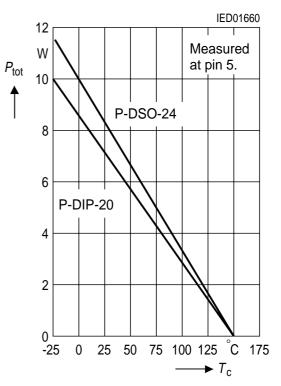
### Typical Power Dissipation $P_{tot}$ versus Output Current $I_Q$ (Non Stepping)



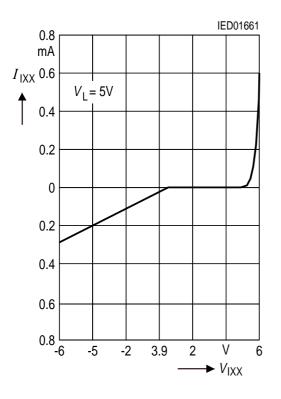




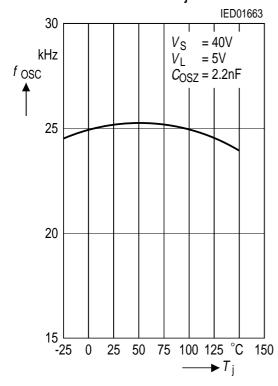
# Permissible Power Dissipation $P_{tot}$ versus Case Temperature $T_{C}$



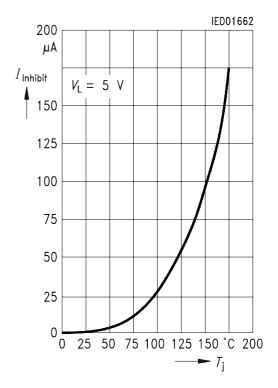
Input Characteristics of  $I_{xx}$ , Phase X, Inhibit

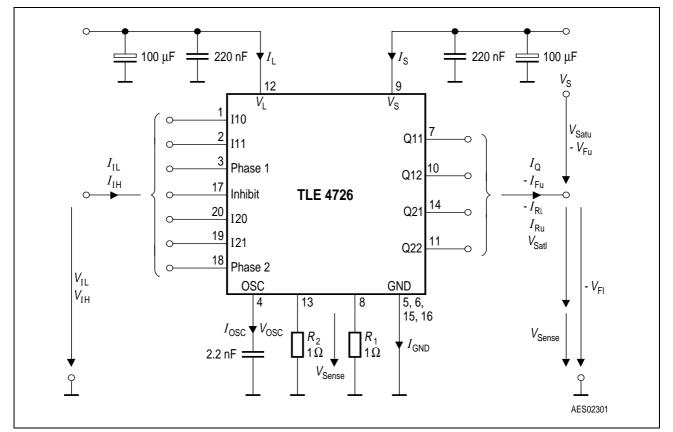


# Oscillator Frequency $f_{\rm OSC}$ versus Junction Temperature $T_{\rm j}$



# Input Current of Inhibit versus Junction Temperature $T_{i}$







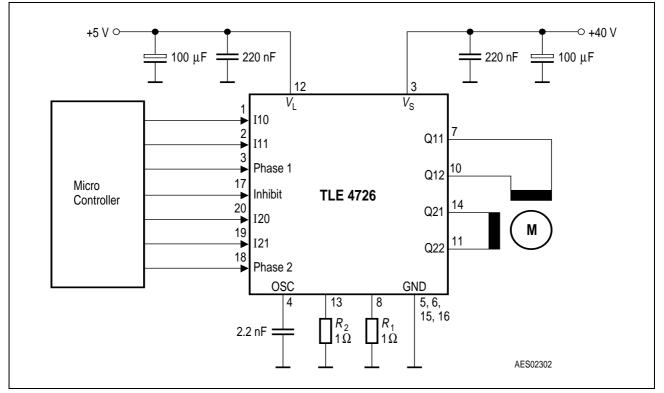
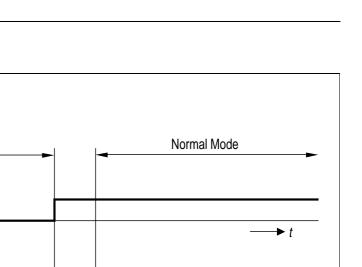
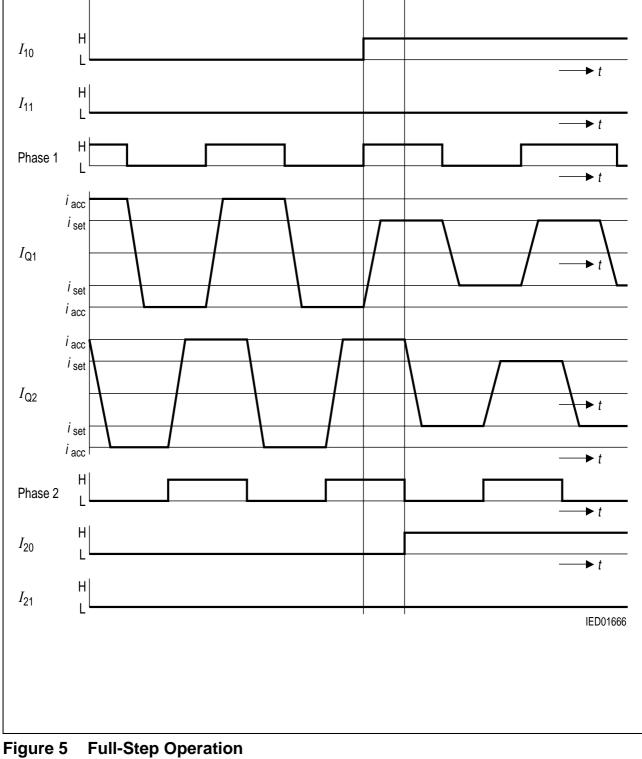


Figure 4 Application Circuit





Accelerate Mode

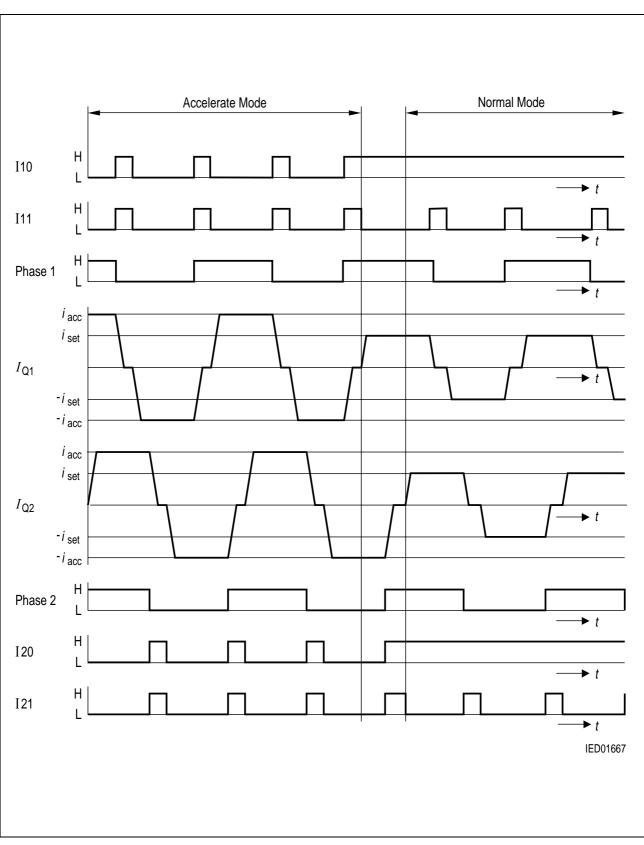


Figure 6 Half-Step Operation

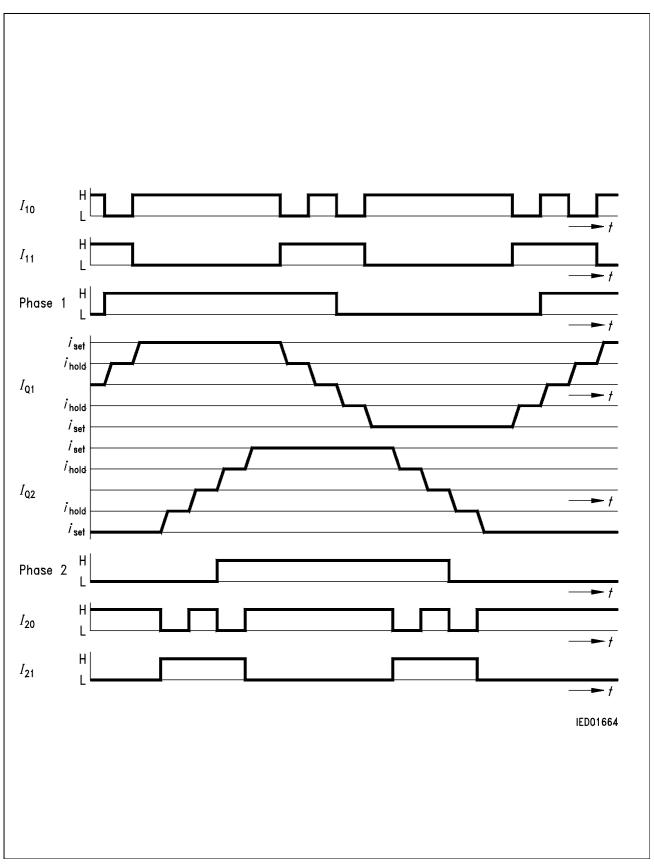
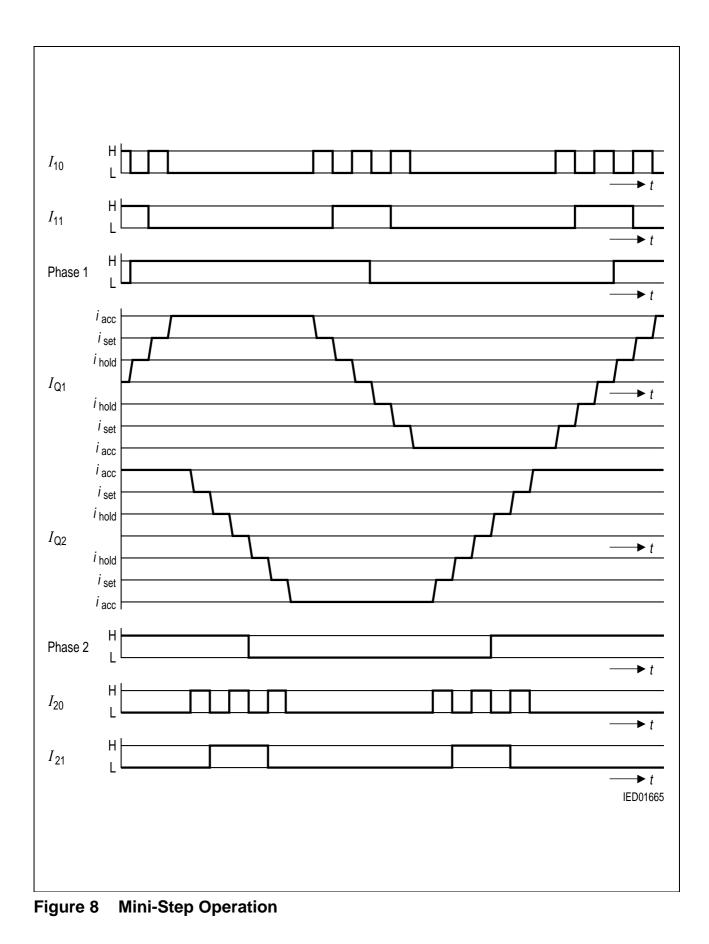


Figure 7 Quarter-Step Operation



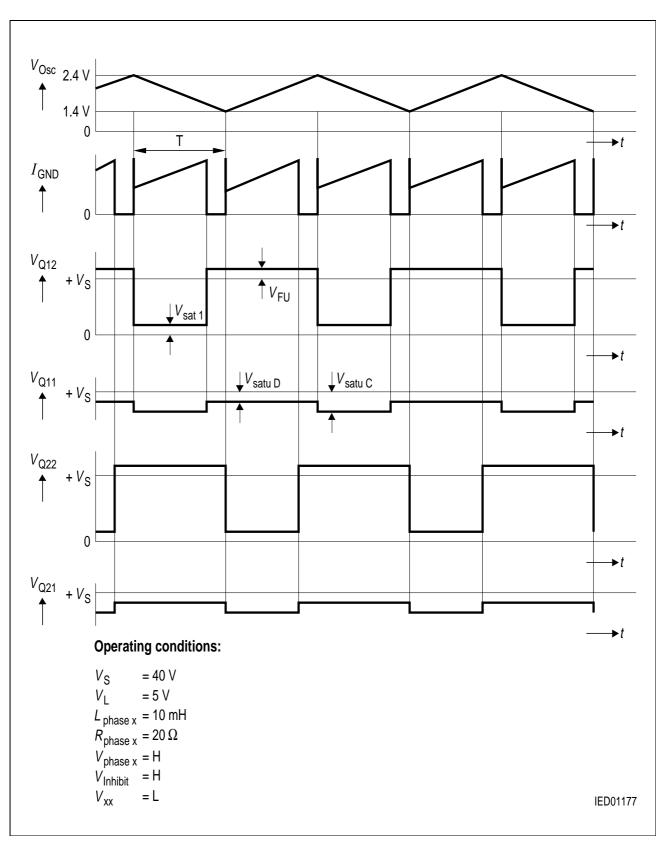


Figure 9 Current Control

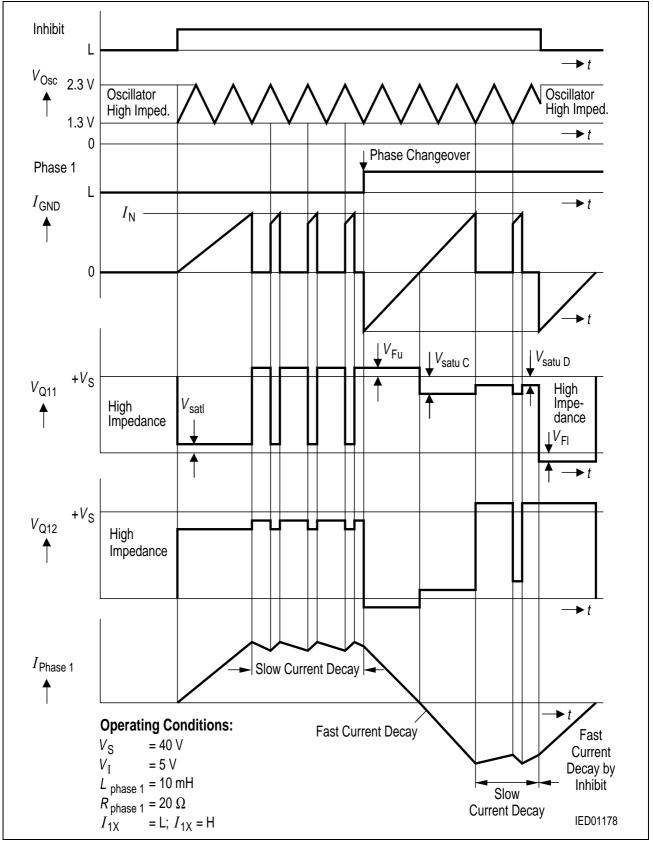


Figure 10 Phase Reversal and Inhibit

### **Calculation of Power Dissipation**

The total power dissipation  $P_{tot}$  is made up of

saturation losses $P_{sat}$	(transistor saturation voltage and diode forward voltages),
quiescent losses $P_q$	(quiescent current times supply voltage) and
switching losses P <sub>s</sub>	(turn-ON / turn-OFF operations).

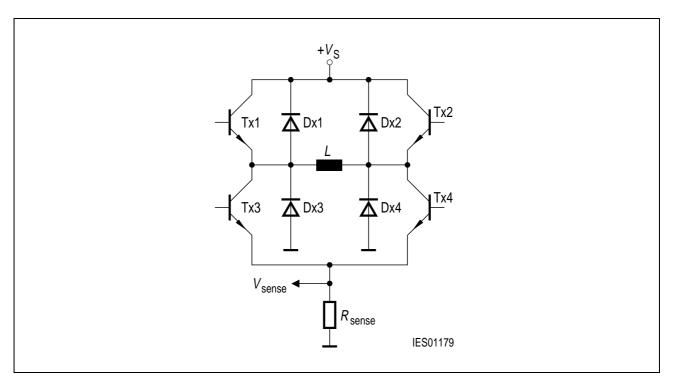
The following equations give the power dissipation for chopper operation without phase reversal. This is the worst case, because full current flows for the entire time and switching losses occur in addition.

$$P_{\text{tot}} = 2 \times P_{\text{sat}} + P_{\text{q}} + 2 \times P_{\text{s}}$$
where
$$P_{\text{sat}} \cong I_{\text{N}} \{ V_{\text{satl}} \times d + V_{\text{Fu}} (1 - d) + V_{\text{satuC}} \times d + V_{\text{satuD}} (1 - d) \}$$

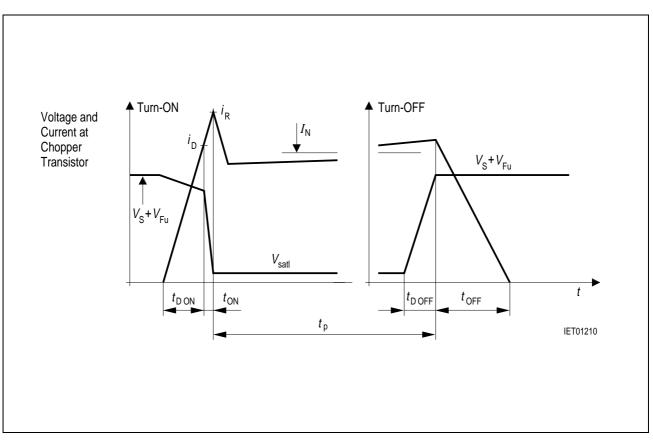
$$P_{\text{q}} = I_{\text{q}} \times V_{\text{S}} + I_{\text{L}} \times V_{\text{L}}$$

$$P_{\text{S}} \cong \frac{V_{\text{S}}}{T} \left\{ \frac{i_{\text{D}} \times t_{\text{DON}}}{2} + \frac{i_{\text{D}} + i_{\text{R}} \times t_{\text{ON}}}{4} + \frac{I_{\text{N}}}{2} t_{\text{DOFF}} + t_{\text{OFF}} \right\}$$

- $I_{\rm N}$  = nominal current (mean value)
- $I_q$  = quiescent current
- $\dot{i_D}$  = reverse current during turn-on delay
- $i_{\rm R}$  = peak reverse current
- $t_{p}$  = conducting time of chopper transistor
- $\dot{t}_{ON}$  = turn-ON time
- $t_{OFF}$  = turn-OFF time
- $t_{\text{DON}}$  = turn-ON delay
- $t_{DOFF}$  = turn-OFF delay
- T = cycle duration
- $d = \text{duty cycle } t_{\text{p}}/T$
- $V_{\text{satl}}$  = saturation voltage of sink transistor (T3, T4)
- $V_{\text{satuC}}$  = saturation voltage of source transistor (T1, T2) during charge cycle
- $V_{satuD}$  = saturation voltage of source transistor (T1, T2) during discharge cycle
- $V_{Fu}$  = forward voltage of free-wheeling diode (D1, D2)
- $V_{\rm S}$  = supply voltage
- $V_{\rm L}$  = logic supply voltage
- $I_{\rm L}$  = current from logic supply



### Figure 11



### Figure 12

### **Application Hints**

The TLE 4726 is intended to drive both phases of a stepper motor. Special care has been taken to provide high efficiency, robustness and to minimize external components.

### Power Supply

The TLE 4726 will work with supply voltages ranging from 5 V to 50 V at pin  $V_{\rm S}$ . As the circuit operates with chopper regulation of the current, interference generation problems can arise in some applications. Therefore the power supply should be decoupled by a 0.22  $\mu$ F ceramic capacitor located near the package. Unstabilized supplies may even afford higher capacities.

### **Current Sensing**

The current in the windings of the stepper motor is sensed by the voltage drop across  $R_1$  and  $R_2$ . Depending on the selected current internal comparators will turn off the sink transistor as soon as the voltage drop reaches certain thresholds (typical 0 V, 0.25 V, 0.5 V and 0.75 V); ( $R_1$ ,  $R_2 = 1 \Omega$ ). These thresholds are neither affected by variations of  $V_L$  nor by variations of  $V_S$ .

Due to chopper control fast current rises (up to 10 A/ $\mu$ s) will occur at the sensing resistors  $R_1$  and  $R_2$ . To prevent malfunction of the current sensing mechanism  $R_1$  and  $R_2$  should be pure ohmic. The resistors should be wired to GND as directly as possible. Capacitive loads such as long cables (with high wire to wire capacity) to the motor should be avoided for the same reason.

### Synchronizing Several Choppers

In some applications synchrone chopping of several stepper motor drivers may be desireable to reduce acoustic interference. This can be done by forcing the oscillator of the TLE 4726 by a pulse generator overdriving the oscillator loading currents (approximately  $\check{S}\pm$  100 µA). In these applications low level should be between 0 V and 1 V while high level should be between 2.6 V and  $V_{\rm L}$ .

### **Optimizing Noise Immunity**

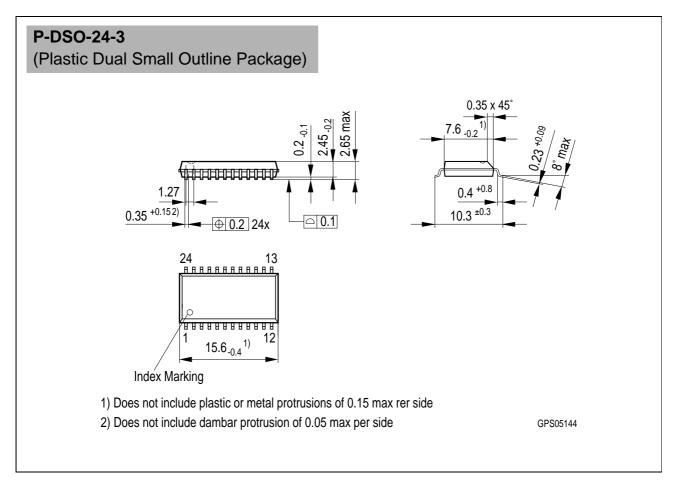
Unused inputs should always be wired to proper voltage levels in order to obtain highest possible noise immunity.

To prevent crossconduction of the output stages the TLE 4726 uses a special break before make timing of the power transistors. This timing circuit can be triggered by short glitches (some hundred nanoseconds) at the Phase inputs causing the output stage to become high resistive during some microseconds. This will lead to a fast current decay during that time. To achieve maximum current accuracy such glitches at the Phase inputs should be avoided by proper control signals.

#### Thermal Shut Down

To protect the circuit against thermal destruction, thermal shut down has been implemented. To provide a warning in critical applications, the current of the sensing element is wired to input Inhibit. Before thermal shut down occurs Inhibit will start to pull down by some hundred microamperes. This current can be sensed to build a temperature prealarm.

#### **Package Outlines**



Sorts of Packing Package outlines for tubes, trays etc. are contained in our Data Book "Package Information". SMD = Surface Mounted Device

Dimensions in mm