

## 16-A, 12-V INPUT NONISOLATED WIDE-OUTPUT ADJUST SIP MODULE

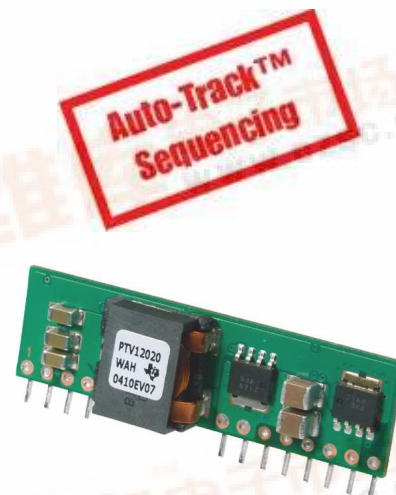


### FEATURES

- Up to 16-A Output Current
- 12-V Input Voltage
- Wide-Output Voltage Adjust (1.2 V to 5.5 V)/(0.8 V to 1.8 V)
- Efficiencies up to 93%
- On/Off Inhibit
- Output Voltage Sense
- Prebias Start Up
- Undervoltage Lockout
- Auto-Track™ Sequencing
- Output Overcurrent Protection (Nonlatching, Auto-Reset)
- Overtemperature Protection
- Operating Temperature: –40°C to 85°C
- Safety Agency Approvals: UL/cUL 60950, EN60950 VDE (Pending)
- POLA™ Alliance Compatible

### APPLICATIONS

- Multivoltage Digital Systems
- High-End Computing
- Networking
- 12-V Intermediate Bus Architectures



### DESCRIPTION

The PTV12020 series of nonisolated power modules are part of a new class of complete dc/dc switching regulator modules from Texas Instruments. These regulators combine high performance with double-sided, surface mount construction to give designers the flexibility to power the most complex multiprocessor digital systems using off-the-shelf catalog parts.

The PTV12020 series is produced in a 12-pin, single in-line pin (SIP) package. The SIP footprint minimizes board space, and offers an alternate package option for space conscious applications. Operating from a 12-V input bus, the series provides step-down conversion to a wide range of output voltages, at up to 16 A of output current. The output voltage of the W-suffix parts can be set to any value over the range of 1.2 V to 5.5 V. The L-suffix parts have an adjustment range of 0.8 V to 1.8 V. The output voltage is set using a single external resistor.

This series includes Auto-Track™. Auto-Track™ simplifies the task of supply-voltage sequencing in a power system by enabling the output voltage of multiple modules to accurately track each other, or any external voltage, during power up and power down.

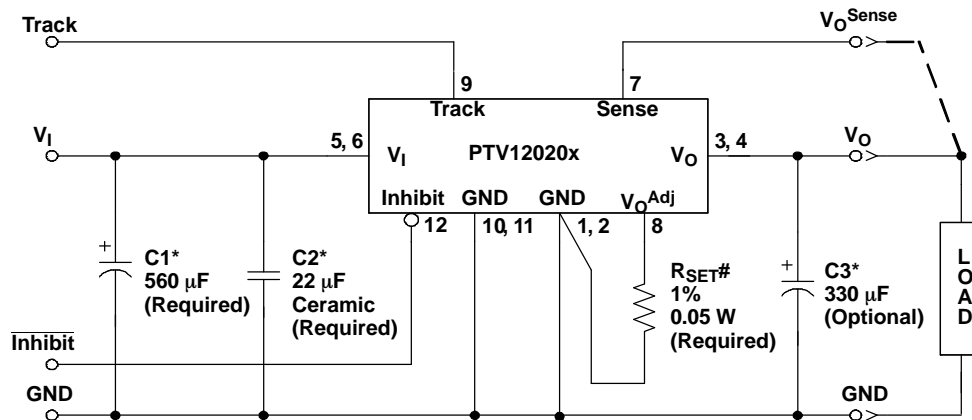
Other operating features include an on/off inhibit, and the ability to start up into an existing output voltage or prebias. For improved load regulation, an output voltage sense is provided. A nonlatching overcurrent trip and overtemperature shutdown protects against load faults.

Target applications include complex multivoltage, multiprocessor systems that incorporate the industry's high-speed DSPs, microprocessors, and bus drivers.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### STANDARD APPLICATION



\* See the Application Information section for capacitor recommendations.

#  $R_{SET}$  is required to adjust the output voltage higher than its lowest value. See the Application Information section for values.

### ORDERING INFORMATION

PTV12020 (Basic Model)			
Output Voltage	Part Number	DESCRIPTION	Package <sup>(1)</sup>
1.2 V – 5.5 V (Adjustable)	PTV12020WAH	Vertical T/H	EVC
0.8 V – 1.8 V (Adjustable)	PTV12020LAH	Vertical T/H	EVC

(1) See the applicable package drawing for dimensions and PC board layout.

### ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range unless otherwise noted<sup>(1)</sup>

		UNIT
$V_{(Track)}$	Track input	–0.3 V to $V_I$ +0.3 V
$T_A$	Operating temperature range	–40°C to 85°C
	Lead temperature	5 seconds
		260°C <sup>(2)</sup>
$T_{stg}$	Storage temperature	–40°C to 125°C
$V_{(Inhibit)}$	Inhibit (pin 12) input voltage	–0.3 V to 7 V

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) This product is not compatible with surface-mount reflow solder processes.

### PACKAGE SPECIFICATIONS

PTV12020x (Suffix AH)		
Weight		5.5 grams
Flammability	Meets UL 94 V-O	
Mechanical shock	Per Mil-STD-883D, Method 2002.3, 1 ms, 1/2 sine, mounted	500 Gs <sup>(1)</sup>
Mechanical vibration	Mil-STD-883D, Method 2007.2, 20 Hz - 2000 Hz	10 Gs <sup>(1)</sup>

(1) Qualification limit.

## ELECTRICAL CHARACTERISTICS

operating at 25°C free-air temperature,  $V_I = 12\text{ V}$ ,  $V_O = 3.3\text{ V}$ ,  $C_1 = 560\text{ }\mu\text{F}$ ,  $C_2 = 22\text{ }\mu\text{F}$ ,  $C_3 = 0\text{ }\mu\text{F}$ , and  $I_O = I_O\text{ max}$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	PTV12020W			UNIT
			MIN	TYP	MAX	
$I_O$	Output current	Natural convection airflow	0		16 <sup>(1)</sup>	A
$V_I$	Input voltage range	Over $I_O$ load range	10.8		13.2	V
$V_O$	Set-point voltage tolerance				$\pm 2\%$ <sup>(2)</sup>	
	Temperature variation	$-40^\circ\text{C} < T_A < 85^\circ\text{C}$		$\pm 0.5\%$		
	Line regulation	Over $V_I$ range		$\pm 5$		mV
	Load regulation	Over $I_O$ range		$\pm 10$		mV
	Total output variation	Includes set-point, line, load, $-40^\circ\text{C} \leq T_A \leq 85^\circ\text{C}$			$\pm 3$ <sup>(2)</sup>	% $V_O$
	Adjust range	Over $V_I$ range	1.2		5.5	V
$\eta$	Efficiency	$I_O = I_O\text{ max}$	$R_{SET} = 280\text{ }\Omega$ , $V_O = 5\text{ V}$		93%	
			$R_{SET} = 2.0\text{ k}\Omega$ , $V_O = 3.3\text{ V}$		91%	
			$R_{SET} = 4.32\text{ k}\Omega$ , $V_O = 2.5\text{ V}$		89%	
			$R_{SET} = 11.5\text{ k}\Omega$ , $V_O = 1.8\text{ V}$		86%	
			$R_{SET} = 24.3\text{ k}\Omega$ , $V_O = 1.5\text{ V}$		84%	
			$R_{SET} = \text{open cct.}$ , $V_O = 1.2\text{ V}$		81%	
	Output voltage ripple (pk-pk)	20-MHz bandwidth	$V_O \leq 2.5\text{ V}$		1	% $V_O$
			$V_O > 2.5\text{ V}$		1.5	
$I_O$ (trip)	Overcurrent threshold	Reset, followed by auto-recovery		30		A
	Transient response	1-A/ $\mu\text{s}$ load step, 50 to 100% $I_O\text{ max}$ , $C_3 = 330\text{ }\mu\text{F}$				
			Recovery time		70	$\mu\text{s}$
			$V_O$ over/undershoot		100	mV
	Track control (pin 9)	$I_{IL}$ Input low current	Pin to GND		-0.13	mA
		Control slew-rate limit	$C_3 \leq C_3\text{ (max)}$		1	V/ms
UVLO	Undervoltage lockout	$V_I$ increasing	9.5	10.4		V
		$V_I$ decreasing	8.8	9		
	Inhibit control (pin 12)	$V_{IH}$ Input high voltage	Referenced to GND		2	Open <sup>(3)</sup>
		$V_{IL}$ Input low voltage			-0.2	
		$I_{IL}$ Input low current	Pin to GND		-0.24	mA
$I_i$ (stby)	Input standby current	Inhibit (pin 12) to GND, Track (pin 9) open		10		mA
$f_s$	Switching frequency	Over $V_I$ and $I_O$ ranges	250	325	400	kHz
	External input capacitance	Nonceramic (C1)	560 <sup>(4)</sup>			$\mu\text{F}$
		Ceramic (C2)	22 <sup>(4)</sup>			
	External output capacitance (C3)	Capacitance value	Nonceramic	0	330 <sup>(5)</sup>	6,600 <sup>(6)</sup>
			Ceramic	0		300
		Equivalent series resistance (nonceramic)	4 <sup>(7)</sup>			m $\Omega$
MTBF	Reliability	Per Telcordia SR-332, 50% stress, $T_A = 40^\circ\text{C}$ , ground benign	4.9			$10^6\text{ Hrs}$

- (1) See thermal derating curves for safe operating area (SOA), or consult factory for appropriate derating.
- (2) The set-point voltage tolerance is affected by the tolerance and stability of  $R_{SET}$ . The stated limit is unconditionally met if  $R_{SET}$  has a tolerance of 1%, with 100 ppm/ $^\circ\text{C}$  or better temperature stability.
- (3) This control pin is pulled up to an internal supply voltage. To avoid risk of damage to the module, *do not* apply an external voltage greater than 7 V. If this input is left open-circuit, the module operates when input power is applied. A small low-leakage (<100 nA) MOSFET is recommended for control. For further information, consult the related application note.
- (4) A 22- $\mu\text{F}$  high-frequency ceramic capacitor and 560- $\mu\text{F}$  electrolytic input capacitor are required for proper operation. The electrolytic capacitor must be rated for the minimum ripple current rating. Consult the Application Information for further guidance on input capacitor selection.
- (5) An external output capacitor is not required for basic operation. Adding 330  $\mu\text{F}$  of distributed capacitance at the load improves the transient response.
- (6) This is the calculated maximum. The minimum ESR limitation often results in a lower value. Consult the Application Information for further guidance.
- (7) This is the typical ESR for all the electrolytic (nonceramic) output capacitance. Use 7 m $\Omega$  as the minimum when using max-ESR values to calculate.

## ELECTRICAL CHARACTERISTICS

operating at 25°C free-air temperature,  $V_I = 12\text{ V}$ ,  $V_O = 1.8\text{ V}$ ,  $C_1 = 560\text{ }\mu\text{F}$ ,  $C_2 = 22\text{ }\mu\text{F}$ ,  $C_3 = 0\text{ }\mu\text{F}$ , and  $I_O = I_O\text{ max}$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	PTV12020L			UNIT
			MIN	TYP	MAX	
$I_O$	Output current	Natural convection airflow	0		16 <sup>(1)</sup>	A
$V_I$	Input voltage range	Over $I_O$ load range	10.8		13.2	V
$V_O$	Set-point voltage tolerance				$\pm 2\%$ <sup>(2)</sup>	
	Temperature variation	$-40^\circ\text{C} < T_A < 85^\circ\text{C}$		$\pm 0.5\%$		
	Line regulation	Over $V_I$ range		$\pm 10$		mV
	Load regulation	Over $I_O$ range		$\pm 12$		mV
	Total output variation	Includes set-point, line, load, $-40^\circ\text{C} \leq T_A \leq 85^\circ\text{C}$			$\pm 3$ <sup>(2)</sup>	% $V_O$
	Adjust range	Over $V_I$ range	0.8		1.8	V
$\eta$	Efficiency	$I_O = I_O\text{ max}$	$R_{SET} = 130\text{ }\Omega$ , $V_O = 1.8\text{ V}$		87%	
			$R_{SET} = 3.57\text{ k}\Omega$ , $V_O = 1.5\text{ V}$		85%	
			$R_{SET} = 12.1\text{ k}\Omega$ , $V_O = 1.2\text{ V}$		83%	
			$R_{SET} = 32.4\text{ k}\Omega$ , $V_O = 1\text{ V}$		80%	
			$R_{SET} = \text{open cct.}$ , $V_O = 0.8\text{ V}$		77%	
	Output voltage ripple (pk-pk)	20-MHz bandwidth		2		% $V_O$
$I_O$ (trip)	Overcurrent threshold	Reset, followed by auto-recovery		30		A
	Transient response	1-A/ $\mu\text{s}$ load step, 50 to 100% $I_O\text{ max}$ , $C_3 = 330\text{ }\mu\text{F}$				
		Recovery time		70		$\mu\text{s}$
		$V_O$ over/undershoot		100		mV
	Track control (pin 9)	$I_{IL}$ Input low current	Pin to GND		-0.13	mA
		Control slew-rate limit	$C_3 \leq C_3\text{ (max)}$		1	V/ms
	Inhibit control (pin 12)	$V_{IH}$ Input high voltage	Referenced to GND	2	Open <sup>(3)</sup>	V
		$V_{IL}$ Input low voltage		-0.2	0.6	
		$I_{IL}$ Input low current	Pin to GND		-0.24	mA
$I_I$ (stby)	Input standby current	Inhibit (pin 12) to GND, Track (pin 9) open		10		mA
UVLO	Undervoltage lockout	$V_I$ increasing		9.5	10.4	V
		$V_I$ decreasing		8.8	9	
$f_S$	Switching frequency	Over $V_I$ and $I_O$ ranges		200	250 300	kHz
	External input capacitance	Nonceramic (C1)	560 <sup>(4)</sup>			$\mu\text{F}$
		Ceramic (C2)	22 <sup>(4)</sup>			
	External output capacitance (C3)	Capacitance value	Nonceramic	0	330 <sup>(5)</sup> 6,600 <sup>(6)</sup>	$\mu\text{F}$
			Ceramic	0	300	
		Equivalent series resistance (nonceramic)		4 <sup>(7)</sup>		m $\Omega$
MTBF	Reliability	Per Telcordia SR-332, 50% stress, $T_A = 40^\circ\text{C}$ , ground benign		4.9		$10^6\text{ Hrs}$

- (1) See thermal derating curves for safe operating area (SOA), or consult factory for appropriate derating.
- (2) The set-point voltage tolerance is affected by the tolerance and stability of  $R_{SET}$ . The stated limit is unconditionally met if  $R_{SET}$  has a tolerance of 1%, with 100 ppm/ $^\circ\text{C}$  or better temperature stability.
- (3) This control pin is pulled up to an internal supply voltage. To avoid risk of damage to the module, *do not* apply an external voltage greater than 7 V. If this input is left open-circuit, the module operates when input power is applied. A small low-leakage (<100 nA) MOSFET is recommended for control. For further information, consult the related application note.
- (4) A 22- $\mu\text{F}$  high-frequency ceramic capacitor and 560- $\mu\text{F}$  electrolytic input capacitor are required for proper operation. The electrolytic capacitor must be rated for the minimum ripple current rating. Consult the Application Information for guidance on input capacitor selection.
- (5) An external output capacitor is not required for basic operation. Adding 330  $\mu\text{F}$  of distributed capacitance at the load improves the transient response.
- (6) This is the calculated maximum. The minimum ESR limitation often results in a lower value. Consult the Application Information for further guidance.
- (7) This is the typical ESR for all the electrolytic (nonceramic) output capacitance. Use 7 m $\Omega$  as the minimum when using max-ESR values to calculate.

# PTV12020W Characteristic Data; 1.2 V to 5.5 V

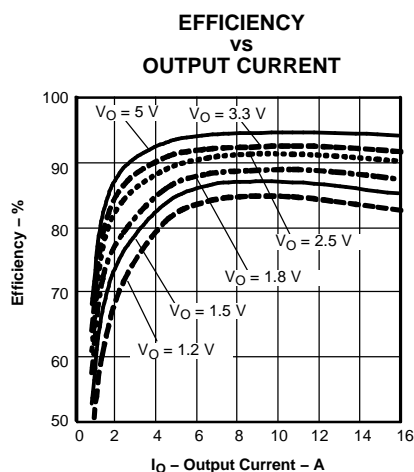


Figure 1.

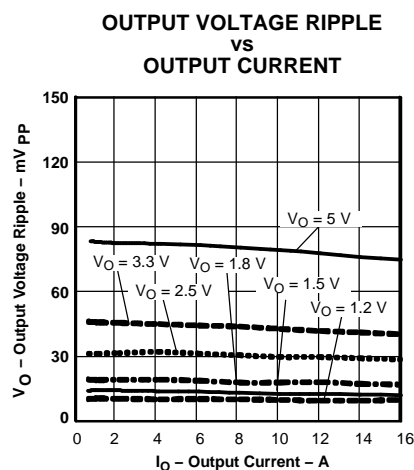


Figure 2.

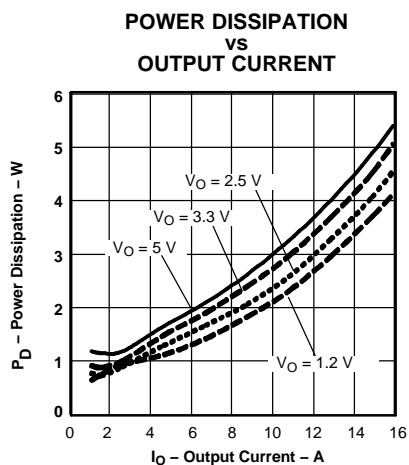


Figure 3.

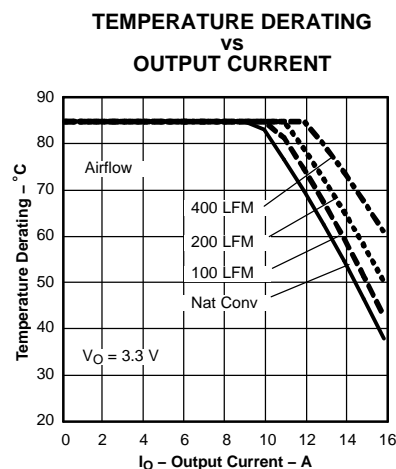


Figure 4.

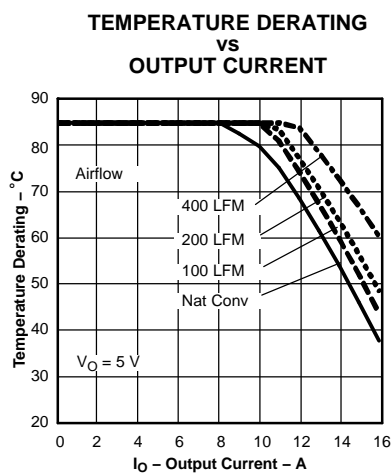


Figure 5.

## PTV12020L Characteristic Data; 0.8 V to 1.8 V

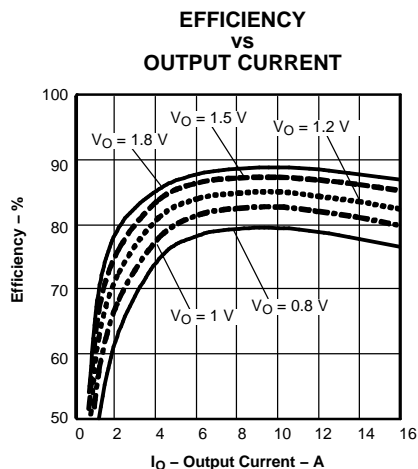


Figure 6.

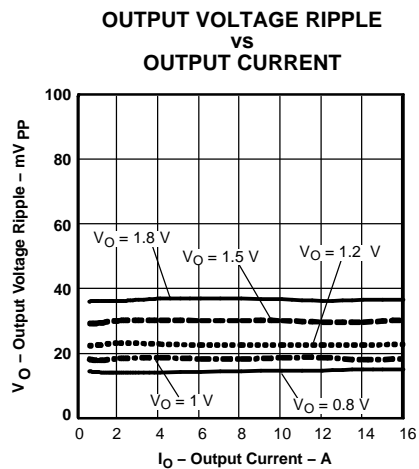


Figure 7.

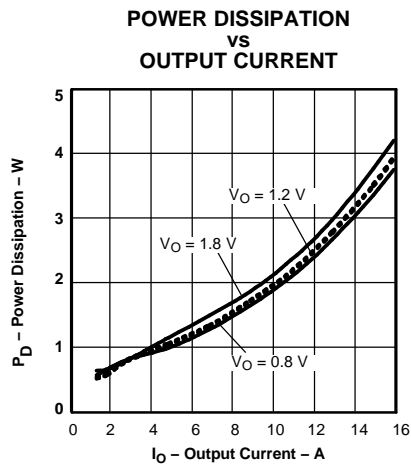


Figure 8.

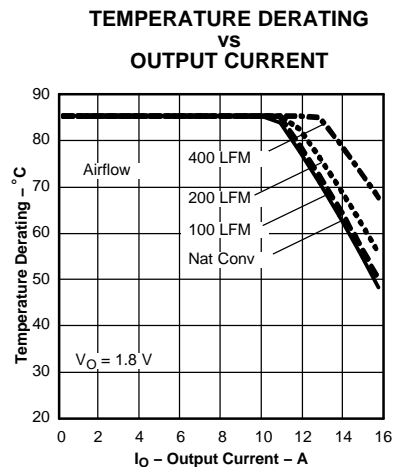


Figure 9.

## DEVICE INFORMATION

### TERMINAL FUNCTIONS

TERMINAL		DESCRIPTION
NAME	NO.	
$V_I$	5, 6	The positive input voltage power node to the module, which is referenced to common GND.
$V_O$	3, 4	The regulated positive power output with respect to the GND node.
GND	1, 2, 10, 11	This is the common ground connection for the $V_I$ and $V_O$ power connections. It is also the 0 VDC reference for the control inputs.
Inhibit	12	The Inhibit pin is an open-collector/drain, active-low input that is referenced to GND. Applying a low-level ground signal to this input disables the module's output and turns off the output voltage. When the Inhibit control is active, the input current drawn by the regulator is significantly reduced. If the inhibit feature is not used, the control pin should be left open-circuit. The module then produces an output voltage whenever a valid input source is applied.
$V_O$ Adjust	8	A 1% resistor must be connected directly between this pin and GND (pin 1 or 2) to set the output voltage of the module higher than its lowest value. The temperature stability of the resistor should be 100 ppm/°C (or better). The set-point range is 1.2 V to 5.5 V for W-suffix devices and 0.8 V to 1.8 V for L-suffix devices. The resistor value required for a given output voltage may be calculated using a formula. If left open-circuit, the module output voltage defaults to its lowest value. For further information on output voltage adjustment, consult the related application note.  The specification table gives the standard resistor values for a number of common output voltages.
$V_O$ Sense	7	The sense input allows the regulation circuit to compensate for voltage drop between the module and the load. For optimal voltage accuracy $V_O$ Sense should be connected to $V_O$ . It can also be left disconnected.
Track	9	This is an analog control input that enables the output voltage to follow an external voltage. This pin becomes active typically 20 ms after the input voltage has been applied, and allows direct control of the output voltage from 0 V up to the nominal set-point voltage. Within this range, the output follows the voltage at the Track pin on a volt-for-volt basis. When the control voltage is raised above this range, the module regulates at its set-point voltage. The feature allows the output voltage to rise simultaneously with other modules powered from the same input bus. If unused, this input should be connected to $V_I$ .  <i>NOTE: Due to the undervoltage lockout feature, the output of the module cannot follow its own input voltage during power up. Consult the related Application Information for further guidance.</i>

Front View of Module

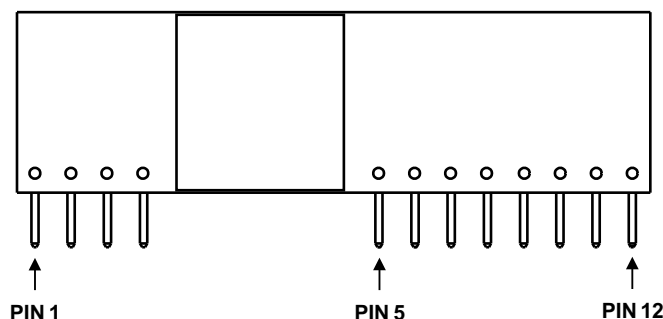


Figure 10. Pin/Terminal Locations

## APPLICATION INFORMATION

### Capacitor Recommendations for the PTV12020 Series of Power Modules

#### Input Capacitors

The required input capacitors are a 22- $\mu\text{F}$  ceramic and 560- $\mu\text{F}$  electrolytic type. For  $V_O > 2.1\text{ V}$  and  $I_O \geq 11\text{ A}$ , the 560- $\mu\text{F}$  capacitance must be rated for 1,200 mArms ripple current capability. For other conditions,  $V_O > 2.1\text{ V}$  at  $I_O < 11\text{ A}$  and  $V_O \leq 2.1\text{ V}$  for all loads, the ripple current rating must be at least 750 mArms. Where applicable, Table 1 gives the maximum output voltage and current limits for a capacitor's rms ripple current rating.

The above ripple current requirements are *conditional* that the 22- $\mu\text{F}$  ceramic capacitor is present. The 22- $\mu\text{F}$  X5R/X7R ceramic capacitor is necessary to reduce both the magnitude of ripple current through the electrolytic capacitor and the amount of ripple current reflected back to the input source. Ceramic capacitors should be located within 0.5 in. (1.3 cm) of the module's input pins. Additional ceramic capacitors can be added to reduce the RMS ripple current requirement for the electrolytic capacitor.

Ripple current (Arms) rating, less than 100-m $\Omega$  equivalent series resistance (ESR), and temperature are the major considerations when selecting input capacitors. Unlike polymer-tantalum capacitors, regular tantalum capacitors have a recommended minimum voltage rating of  $2 \times$  (max. DC voltage + AC ripple). This is standard practice to ensure reliability. Only a few tantalum capacitors were found to have sufficient voltage rating to meet this requirement. At temperatures below 0°C, the ESR of aluminum electrolytic capacitors increases. For these applications Os-Con, polymer-tantalum, and polymer-aluminum types should be considered.

#### Output Capacitor (Optional)

For applications with load transients (sudden changes in load current), regulator response benefits from external output capacitance. The recommended output capacitance of 330  $\mu\text{F}$  allows the module to meet its transient response specification. For most applications, a high-quality computer-grade aluminum electrolytic capacitor is adequate. These capacitors provide decoupling over the frequency range, 2 kHz to 150 kHz, and are suitable when ambient temperatures are above 0°C. For operation below 0°C, tantalum, ceramic, or Os-Con type capacitors are recommended. When using one or more nonceramic capacitors, the calculated equivalent ESR should be no lower than 4 m $\Omega$  (7 m $\Omega$  using the manufacturer's maximum ESR for a single capacitor). A list of preferred low-ESR type capacitors are identified in Table 1.

#### Ceramic Capacitors

Above 150 kHz, the performance of aluminum electrolytic capacitors is less effective. Multilayer ceramic capacitors have low ESR and a resonant frequency higher than the bandwidth of the regulator. They can be used to reduce the reflected ripple current at the input as well as improve the transient response of the output. When used on the output their combined ESR is not critical as long as the total value of ceramic capacitance does not exceed approximately 300  $\mu\text{F}$ . Also, to prevent the formation of local resonances, do not place more than five identical ceramic capacitors in parallel with values of 10  $\mu\text{F}$  or greater.

#### Tantalum Capacitors

Tantalum-type capacitors can only be used on the output bus, and are recommended for applications where the ambient operating temperature can be less than 0°C. The AVX TPS, Sprague 593D/594/595 and Kemet T495/T510 capacitor series are suggested over many other tantalum types due to their higher rated surge, power dissipation, and ripple current capability. As a caution, many general-purpose tantalum capacitors have considerably higher ESR, reduced power dissipation and lower ripple current capability. These capacitors are also less reliable as they have reduced power dissipation and surge current ratings. Tantalum capacitors that have no stated ESR or surge current rating are not recommended for power applications.

When specifying Os-con and polymer tantalum capacitors for the output, the minimum ESR limit is encountered before the maximum capacitance value is reached.

#### Capacitor Table

Table 1 identifies the characteristics of capacitors from a number of vendors with acceptable ESR and ripple current (rms) ratings. The recommended number of capacitors required at both the input and output buses is identified for each capacitor type.

## APPLICATION INFORMATION (continued)

**Note:** This is not an extensive capacitor list. Capacitors from other vendors are available with comparable specifications. Those listed are for guidance. The RMS ripple current rating and ESR (at 100 kHz) are critical parameters necessary to ensure both optimum regulator performance and long capacitor life.

### Designing for Fast Load Transients

The transient response of the dc/dc converter has been characterized using a load transient with a di/dt of 1 A/μs. The typical voltage deviation for this load transient is given in the data sheet specification table using the optional value of output capacitance. As the di/dt of a transient is increased, the response of a converter regulation circuit ultimately depends on its output capacitor decoupling network. This is an inherent limitation with any dc/dc converter once the speed of the transient exceeds its bandwidth capability. If the target application specifies a higher di/dt or lower voltage deviation, the requirement can only be met with additional output capacitor decoupling. In these cases special attention must be paid to the type, value and ESR of the capacitors selected.

If the transient performance requirements exceed that specified in the data sheet, or the total amount of load capacitance is above 3,000 μF, the selection of output capacitors becomes more important.

**Table 1. Input/Output Capacitors**

Capacitor Vendor, Type/Series (Style)	Capacitor Characteristics					Quantity		Vendor Part Number
	Working Voltage (V)	Value (μF)	Max ESR at 100 kHz (Ω)	Max Ripple Current at 85°C (Irms) (mA)	Physical Size (mm)	Input Bus	Optional Output Bus	
Panasonic, Aluminum	25	330	0.090	775	10 × 12.5	2	1	EEUFC1E331 (V <sub>O</sub> ≤ 2.1 V, or V <sub>O</sub> > 2.1 V and I <sub>O</sub> ≤ 10 A)
FC (Radial)	25	560	0.065	1205	12.5 × 15	1	1	EEUFC1E561S
	25	1,000	0.060	1100	12.5 × 13.5	1	1	EEVFK1E102Q (V <sub>O</sub> ≤ 3.4 V and I <sub>O</sub> ≤ 16 A)
FK (SMD)	35	680	0.060	1100	12.5 × 13.5	1	1	EEVFK1V681Q (V <sub>O</sub> ≤ 3.4 V and I <sub>O</sub> ≤ 16 A)
United Chemi-Con	16	330	0.018	4500	10 × 10.5	2	≤ 3	16FX330M
FX, OS-Con (SMD)	16	330	0.090	760	10 × 12.5	2	1	LXZ25VB331M10X12LL (V <sub>O</sub> ≤ 2.1V, or V <sub>O</sub> > 2.1V and I <sub>O</sub> ≤ 10 A)
LXZ, Aluminum (Radial)	25	680	0.068	1050	10 × 16	1	1	LXZ16VB681M10X16LL (V <sub>O</sub> ≤ 3.4 V and I <sub>O</sub> ≤ 16 A)
PS, Poly-Aluminum (Radial)	16	330	0.014	5060	10 × 12.5	2	≤ 2	16PS330MJ12
PXA, Poly-Aluminum (SMD)	16	330	0.014	5050	10 × 12.2	2	≤ 3	PXA16VCMJ12
Nichicon, Aluminum	25	560	0.060	1060	12.5 × 15	1	1	UPM1E561MHH6 (V <sub>O</sub> ≤ 3.4 V and I <sub>O</sub> ≤ 16 A)
HD (Radial)	25	680	0.038	1430	10 × 16	1	1	UHD1C681MHR
PM (Radial)	35	560	0.048	1360	16 × 15	1	1	UPM1V561MHH6
Panasonic, Poly-Aluminum								
A (SMD)	16	330	0.022	4100	10 × 10.2	2	≤ 3	EEFWA1C331P
S/SE (SMD)	6.3	180	0.005	4000	7.3 × 154.3 × 4.2	N/R <sup>(1)</sup>	≤ 1	EEFSE0J181R (V <sub>O</sub> ≤ 5.1 V)
Sanyo								
TP, Psocap	10	330	0.025	3000	7.3 L × 5.7 W	N/R <sup>(1)</sup>	≤ 4	10TPE330M
SP, Os-Con	16	270	0.018	>3500	10 × 10.5	2 <sup>(2)</sup>	≤ 3	16SP270M
SVP, Os-Con (SMD)	16	330	0.016	4700	11 × 12	2	≤ 3	16SVP330M
AVX, Tantalum, Series III	10	470	0.045	>1723		N/R <sup>(1)</sup>	≤ 5	TPSE477M010R0045 (V <sub>O</sub> ≤ 5.1 V)
TPS (SMD)	10	330	0.045	>1723	7.3L × 5.7 W × 4.1 H	N/R <sup>(1)</sup>	≤ 5	TPSE337M010R0045 (V <sub>O</sub> ≤ 5.1 V)
Kemet (SMD)								

(1) N/R – Not recommended. The voltage rating does not meet the minimum operating limits.

(2) Total capacitance of 540 μF is acceptable based on the combined ripple current rating.

**APPLICATION INFORMATION (continued)****Table 1. Input/Output Capacitors (continued)**

Capacitor Vendor, Type/Series (Style)	Capacitor Characteristics					Quantity		Vendor Part Number
	Working Voltage (V)	Value ( $\mu$ F)	Max ESR at 100 kHz ( $\Omega$ )	Max Ripple Current at 85°C (Irms) (mA)	Physical Size (mm)	Input Bus	Optional Output Bus	
T520, Poly-Tant	10	330	0.040	1800	43 W $\times$ 7.3 L $\times$ 4 H	N/R <sup>(1)</sup>	$\leq 5$	T520X337M010AS
T530, Poly-Tant/Organic	10	330	0.010	>3800		N/R <sup>(1)</sup>	$\leq 1$	T530X337M010ASE010
	6.3	470	0.010	4200		N/R <sup>(1)</sup>	$\leq 1$	T530X477M006ASE010 ( $V_O \leq 5.1$ V)
Vishay-Sprague								
595D, Tantalum (SMD)	10	470	0.100	1440	7.2 L $\times$ 6 W $\times$ 4.1 H	N/R <sup>(1)</sup>	$\leq 5$	595D477X0010R2T ( $V_O \leq 5.1$ V)
94SA, Os-Con (Radial)	16	1,000	0.015	9740	16 $\times$ 25	1	$\leq 2$	94SA108X0016HBP
Kemet, Ceramic X5R (SMD)	16	10	0.002	—	3225	$\Rightarrow 2$ <sup>(3)</sup>	$\leq 5$	C1210C106M4PAC
	6.3	47	0.002		3225	N/R <sup>(1)</sup>	$\leq 5$	C1210C476K9PAC
Murata, Ceramic X5R (SMD)	6.3	100	0.002	—	3225	N/R <sup>(1)</sup>	$\leq 3$	GRM32ER60J107M
	6.3	47			3225	N/R <sup>(1)</sup>	$\leq 5$	GRM32ER60J476M
	16	22				$\Rightarrow 1$ <sup>(3)</sup>	$\leq 5$	GRM32ER61C226K
	16	10				$\Rightarrow 2$ <sup>(3)</sup>	$\leq 5$	GRM32DR61C106K
TDK, Ceramic X5R (SMD)	6.3	100	0.002	—	3225	N/R <sup>(1)</sup>	$\leq 3$	C3225X5R0J107MT
	6.3	47			3225	N/R <sup>(1)</sup>	$\leq 5$	C3225X5R0J476MT
	16	22				$\Rightarrow 1$ <sup>(3)</sup>	$\leq 5$	C3225X5R1C226MT
	16	10				$\Rightarrow 2$ <sup>(4)</sup>	$\leq 5$	C3225X5R1C106MT

(3) Ceramic capacitors are required to complement electrolytic types at the input and to reduce high-frequency ripple current.

(4) Ceramic capacitors are required to complement electrolytic types at the input and to reduce high-frequency ripple current.

**Adjusting the Output Voltage of the PTV12020x Series**

The  $V_O$  Adjust control (pin 8) sets the output voltage of the PTV12020 product. The adjustment range is from 1.2 V to 5.5 V for the W-suffix modules and 0.8 V to 1.8 V for L-suffix modules. The adjustment method requires the addition of a single external resistor,  $R_{SET}$ , that must be connected directly between the  $V_O$  Adjust and GND (pin 1 or 2). Table 2 gives the preferred value of the external resistor for a number of standard voltages, along with the actual output voltage that this resistance value provides. Figure 11 shows the placement of the required resistor.

**Table 2. Standard Values of  $R_{SET}$  for Common Output Voltages**

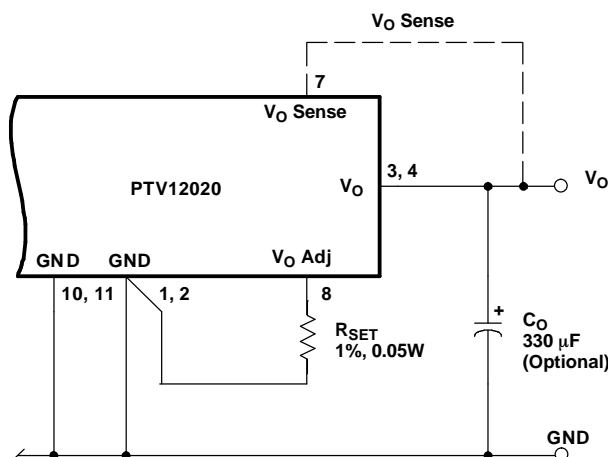
$V_O$ (Required)	PTV12020W		PTV12020L	
	$R_{SET}$ (Standard Value)	$V_O$ (Actual)	$R_{SET}$ (Standard Value)	$V_O$ (Actual)
5 V	280 $\Omega$	5.009 V	N/A	N/A
3.3 V	2.0 k $\Omega$	3.294 V	N/A	N/A
2.5 V	4.32 k $\Omega$	2.503 V	N/A	N/A
2 V	8.06 k $\Omega$	2.010 V	N/A	N/A
1.8 V	11.5 k $\Omega$	1.801 V	130 $\Omega$	1.800 V
1.5 V	24.3 k $\Omega$	1.506 V	3.57 k $\Omega$	1.499 V
1.2 V	Open	1.200 V	12.1 k $\Omega$	1.201 V
1.1 V	N/A	N/A	18.7 k $\Omega$	1.101 V
1.0 V	N/A	N/A	32.4 k $\Omega$	0.999 V
0.9 V	N/A	N/A	71.5 k $\Omega$	0.901 V
0.8 V	N/A	N/A	Open	0.800 V

For other output voltages, the value of the required resistor can either be calculated or simply selected from the range of values given in Table 4. Equation 1 may be used for calculating the adjust resistor value. Select the appropriate value for the parameters,  $R_s$  and  $V_{min}$ , from Table 3.

$$R_{set} = 10 \text{ k}\Omega \times \frac{0.8 \text{ V}}{V_{out} - V_{min}} - R_s \text{ k}\Omega \quad (1)$$

**Table 3. Adjust Formula Parameters**

Pt. No.	PTV12020W	PTV12020L
$V_{min}$	1.2 V	0.8 V
$V_{max}$	5.5 V	1.8 V
$R_s$	1.82 k $\Omega$	7.87 k $\Omega$



- (1) A 0.05-W rated resistor may be used. The tolerance should be 1%, with temperature stability of 100 ppm/ $^{\circ}$ C (or better). Place the resistor as close to the regulator as possible. Connect the resistor directly between pin 8 and pins 1 or 2, using dedicated PCB traces.
- (2) Never connect capacitors from  $V_o$ Adj to either GND or  $V_o$ . Any capacitance added to the  $V_o$ Adj pin affects the stability of the regulator.

**Figure 11.  $V_o$  Adjust Resistor Placement**

**Table 4. Calculated Values of  $R_{SET}$  for Other Output Voltages**

PTV12020W				PTV12020L	
$V_{OUT}$	$R_{SET}$	$V_{OUT}$	$R_{SET}$	$V_{OUT}$	$R_{SET}$
1.200	Open	2.70	3.51 k $\Omega$	0.800	Open
1.250	158.0 k $\Omega$	2.80	3.18 k $\Omega$	0.825	312.0 k $\Omega$
1.300	78.2 k $\Omega$	2.90	2.89 k $\Omega$	0.850	152.0 k $\Omega$
1.350	51.5 k $\Omega$	3.00	2.62 k $\Omega$	0.875	98.8 k $\Omega$
1.400	38.2 k $\Omega$	3.10	2.39 k $\Omega$	0.900	72.1 k $\Omega$
1.450	30.2 k $\Omega$	3.20	2.18 k $\Omega$	0.925	56.1 k $\Omega$
1.50	24.8 k $\Omega$	3.30	1.99 k $\Omega$	0.950	45.5 k $\Omega$
1.55	21.0 k $\Omega$	3.40	1.82 k $\Omega$	0.975	37.8 k $\Omega$
1.60	18.2 k $\Omega$	3.50	1.66 k $\Omega$	1.000	32.1 k $\Omega$
1.65	16.0 k $\Omega$	3.60	1.51 k $\Omega$	1.025	27.7 k $\Omega$
1.70	14.2 k $\Omega$	3.70	1.38 k $\Omega$	1.050	24.1 k $\Omega$
1.75	12.7 k $\Omega$	3.80	1.26 k $\Omega$	1.075	21.2 k $\Omega$
1.80	11.5 k $\Omega$	3.90	1.14 k $\Omega$	1.100	18.8 k $\Omega$
1.85	10.5 k $\Omega$	4.00	1.04 k $\Omega$	1.125	16.7 k $\Omega$
1.90	9.61 k $\Omega$	4.10	939 $\Omega$	1.150	15.0 k $\Omega$
1.95	8.85 k $\Omega$	4.20	847 $\Omega$	1.175	13.5 k $\Omega$
2.00	8.18 k $\Omega$	4.30	761 $\Omega$	1.200	12.1 k $\Omega$
2.05	7.59 k $\Omega$	4.40	680 $\Omega$	1.250	9.91 k $\Omega$
2.10	7.07 k $\Omega$	4.50	604 $\Omega$	1.300	8.13 k $\Omega$
2.15	6.60 k $\Omega$	4.60	533 $\Omega$	1.350	6.68 k $\Omega$
2.20	6.18 k $\Omega$	4.70	466 $\Omega$	1.400	5.46 k $\Omega$
2.25	5.80 k $\Omega$	4.80	402 $\Omega$	1.450	4.44 k $\Omega$
2.30	5.45 k $\Omega$	4.90	342 $\Omega$	1.50	3.56 k $\Omega$
2.35	5.14 k $\Omega$	5.00	285 $\Omega$	1.55	2.8 k $\Omega$
2.40	4.85 k $\Omega$	5.10	231 $\Omega$	1.60	2.13 k $\Omega$
2.45	4.58 k $\Omega$	5.20	180 $\Omega$	1.65	1.54 k $\Omega$
2.50	4.33 k $\Omega$	5.30	131 $\Omega$	1.70	1.02 k $\Omega$
2.55	4.11 k $\Omega$	5.40	85 $\Omega$	1.75	551 $\Omega$
2.60	3.89 k $\Omega$	5.50	41 $\Omega$	1.80	130 $\Omega$
2.65	3.70 k $\Omega$				

## Features of the PTH/PTV Family of Non-Isolated, Wide-Output Adjust Power Modules

### POLA™ Compatibility

The PTH/PTV family of non-isolated, wide-output adjustable power modules from Texas Instruments are optimized for applications that require a flexible, high-performance module that is small in size. Each of these products are POLA™ compatible. POLA-compatible products are produced by a number of manufacturers, and offer customers advanced, non-isolated modules with the same footprint and form factor. POLA parts are also ensured to be interoperable, thereby providing customers with true second-source availability.

### Soft-Start Power Up

The Auto-Track feature allows the power up of multiple PTH/PTV modules to be directly controlled from the *Track* pin. However, in a stand-alone configuration, or when the Auto-Track feature is not being used, the *Track* pin should be directly connected to the input voltage,  $V_i$  (see Figure 12).

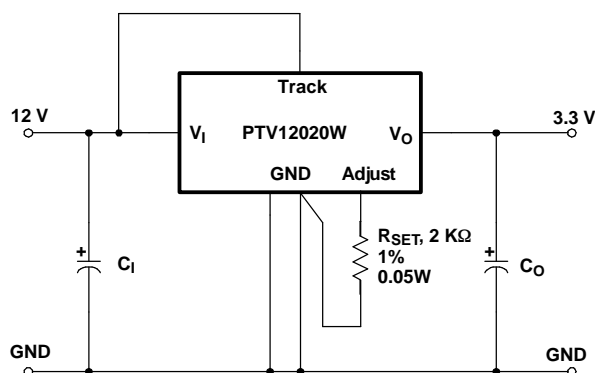


Figure 12.

When the *Track* pin is connected to the input voltage, the Auto-Track function is permanently disengaged. This allows the module to power up entirely under the control of its internal soft-start circuitry. When power up is under soft-start control, the output voltage rises to the set point at a quicker and more linear rate.

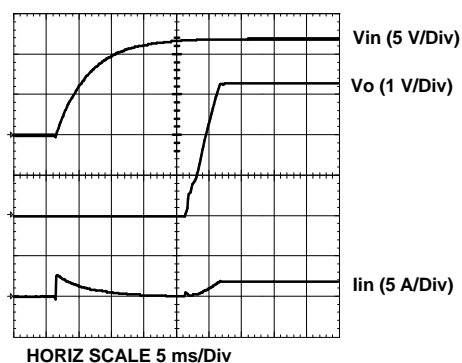


Figure 13.

From the moment a valid input voltage is applied, the soft-start control introduces a short time delay (typically 8 ms–15 ms) before allowing the output voltage to rise. The output then progressively rises to the module set-point voltage. Figure 13 shows the soft-start power-up characteristic of the 16-A output product (PTV12020W), operating from a 12-V input bus and configured for a 3.3-V output. The waveforms were measured with a 5-A resistive load and the Auto-Track feature disabled. The initial rise in input current when the input voltage first starts to rise is the charge current drawn by the input capacitors. Power up is complete within 25 ms.

## Overcurrent Protection

For protection against load faults, the modules incorporate output overcurrent protection. Applying a load that exceeds the overcurrent threshold causes the regulated output to shut down. Following shutdown, a module periodically attempts to recover by initiating a soft-start power up. This is described as a *hiccup* mode of operation, whereby the module continues in a cycle of successive shutdown and power up until the load fault is removed. During this period, the average current flowing into the fault is significantly reduced. Once the fault is removed, the module automatically recovers and returns to normal operation.

## Overtemperature Protection (OTP)

An onboard temperature sensor protects the module internal circuitry against excessively high temperatures. A rise in the internal temperature may be the result of a drop in airflow or a high ambient temperature. If the internal temperature exceeds the OTP threshold, the module Inhibit control is internally pulled low. This turns the output off. The output voltage drops as the external output capacitors are discharged by the load circuit. The recovery is automatic, and begins with a soft-start power up. It occurs when the sensed temperature decreases by about 10°C below the trip point.

**Note:** The overtemperature protection is a last resort mechanism to prevent thermal stress to the regulator. Operation at or close to the thermal shutdown temperature is not recommended and reduces the long-term reliability of the module. Always operate the regulator within the specified Safe Operating Area (SOA) limits for the worst-case conditions of ambient temperature and airflow.

## Output On/Off Inhibit

For applications requiring output voltage on/off control, the modules incorporate an output Inhibit control pin. The inhibit feature can be used wherever there is a requirement for the output voltage from the regulator to be turned off.

The power modules function normally when the *Inhibit* input is left open-circuit, providing a regulated output whenever a valid source voltage is connected to  $V_I$  with respect to GND.

Figure 14 shows the typical application of the inhibit function. Note the discrete transistor (Q1). The *Inhibit* input has its own internal pull up (see footnotes to electrical characteristics table). The input is not compatible with TTL logic devices. An open-collector (or open-drain) discrete transistor is recommended for control.

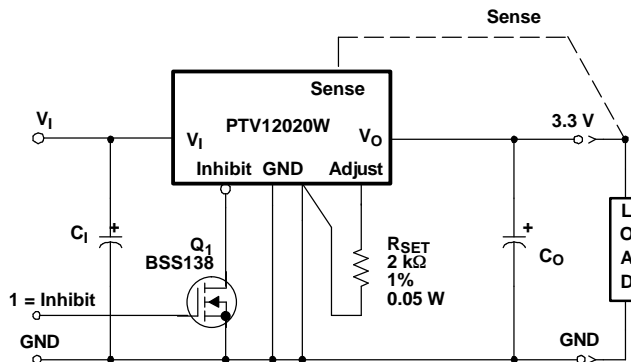
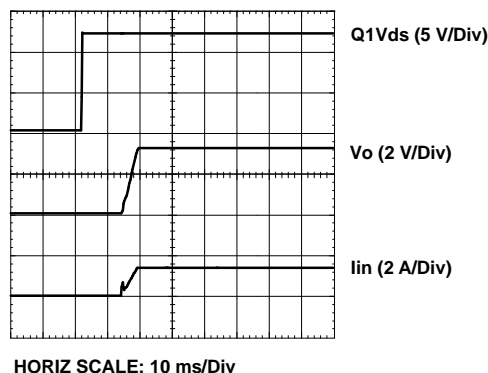


Figure 14.

Turning Q1 on applies a low voltage to the Inhibit control pin and disables the output of the module. If Q1 is then turned off, the module executes a soft-start power-up sequence. A regulated output voltage is produced within 25 ms. Figure 15 shows the typical rise in both the output voltage and input current, following the turnoff of Q1. The turnoff of Q1 corresponds to the rise in the waveform, Q1  $V_{DS}$ . The waveforms were measured with a 5-A constant current load.



**Figure 15.**

### Auto-Track™ Function

The Auto-Track function is unique to the PTH/PTV family, and is available with all POLA products. Auto-Track was designed to simplify the amount of circuitry required to make the output voltage from each module power up and power down in sequence. The sequencing of two or more supply voltages during power up is a common requirement for complex mixed-signal applications, that use dual-voltage VLSI ICs such as DSPs, microprocessors, and ASICs.

### How Auto-Track™ Works

Auto-Track works by forcing the module output voltage to follow a voltage presented at the Track control pin <sup>1</sup>. This control range is limited to between 0 V and the module set-point voltage. Once the track-pin voltage is raised above the set-point voltage, the module's output remains at its set point <sup>2</sup>. As an example, if the Track pin of a 2.5-V regulator is at 1 V, the regulated output will be 1 V. But if the voltage at the *Track* pin rises to 3 V, the regulated output does not go higher than 2.5 V.

When under Auto-Track control, the regulated output from the module follows the voltage at its *Track* pin on a volt-for-volt basis. By connecting the *Track* pin of a number of these modules together, the output voltages follow a common signal during power up and power down. The control signal can be an externally generated master ramp waveform, or the output voltage from another power supply circuit <sup>3</sup>. For convenience, the *Track* input incorporates an internal RC-charge circuit. This operates off the module input voltage to produce a suitable rising waveform at power up.

### Typical Application

The basic implementation of Auto-Track allows for simultaneous voltage sequencing of a number of Auto-Track compliant modules. Connecting the Track control pins of two or more modules forces the Track control of all modules to follow the same collective RC-ramp waveform, and allows them to be controlled through a single transistor or switch; see Q1 in Figure 16.

To initiate a power-up sequence, it is recommended that the Track control first be pulled to ground potential. This is done at or before input power is applied to the modules, and then held for at least 10 ms thereafter. This brief period gives the modules time to complete their internal soft-start initialization. Applying a logic level high signal to the circuit On/Off Control turns Q1 on and applies a ground signal to the Track pins. After completing their internal soft-start initialization, the output of all modules remains at zero volts while Q1 is on.

Q1 may be turned off 10 ms after a valid input voltage has been applied to the modules. This allows the track control voltage to automatically rise to the module input voltage. During this period, the output voltage of each module rises in unison with other modules to its respective set-point voltage.

Figure 17 shows the output voltage waveforms from the circuit of Figure 16 after the On/Off Control is set from a high-level to a low-level voltage. The waveforms,  $V_{O1}$  and  $V_{O2}$  represent the output voltages from the two power modules, U1 (3.3 V) and U2 (2 V), respectively.  $V_{O1}$  and  $V_{O2}$  are shown rising together to produce the desired simultaneous power-up characteristic.

The same circuit also provides a power-down sequence. Power down is the reverse of power up, and is accomplished by lowering the track control voltage back to zero volts. The important constraint is that a valid input voltage must be maintained until the power down is complete. It also requires that Q1 be turned off relatively slowly. This is so that the Track control voltage does not fall faster than Auto-Track slew rate capability, which is 1 V/ms. The components R1 and C1 in Figure 16 limit the rate at which Q1 pulls down the Track control voltage. The values of 100 k $\Omega$  and 0.1  $\mu$ F correlate to a decay rate of about 0.17 V/ms.

The power-down sequence is initiated with a low-to-high transition at the On/Off Control input to the circuit. Figure 18 shows the power-down waveforms. As the Track control voltage falls below the nominal set-point voltage of each power module, then its output voltage decays with all the other modules under Auto-Track control.

#### Notes on Use of Auto-Track™

1. The Track pin voltage must be allowed to rise above the module set-point voltage before the module can regulate at its adjusted set-point voltage.
2. The Auto-Track function tracks almost any voltage ramp during power up, and is compatible with ramp speeds of up to 1 V/ms.
3. The absolute maximum voltage that may be applied to the Track pin is the input voltage  $V_I$ .
4. The module does not follow a voltage at its Track control input until it has completed its soft-start initialization. This takes about 10 ms from the time that the module has sensed that a valid voltage has been applied to its input. During this period, it is recommended that the Track pin be held at ground potential.
5. The module is capable of both sinking and sourcing current when following a voltage at its Track pin. Therefore, start up into an output prebias cannot be supported when a module is under Auto-Track control.  
**Note:** A prebias holdoff is not necessary when all supply voltages rise simultaneously under the control of Auto-Track.
6. The Auto-Track function can be disabled by connecting the Track pin to the input voltage ( $V_I$ ). When Auto-Track is disabled, the output voltage rises at a quicker and more linear rate after input power is applied.

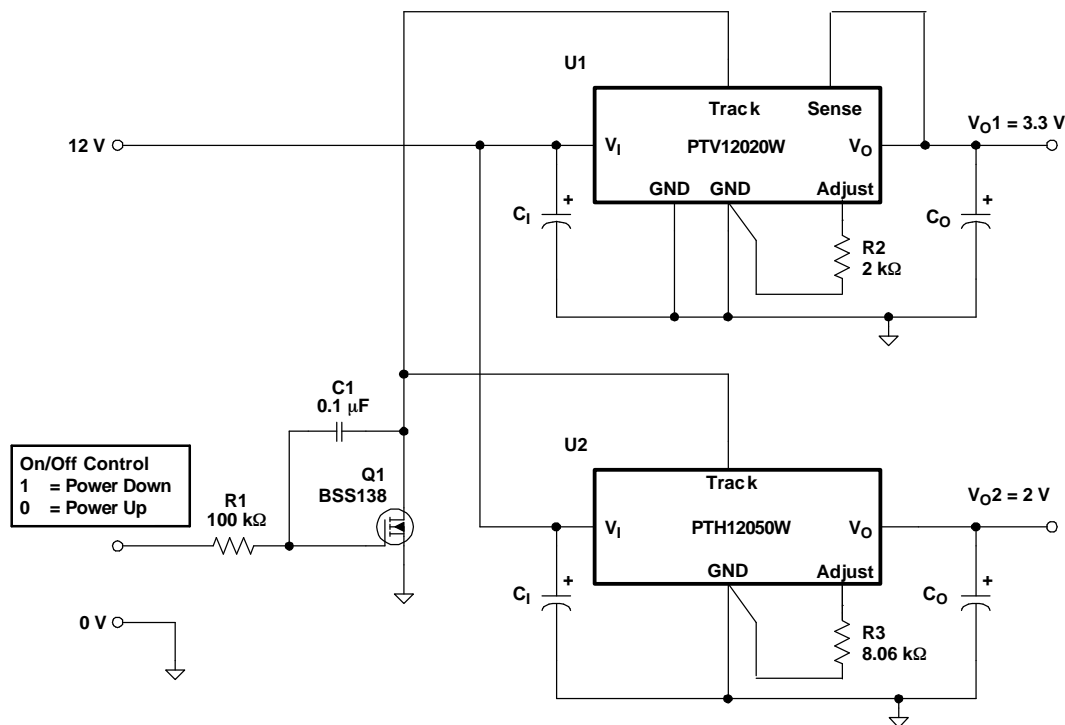


Figure 16. Sequenced Power Up and Power Down Using Auto-Track

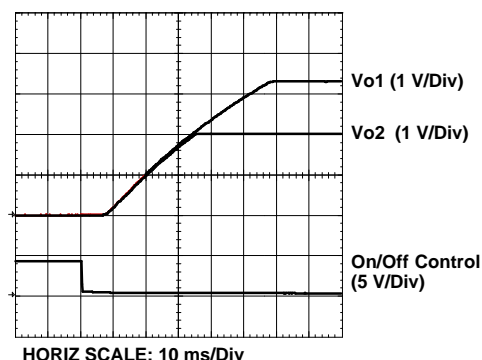


Figure 17. Simultaneous Power Up With Auto-Track Control

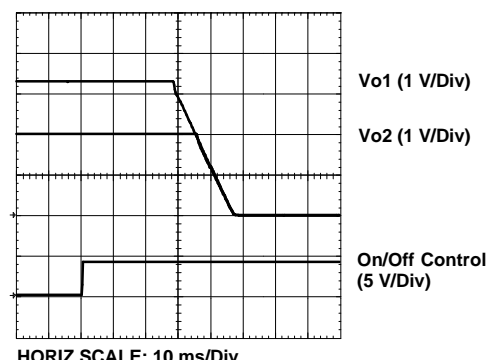


Figure 18. Simultaneous Power Down With Auto-Track Control

### Prebias Start-Up Capability

A prebias start-up condition occurs as a result of an external voltage being present at the output of a power module prior to its output becoming active. This often occurs in complex digital systems when current from another power source is backed through a dual-supply logic component, such as an FPGA or ASIC. Another path might be via clamp diodes, sometimes used as part of a dual-supply power-up sequencing arrangement. A prebias can cause problems with power modules that incorporate synchronous rectifiers. This is because under most operating conditions, such modules can sink as well as source output current. The 12-V input modules incorporate synchronous rectifiers, but do not sink current during start up, or whenever the *Inhibit* pin is held low. Start up includes an initial delay (approximately 8–15 ms), followed by the rise of the output voltage under the control of the module internal soft-start mechanism; see Figure 19.

### Conditions for Prebias Holdoff

In order for the module to allow an output prebias voltage to exist (and not sink current), certain conditions must be maintained. The module holds off a prebias voltage when the *Inhibit* pin is held low, and whenever the output is allowed to rise under soft-start control. Power up under soft-start control occurs on the removal of the ground signal to the *Inhibit* pin (with input voltage applied), or when input power is applied with Auto-Track disabled<sup>2</sup>. To further ensure that the regulator does not sink output current (even with a ground signal applied to its *Inhibit*), the input voltage must always be greater than the applied prebias source. This condition must exist throughout the power-up sequence<sup>3</sup>.

The soft-start period is complete when the output begins rising above the prebias voltage. Once it is complete, the module functions as normal and sinks current if a voltage higher than the nominal regulation value is applied to its output.

**Note:** If a prebias condition is not present, the soft-start period is complete when the output voltage has risen to either the set-point voltage, or the voltage applied at the module Track control pin, whichever is lowest, to its output.

### Demonstration Circuit

Figure 20 shows the start-up waveforms for the demonstration circuit shown in Figure 21. The initial rise in  $V_{O2}$  is the prebias voltage, which is passed from the VCCIO to the VCORE voltage rail through the ASIC. Note that the output current from the module ( $I_{O2}$ ) is negligible until its output voltage rises above the applied prebias.

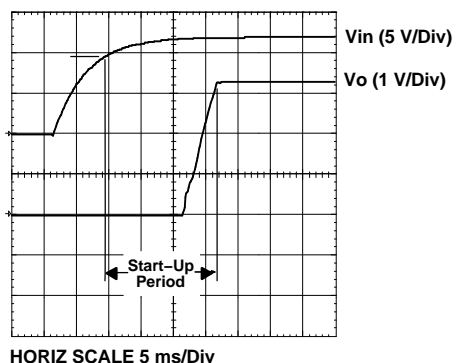


Figure 19. PTV12020W Start Up

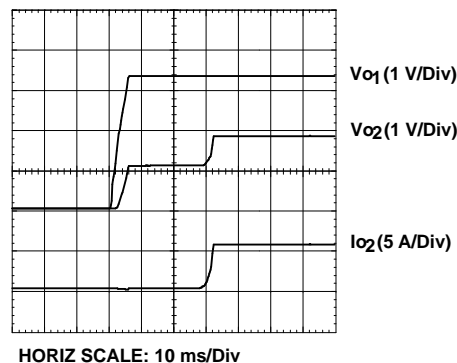


Figure 20. Prebias Start-Up Waveforms

**NOTES:**

1. The prebias start-up feature is not compatible with Auto-Track. If the rise in the output is limited by the voltage applied to the *Track* control pin, the output sinks current during the period that the track control voltage is below that of the back-feeding source. For this reason, Auto-Track should be disabled when not being used. This is accomplished by connecting the *Track* pin to the input voltage,  $V_I$ . This raises the *Track* pin well above the set-point voltage prior to start up, thereby defeating the Auto-Track feature.
2. To further ensure that the regulator output does not sink current when power is first applied (even with a ground signal applied to the *Inhibit* control pin), the input voltage *must* always be greater than the applied prebias source. This condition must exist *throughout* the power-up sequence of the power system.

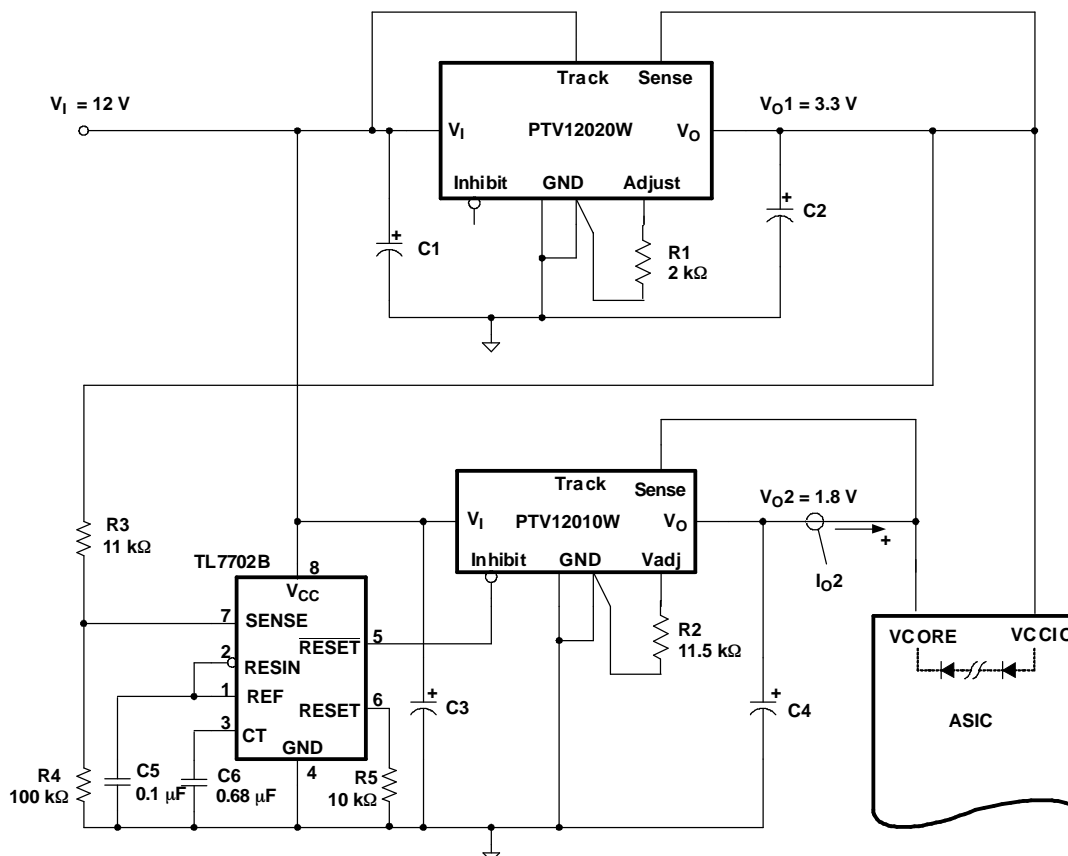


Figure 21. Application Circuit Demonstrating Prebias Startup

## Remote Sense

Products with this feature incorporate an output voltage sense pin,  $V_O$  Sense. A remote sense improves the load regulation performance of the module by allowing it to compensate for any  $IR$  voltage drop between its output and the load. An  $IR$  drop is caused by the high output current flowing through the small amount of pin and trace resistance.

To use this feature, simply connect the  $V_O$  Sense pin to the  $V_O$  node, close to the load circuit (see the data sheet standard application). If a sense pin is left open-circuit, an internal low-value resistor ( $15\ \Omega$  or less) connected between the pin and the output node, ensures that the output remains in regulation.

With the sense pin connected, the difference between the voltage measured directly between the  $V_O$  and  $GND$  pins, and that measured from  $V_O$  Sense to  $GND$ , is the amount of  $IR$  drop being compensated by the regulator. This should be limited to a maximum of  $0.3\text{ V}$ .

**Note:** The remote sense feature is not designed to compensate for the forward drop of nonlinear or frequency dependent components that may be placed in series with the output. Examples include OR-ing diodes, filter inductors, ferrite beads, and fuses. When these components are enclosed by the remote sense connection, they are effectively placed inside the regulation control loop, which can adversely affect the stability of the regulator.

## PACKAGING INFORMATION

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
PTV12020LAH	ACTIVE	SIP MOD ULE	EVC	12	40	Pb-Free (RoHS)	Call TI	N / A for Pkg Type
PTV12020WAD	ACTIVE	SIP MOD ULE	EVC	12	40	Pb-Free (RoHS)	Call TI	N / A for Pkg Type
PTV12020WAH	ACTIVE	SIP MOD ULE	EVC	12	40	Pb-Free (RoHS)	Call TI	N / A for Pkg Type

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

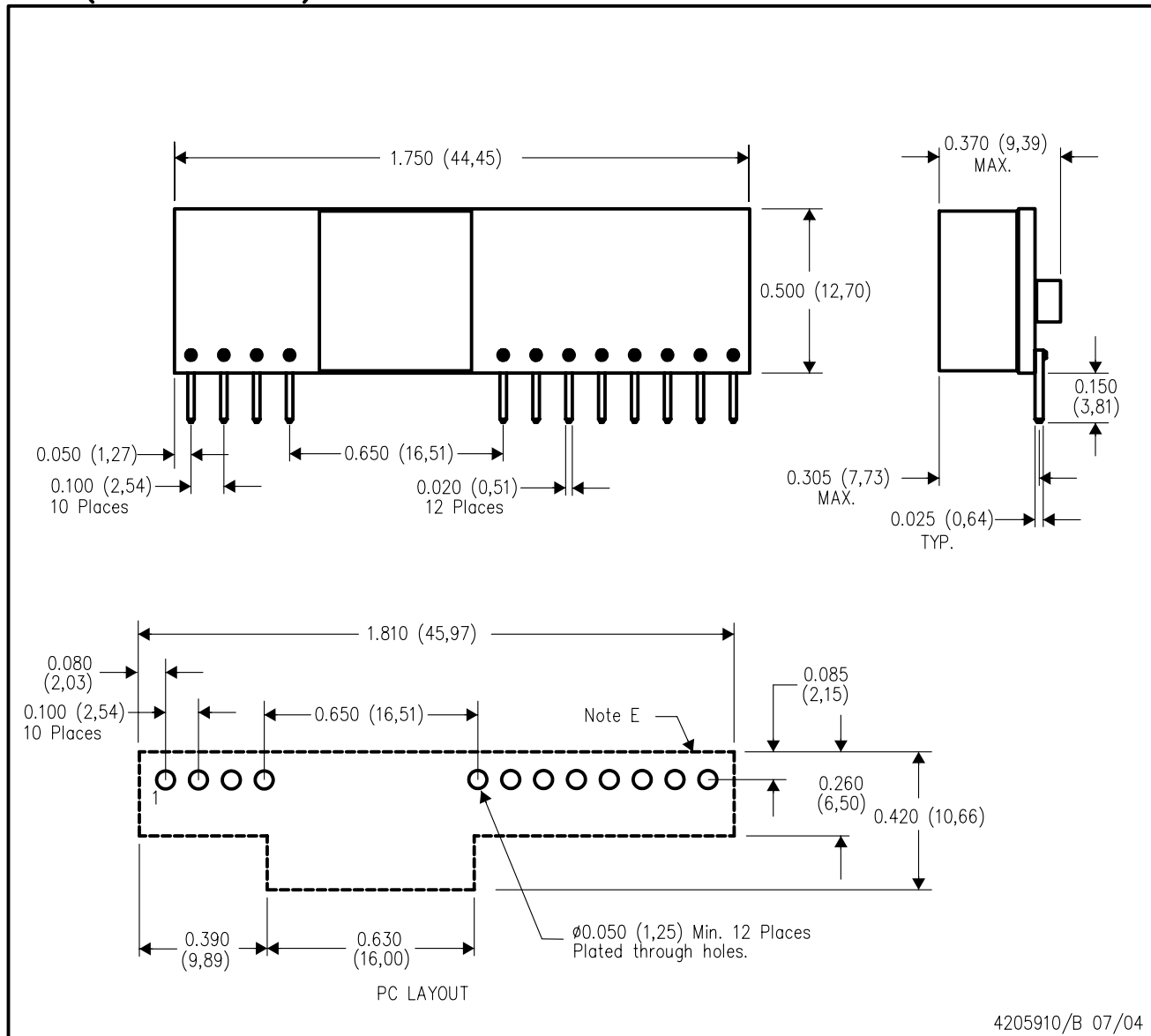
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# MECHANICAL DATA

EVC (R-PDSS-T12)

DOUBLE SIDED MODULE



- NOTES:
- A. All linear dimensions are in inches (mm).
  - B. This drawing is subject to change without notice.
  - C. 2 place decimals are  $\pm 0.030$  ( $\pm 0.76$ mm).
  - D. 3 place decimals are  $\pm 0.010$  ( $\pm 0.25$ mm).
  - E. Recommended keep out area for user components.
  - F. Pins are 0.020" (0,51) x 0.025" (0,64).
  - G. All pins: Material – Copper Alloy  
Finish – Tin (100%) over Nickel plate

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