

DUAL-SLOT PC CARD POWER-INTERFACE SWITCH WITH RESET FOR SERIAL PCMCIA CONTROLLER

SLVS123A – SEPTEMBER 1995 – REVISED JUNE 1998

- Fully Integrated V_{CC} and V_{pp} Switching for Dual-Slot PC Card™ Interface
- P2C™ 3-Lead Serial Interface Compatible With CardBus™ Controllers
- Meets PC Card Standards
- RESET Allows System Initialization of PC Cards
- 12-V Supply Can Be Disabled Except During 12-V Flash Programming
- Short Circuit and Thermal Protection
- Space-Saving 30-Pin SSOP (DB) Package
- Compatible With 3.3-V, 5-V and 12-V PC Cards
- Power Saving $I_{DD} = 83 \mu A$ Typ, $I_Q = 1 \mu A$
- Low $r_{DS(on)}$ (160-m Ω V_{CC} Switch)
- Break-Before-Make Switching

DB OR DF PACKAGE
(TOP VIEW)

5V	1	30	5V
5V	2	29	NC
DATA	3	28	NC
CLOCK	4	27	NC
LATCH	5	26	NC
RESET	6	25	V_{DD}
12V	7	24	12V
AVPP	8	23	BVPP
AVCC	9	22	BVCC
AVCC	10	21	BVCC
AVCC	11	20	BVCC
GND	12	19	BPWR_GOOD
APWR_GOOD	13	18	OC
RESET	14	17	3.3V
3.3V	15	16	3.3V

NC – No internal connection

description

The TPS2202AI PC Card power-interface switch provides an integrated power-management solution for two PC Cards. All of the discrete power MOSFETs, a logic section, current limiting, thermal protection, and power-good reporting for PC Card control are combined on a single integrated circuit (IC), using the Texas Instruments LinBiCMOS™ process. The circuit allows the distribution of 3.3-V, 5-V, and/or 12-V card power by means of the P2C (PCMCIA Peripheral-Control) Texas Instruments nonproprietary serial interface. The current-limiting feature eliminates the need for fuses, which reduces component count and improves reliability. Current-limit reporting can help the user isolate a system fault to a specific card.

The TPS2202AI incorporates a reset function, selectable by one of two inputs, to help alleviate system errors. The reset function enables PC Card initialization concurrent with host platform initialization, allowing a system reset. Reset is accomplished by grounding the V_{CC} and V_{pp} (flash-memory programming voltage) outputs, which discharges residual card voltage.

End equipment for the TPS2202AI includes notebook computers, desktop computers, personal digital assistants (PDAs), digital cameras, handterminals, and bar-code scanners. The TPS2202AI is only available taped and reeled (either TPS2202AIDFLE or TPS2202AIDBLE).



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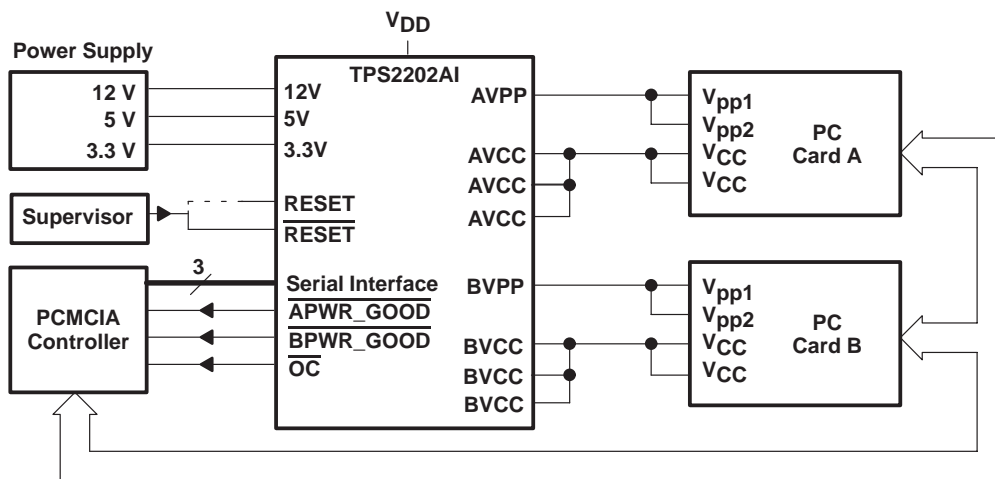
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TPS2202AI

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typical PC card power-distribution application



Terminal Functions

TERMINAL NAME	NO.	I/O	DESCRIPTION
3.3V	15, 16, 17	I	3.3-V V_{CC} input for card power
5V	1, 2, 30	I	5-V V_{CC} input for card power
12V	7, 24	I	12-V V_{pp} input for card power
AVCC	9, 10, 11	O	Switched output that delivers 3.3 V, 5 V, low or high impedance to card
AVPP	8	O	Switched output that delivers 3.3 V, 5 V, 12 V, low or high impedance to card
APWR_GOOD	13	O	Logic-level power-ready output that stays low as long as AVPP is within limits
BVCC	20, 21, 22	O	Switched output that delivers 3.3 V, 5 V, low or high impedance
BVPP	23	O	Switched output that delivers 3.3 V, 5 V, 12 V, low or high impedance
BPWR_GOOD	19	O	Logic-level power-ready output that remains low as long as BVPP is within limits
CLOCK	4	I	Logic-level clock for serial data word
DATA	3	I	Logic-level serial data word
GND	12		Ground
LATCH	5	I	Logic-level latch for serial data word
NC	26, 27, 28, 29		No internal connection
OC	18	O	Logic-level overcurrent reporting output that goes low when an overcurrent condition exists
RESET	6	I	Logic-level RESET input active high. Do not connect if terminal 14 is used.
$\overline{\text{RESET}}$	14	I	Logic-level RESET input active low. Do not connect if terminal 6 is used.
VDD	25	I	5-V power to chip

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absolute maximum ratings over operating free-air temperature (unless otherwise noted)†

Supply voltage range, V_{DD}	-0.3 V to 7 V
Input voltage range for card power: $V_{I(5V)}$	-0.3 V to 7 V
	$V_{I(3.3V)}$ -0.3 V to $V_{I(5V)}$
	$V_{I(12V)}$ -0.3 V to 14 V
Logic input voltage	-0.3 V to 7 V
Continuous total power dissipation	See Dissipation Rating Table
Output current (each card): $I_{O(xVCC)}$	internally limited
	$I_{O(xVPP)}$ internally limited
Operating virtual junction temperature range, T_J	-40°C to 150°C
Operating free-air temperature range, T_A	-40°C to 85°C
Storage temperature range, T_{stg}	-55°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds	260°C

† Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

DISSIPATION RATING TABLE

PACKAGE	$T_A \leq 25^\circ\text{C}$ POWER RATING	DERATING FACTOR‡ ABOVE $T_A = 25^\circ\text{C}$	$T_A = 70^\circ\text{C}$ POWER RATING	$T_A = 85^\circ\text{C}$ POWER RATING
DF	1158 mW	9.26 mW/°C	741 mW	602 mW
DB	1024 mW	8.2 mW/°C	655 mW	532 mW

‡ These devices are mounted on an FR4 board with no special thermal considerations.

recommended operating conditions

	MIN	MAX	UNIT
Supply voltage, V_{DD}	4.75	5.25	V
Input voltage range, V_I	$V_{I(5V)}$	0	5.25
	$V_{I(3.3V)}$	0	$V_{I(5V)}$ §
	$V_{I(12V)}$	0	13.5
Output current	$I_{O(xVCC)}$ at 25°C		1
	$I_{O(xVPP)}$ at 25°C		150
Clock frequency	0	2.5	MHz
Operating virtual junction temperature, T_J	-40	125	°C

§ $V_{I(3.3V)}$ should not be taken above $V_{I(5V)}$.

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electrical characteristics, $T_A = 25^\circ\text{C}$, $V_{DD} = 5\text{ V}$ (unless otherwise noted)

dc characteristics

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
Switch resistances†	5 V to xVCC				160	mΩ
	3.3 V to xVCC				225	
	5 V to xVPP				6	Ω
	3.3 V to xVPP				6	
	12 V to xVPP				1	
$V_O(xVPP)$	Clamp low voltage	I_{pp} at 10 mA			0.8	V
$V_O(xVCC)$	Clamp low voltage	I_{CC} at 10 mA			0.8	V
I_{lkg}	Leakage current	I_{pp} High-impedance state	$T_A = 25^\circ\text{C}$	1	10	μA
			$T_A = 85^\circ\text{C}$		50	
	I_{CC} High-impedance state	$T_A = 25^\circ\text{C}$	1	10		
		$T_A = 85^\circ\text{C}$		50		
I_I	Input current	I_{DD} Supply current	$V_O(AVCC) = V_O(BVCC) = 5\text{ V}$, $V_O(AVPP) = V_O(BVPP) = 12\text{ V}$	83	150	μA
		I_{DD} Supply current in shutdown	$V_O(BVCC) = V_O(AVCC) = V_O(AVPP) = V_O(BVPP) = \text{Hi-Z}$		1	μA
	Power-ready threshold, PWR_GOOD		10.72	11.05	11.4	V
	Power-ready hysteresis, PWR_GOOD	12-V mode		50		mV
Short-circuit output-current limit	$I_O(xVCC)$	$T_J = 85^\circ\text{C}$, Output powered up into a short to GND	0.75	1.3	1.9	A
	$I_O(xVPP)$		120	200	400	mA

† Pulse-testing techniques are used to maintain junction temperature close to ambient temperature; thermal effects must be taken into account separately.

logic section

PARAMETER	TEST CONDITIONS	MIN	MAX	UNIT
Logic input current			1	μA
Logic input high level		2		V
Logic input low level			0.8	V
Logic output high level	$I_O = 1\text{ mA}$	$V_{DD} - 0.4$		V
Logic output low level			0.4	V
Logic input minimum pulse width		1		μs

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switching characteristics†

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT	
t _r	Output rise times	V _O (xVCC)			1.2		ms	
		V _O (xVPP)			5			
t _f	Output fall times	V _O (xVCC)			10			
		V _O (xVPP)			14			
t _{pd}	Propagation delay (see Figure 1‡)	LATCH↑ to V _O (xVPP)	t _{on}		5.8			ms
			t _{off}		18			ms
		LATCH↑ to xVCC (3 V)	t _{on}		5.8		ms	
			t _{off}		28		ms	
		LATCH↑ to xVCC (5 V)	t _{on}		4		ms	
			t _{off}		30		ms	

† Refer to Parameter Measurement Information

‡ Propagation delays are with C_L = 100 μF.

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PARAMETER MEASUREMENT INFORMATION

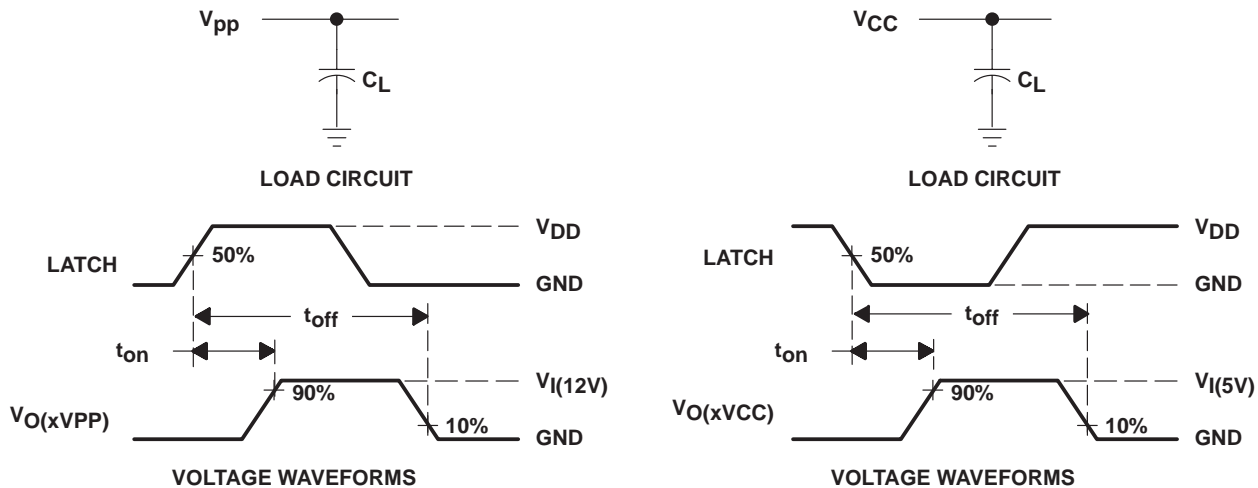
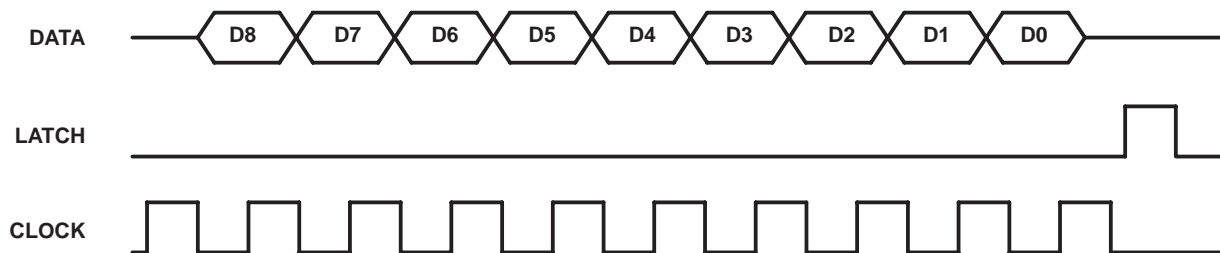


Figure 1. Test Circuits and Voltage Waveforms

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xVPP Propagation Delay and Fall Time With 100- μ F Load, 12-V Switch	14



NOTE A: Data is clocked in on the positive leading edge of the clock. The latch should occur before next positive leading edge of the clock. For definition of D0 to D8, see the control logic table.

Figure 2. Serial-Interface Timing

PARAMETER MEASUREMENT INFORMATION

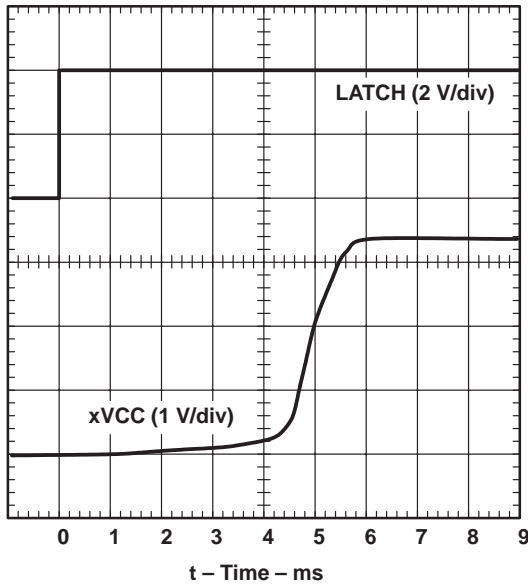


Figure 3. xVCC Propagation Delay and Rise Time With 1- μ F Load, 3.3-V Switch

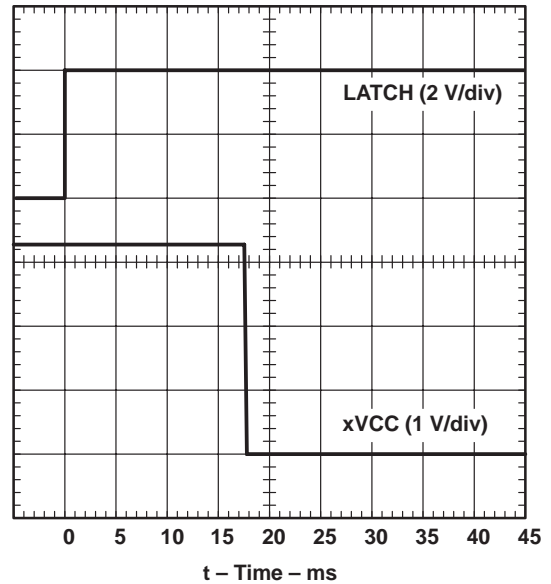


Figure 4. xVCC Propagation Delay and Fall Time With 1- μ F Load, 3.3-V Switch

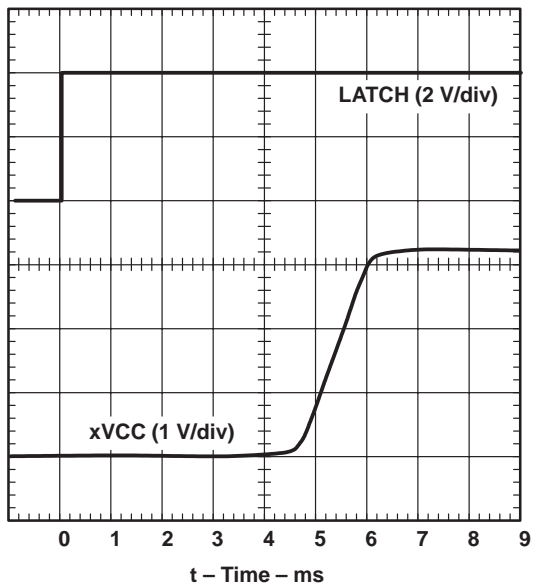


Figure 5. xVCC Propagation Delay and Rise Time With 100- μ F Load, 3.3-V Switch

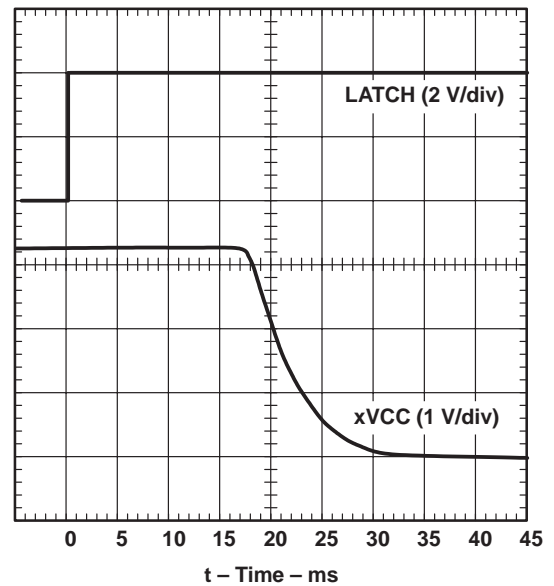


Figure 6. xVCC Propagation Delay and Fall Time With 100- μ F Load, 3.3-V Switch

PARAMETER MEASUREMENT INFORMATION

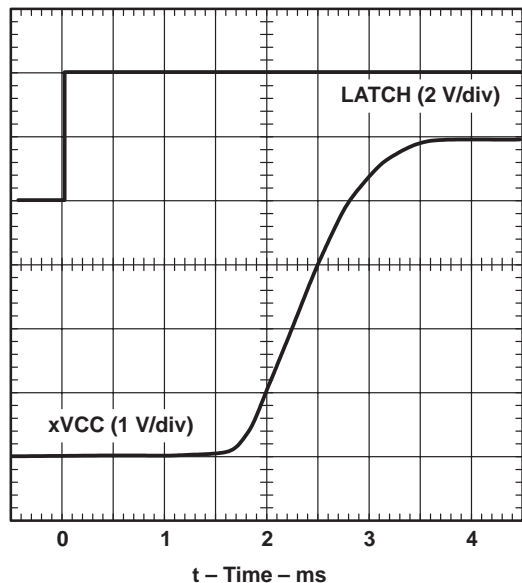


Figure 7. xVCC Propagation Delay and Rise Time With 1- μ F Load, 5-V Switch

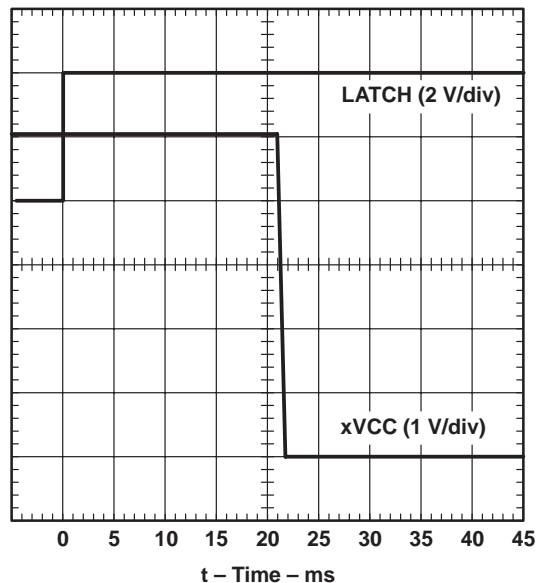


Figure 8. xVCC Propagation Delay and Fall Time With 1- μ F Load, 5-V Switch

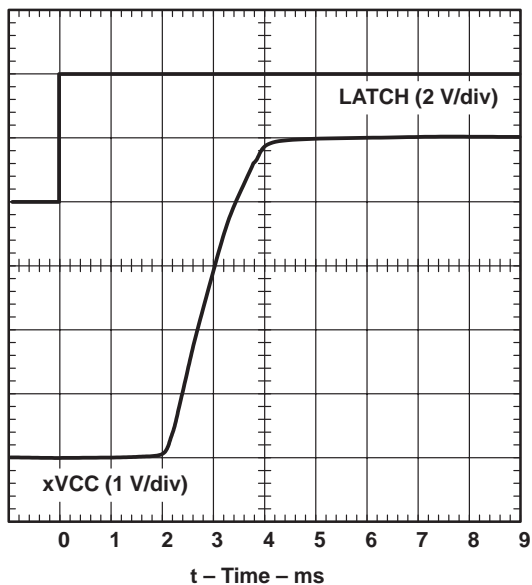


Figure 9. xVCC Propagation Delay and Rise Time With 100- μ F Load, 5-V Switch

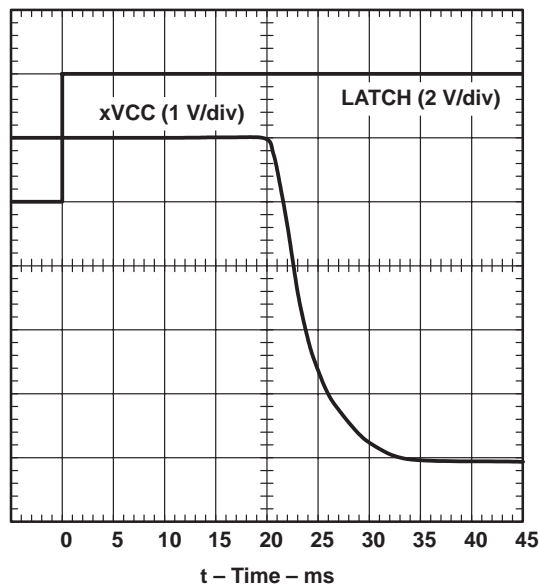


Figure 10. xVCC Propagation Delay and Fall Time With 100- μ F Load, 5-V Switch

PARAMETER MEASUREMENT INFORMATION

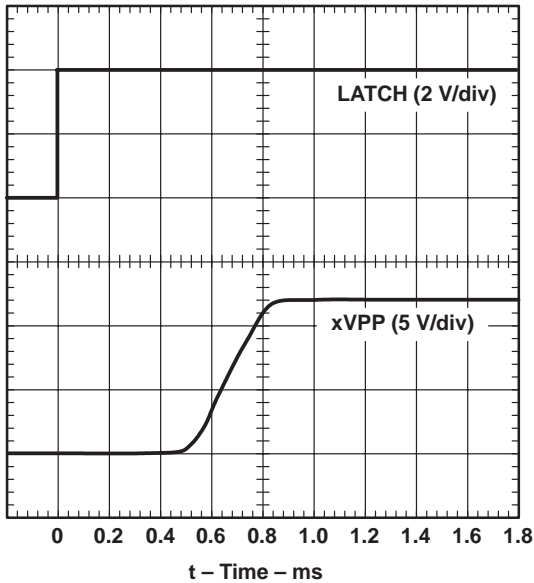


Figure 11. xVPP Propagation Delay and Rise Time With 1- μ F Load, 12-V Switch

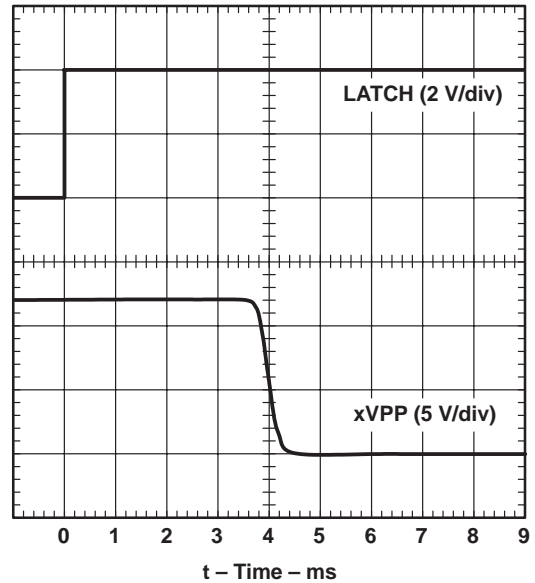


Figure 12. xVPP Propagation Delay and Fall Time With 1- μ F Load, 12-V Switch

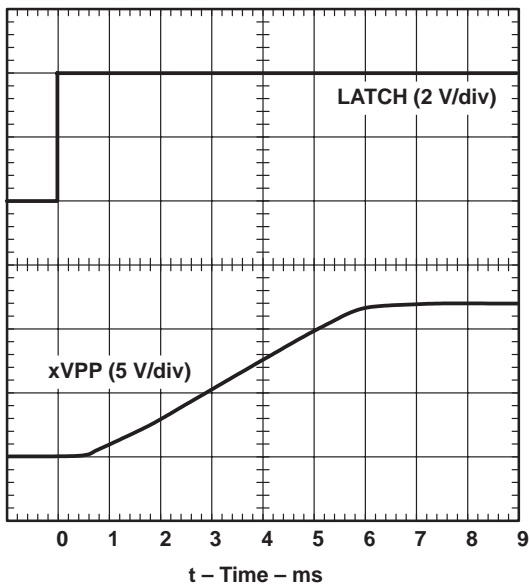


Figure 13. xVPP Propagation Delay and Rise Time With 100- μ F Load, 12-V Switch

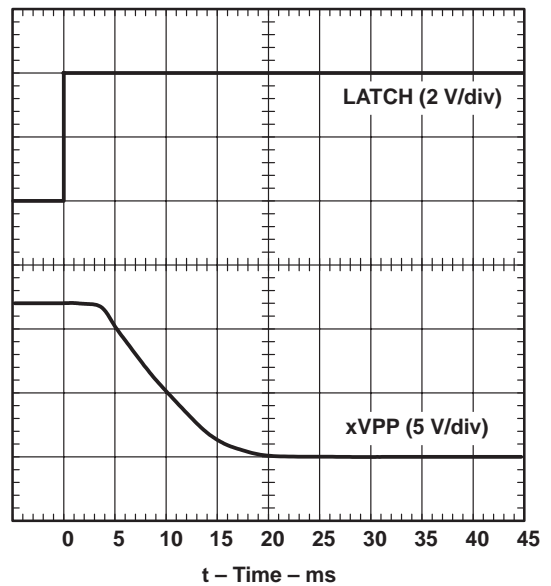


Figure 14. xVPP Propagation Delay and Fall Time With 100- μ F Load, 12-V Switch

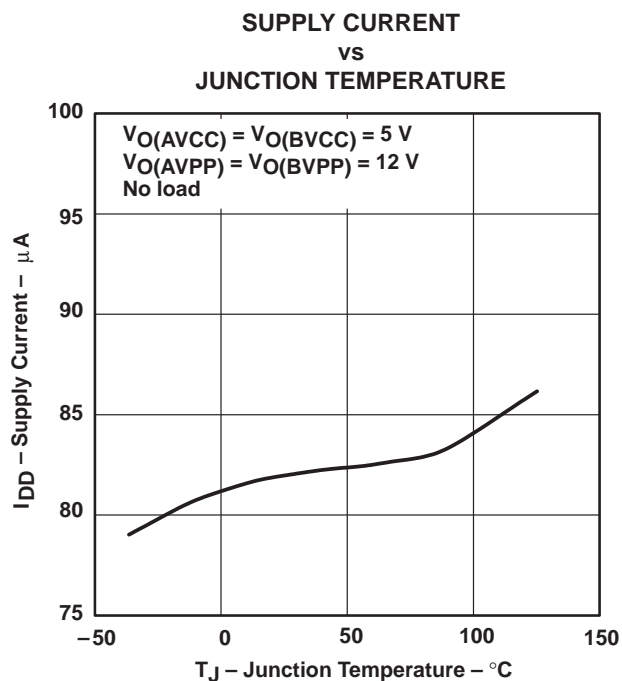
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TYPICAL CHARACTERISTICS†

Table of Graphs

			FIGURE
I_{DD}	Supply current	vs Junction temperature	15
$r_{DS(on)}$	Static drain-source on-state resistance, 3-V switch	vs Junction temperature	16
$r_{DS(on)}$	Static drain-source on-state resistance, 5-V switch	vs Junction temperature	17
$r_{DS(on)}$	Static drain-source on-state resistance, 12-V switch	vs Junction temperature	18
$V_O(xVCC)$	Output voltage, 5-V switch	vs Output current	19
$V_O(xVCC)$	Output voltage, 3.3-V switch	vs Output current	20
xV_{pp}	Output voltage, V_{pp} switch	vs Output current	21
$I_{SC}(xVCC)$	Short-circuit current, 5-V switch	vs Junction temperature	22
$I_{SC}(xVPP)$	Short-circuit current, 12-V switch	vs Junction temperature	23



† t = pulse tested

TYPICAL CHARACTERISTICS†

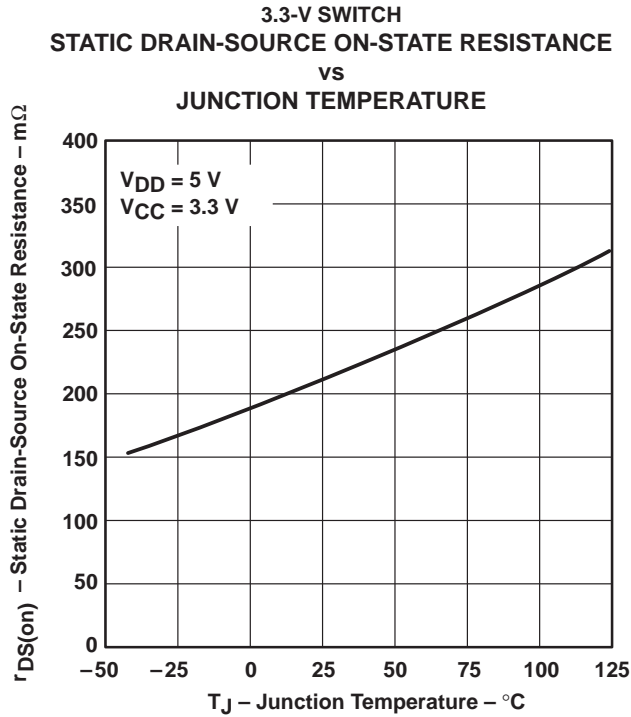


Figure 16

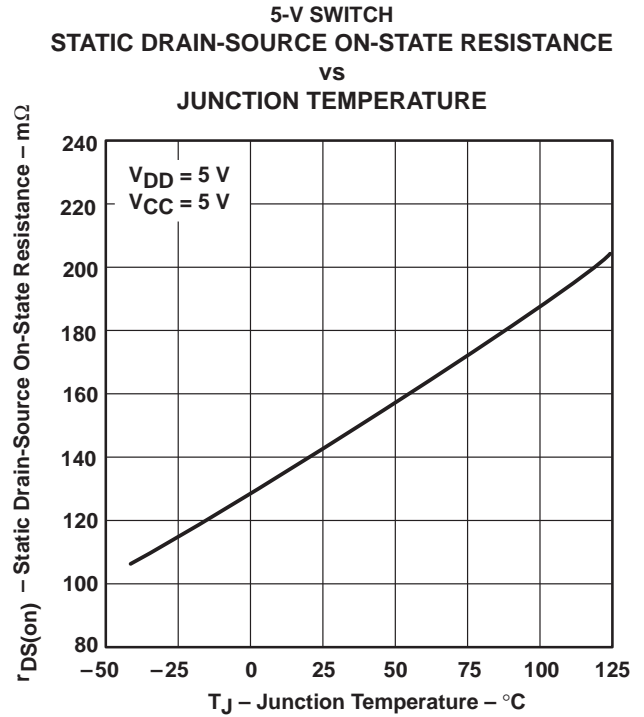


Figure 17

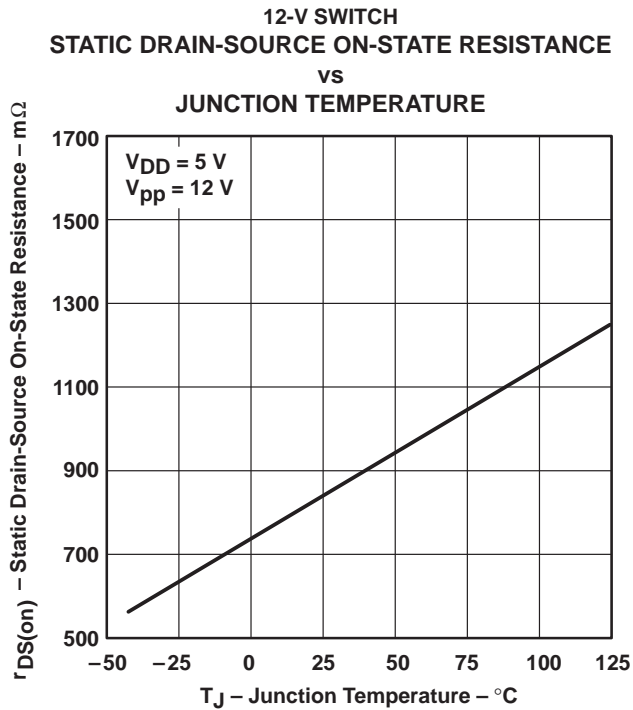


Figure 18

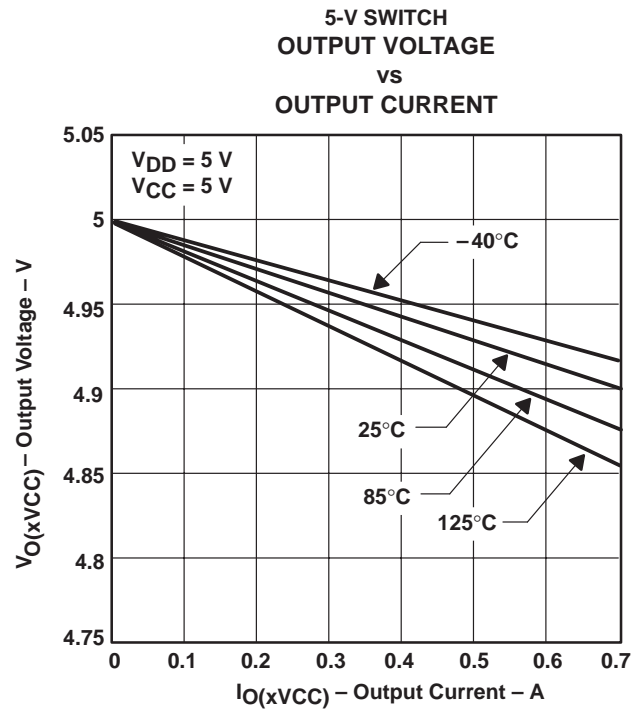


Figure 19

† t = pulse tested

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TYPICAL CHARACTERISTICS†

**3-V SWITCH
 OUTPUT VOLTAGE
 VS
 OUTPUT CURRENT**

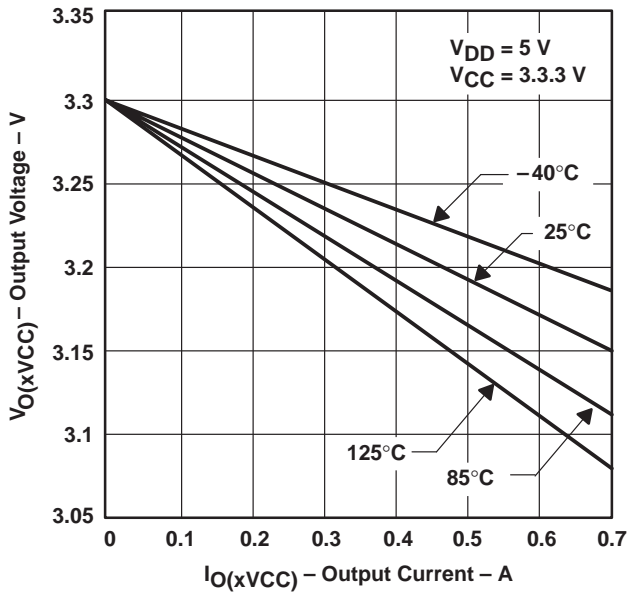


Figure 20

**V_{pp} SWITCH
 OUTPUT VOLTAGE
 VS
 OUTPUT CURRENT**

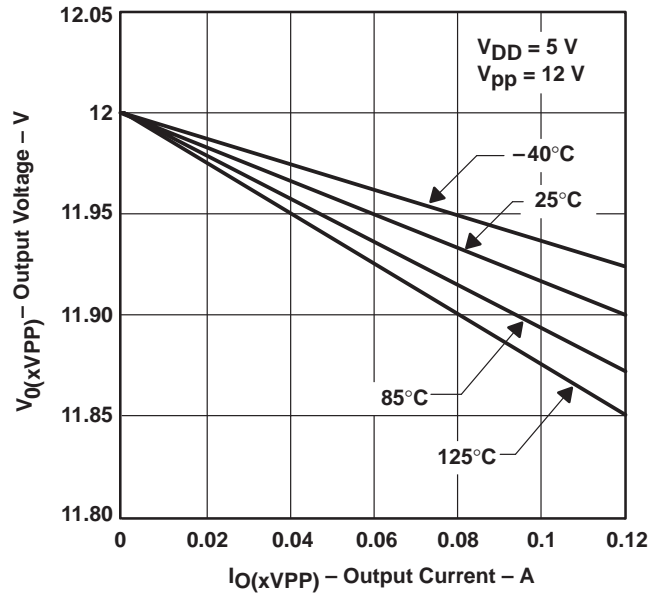


Figure 21

**5-V SWITCH
 SHORT-CIRCUIT CURRENT
 VS
 JUNCTION TEMPERATURE**

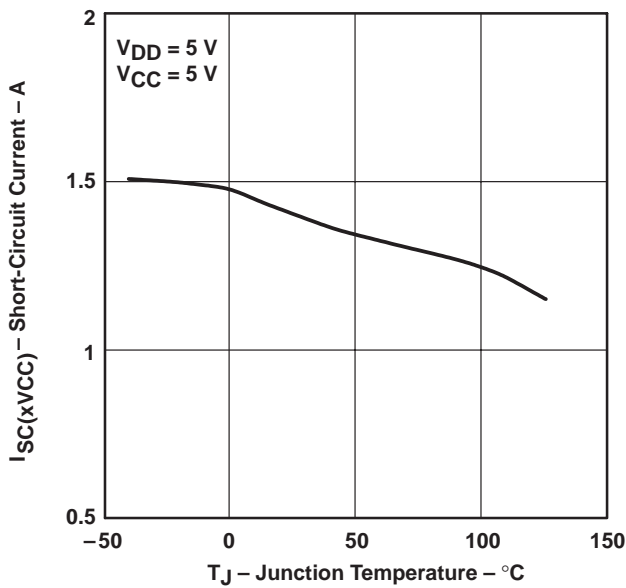


Figure 22

**12-V SWITCH
 SHORT-CIRCUIT CURRENT
 VS
 JUNCTION TEMPERATURE**

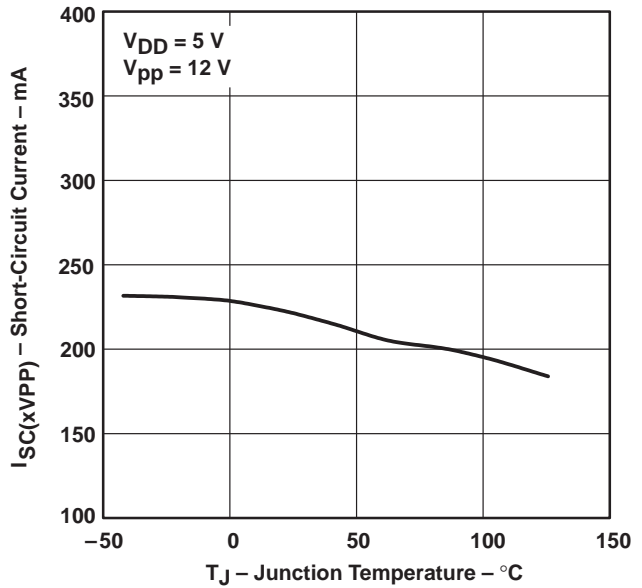


Figure 23

† t = pulse tested

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APPLICATION INFORMATION

overview

PC Cards were initially introduced as a means to add EEPROM (flash memory) to portable computers with limited on-board memory. The idea of add-in cards quickly took hold; modems, wireless LANs, GPS systems, multimedia, and hard-disk versions were soon available. As the number of PC Card applications grew, the engineering community quickly recognized the need for a standard to ensure compatibility across platforms. To this end, the PCMCIA (Personal Computer Memory Card International Association) was established, comprised of members from leading computer, software, PC card, and semiconductor manufacturers. One key goal was to realize the “plug and play” concept. Cards and hosts from different vendors should be compatible and able to communicate with one another transparently.

PC Card power specification

System compatibility also means power compatibility. The most current set of specifications (PC Card Standard) set forth by the PCMCIA committee states that power is to be transferred between the host and the card through eight of the PC Card connector's 68 terminals. This power interface consists of two V_{CC} , two V_{pp} , and four ground terminals. Multiple V_{CC} and ground terminals minimize connector-terminal and line resistance. The two V_{pp} terminals were originally specified as separate signals but are commonly tied together in the host to form a single node to minimize voltage losses. Card primary power is supplied through the V_{CC} terminals; flash-memory programming and erase voltage is supplied through the V_{pp} terminals. As each terminal is rated to 0.5 A, V_{CC} and V_{pp} can theoretically supply up to 1 A, assuming equal terminal resistance and no terminal failure. A conservative design would limit current to 500 mA. Some applications, however, require higher V_{CC} currents. Disk drives, for example, may need as much as 750-mA peak current to create the initial torque necessary to spin up the platter. V_{pp} currents, on the other hand, are defined by flash-memory programming requirements, typically under 120 mA.

future power trends

The 1-A physical-terminal current alluded to in the PC Card specification has caused some host-system engineers to believe they are required to deliver 1 A within the voltage tolerance of the card. Future applications, such as RF cards, could use the extra power for their radio transmitters. The 5 W required for these cards require very robust power supplies and special cooling considerations. The limited number of host sockets that are able to support cards makes the market for these high-powered PC Cards uncertain. The vast majority of the cards require less than 600 mA continuous current, and the trend is towards even lower powered PC Cards that assure compatibility with a greater number of host systems. Recognizing the need for power derating, an ad hoc committee of the PCMCIA is currently working to limit the amount of steady-state dc current to the PC Card to something less than the currently implied 1 A. When a system is designed to support 1 A, the switch $r_{DS(on)}$, power-supply requirements, and PC Card cooling need to be carefully considered.

designing around 1-A delivery

Delivering 1 A means minimizing voltage and power losses across the PC Card power interface, which requires that designers trade off switch resistance and the cost associated with large-die (low $r_{DS(on)}$) MOSFET transistors. The PC Card standard requires that 5 V $\pm 5\%$ or 3.3 V ± 0.3 V be supplied to the card. The approximate 10% tolerance for the 3.3-V supply makes the 3.3-V $r_{DS(on)}$ less critical than the 5-V switch. A conservative approach is to allow 2% for voltage-regulator tolerance and 1% for etch- and pin-resistance drops, which leaves 2% (100 mV) for voltage drop at the 5-V switch and at least 6% (198 mV) for the 3.3-V switch.

Calculating the $r_{DS(on)}$ necessary to support a 100 mV or 198 mV switch loss, using $R = E/I$ and setting $I = 1$ A, the 5-V and 3.3-V switches would need to be 100 m Ω and 198 m Ω respectively. One solution would be to pay for a more expensive switch with lower $r_{DS(on)}$. A second, less expensive approach is to increase the headroom of the power supply—for example, to increase the 5 V supply 1.5% or to 5.075 $\pm 2\%$. Working through the numbers once more, the 2% for the regulator plus 1 % for etch and terminal losses leaves 97% or 4.923 V. The allowable

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APPLICATION INFORMATION

designing around 1-A delivery (continued)

voltage loss across the power distribution switch is now 4.923 V minus 4.750 V or 173 mV. Therefore, a switch with 173 m Ω or less could deliver 1 A or greater. Setting the power supply high is a common practice for delivering voltages to allow for system switch connector and etch losses. This practice has a minimal effect on overall battery life. In the example above, setting the power supply 1.5% high would only decrease a 3-hour battery life by approximately 2.7 minutes, trivial when compared with the decrease in battery life when running a 5-W PC Card.

heat dissipation

A greater concern in delivering 1 A or 5 W is the ability of the host to dissipate the heat generated by the PC Card. For desktop computers the solution is simpler: locate the PC Card cage such that it receives convection cooling from the forced air of the fan. Notebooks and other handheld equipment will not be able to rely on convection, but on conduction of heat away from the PC Card through the rails into the card cage. This is difficult because PC Card/card cage heat transfer is very poor. A typical design scenario would require the PC Card to be held at 60°C maximum with the host platform operating as high as 50°C. Preliminary testing reveals that a PC Card can have a 20°C rise, exceeding the 10°C differential in the example, when dissipating less than 2 W of continuous power. Sixty degrees centigrade was chosen because it is the maximum operating temperature allowable by PC Card specification. Power handling requirements and temperature rises are topics of concern and are currently being addressed by the PCMCIA committee.

overcurrent and over-temperature protection

PC Cards are inherently subject to damage that can result from mishandling. Host systems require protection against short-circuited cards that could lead to power supply or PCB-trace damage. Even systems sufficiently robust to withstand a short circuit would still undergo rapid battery discharge into the damaged PC Card, resulting in the rather sudden and unacceptable loss of system power. Most hosts include fuses for protection. The reliability of fused systems is poor though, as blown fuses require troubleshooting and repair, usually by the manufacturer.

The TPS2202AI takes a two-pronged approach to overcurrent protection. First, instead of fuses, sense FETs monitor each of the power outputs. Excessive current generates an error signal that linearly limits the output current, preventing host damage or failure. Sense FETs, unlike sense resistors or polyfuses, have an added advantage in that they do not add to the series resistance of the switch and thus produce no additional voltage losses. Second, when an overcurrent condition is detected, the TPS2202AI asserts a signal at \overline{OC} that can be monitored by the microprocessor to initiate diagnostics and/or send the user a warning message. In the event that an overcurrent condition persists, causing the IC to exceed its maximum junction temperature, thermal-protection circuitry activates, shutting down all power outputs until the device cools to within a safe operating region.

12-V supply not required

Most PC Card switches use the externally supplied 12-V V_{pp} power for switch-gate drive and other chip functions, which requires that power be present at all times. The TPS2202AI offers considerable power savings by using an internal charge pump to generate the required higher voltages from the 5-V V_{DD} supply; therefore, the external 12-V supply can be disabled except when needed for flash-memory functions, thereby extending battery lifetime. Do not ground the 12-V inputs when 12-V supply is not in use. Additional power savings are realized by the TPS2202AI during a software shutdown in which quiescent current drops to a maximum of 1 μ A.

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voltage transitioning requirement

PC Cards, like portables, are migrating from 5 V to 3.3 V to minimize power consumption, optimize board space, and increase logic speeds. The TPS2202AI is designed to meet all combinations of power delivery as currently defined in the PCMCIA standard. The latest protocol accommodates mixed 3.3-V/5-V systems by first powering the card with 5 V, then polling it to determine its 3.3-V compatibility. The PCMCIA specification requires that the capacitors on 3.3-V-compatible cards be discharged to below 0.8 V before applying 3.3-V power. This ensures that sensitive 3.3-V circuitry is not subjected to any residual 5-V charge and functions as a power reset. The TPS2202AI offers a selectable V_{CC} and V_{pp} ground state, in accordance with PCMCIA 3.3-V/5-V switching specifications, to fully discharge the card capacitors while switching between V_{CC} voltages.

output ground switches

Several PCMCIA power-distribution switches on the market do not have an active-grounding FET switch. These devices do not meet the PC Card specification requiring a discharge of V_{CC} within 100 ms. PC Card resistance can not be relied on to provide a discharge path for voltages stored on PC Card capacitance because of possible high-impedance isolation by power-management schemes. A method commonly shown to alleviate this problem is to add to the switch output an external 100 k Ω resistor in parallel with the PC Card. Considering that this is the only discharge path to ground, a timing analysis will reveal that the RC time constant delays the required discharge time to more than 2 seconds. The only way to ensure timing compatibility with PC Card standards is to use a power-distribution switch that has an internal ground switch, like that of the TPS22xx family, or add an external ground FET to each of the output lines with the control logic necessary to select it.

In summary, the TPS2202AI is a complete single-chip dual-slot PC Card power interface. It meets all currently defined PCMCIA specifications for power delivery in 5-V, 3.3-V, and mixed systems, and offers a serial controller interface. The TPS2202AI offers functionality, power savings, overcurrent and thermal protection, and fault reporting in one 30-pin SSOP surface-mount package for maximum value added to new portable designs.

power supply considerations

The TPS2202AI has multiple pins for each of its 3.3-V, 5-V, and 12-V power inputs and for the switched V_{CC} outputs. Any individual pin can conduct the rated input or output current. Unless all pins are connected in parallel, the series resistance is significantly higher than that specified, resulting in increased voltage drops and lost power. Both 12-V inputs must be connected for proper V_{pp} switching; it is recommended that all input and output power pins be paralleled for optimum operation. The V_{DD} input lead must be connected to the 5-V input leads.

Although the TPS2202AI is fairly immune to power input fluctuations and noise, it is generally considered good design practice to bypass power supplies typically with a 1- μ F electrolytic or tantalum capacitor paralleled by a 0.047- μ F to 0.1- μ F ceramic capacitor. It is strongly recommended that the switched V_{CC} and V_{pp} outputs be bypassed with a 0.1- μ F or larger capacitor; doing so improves the immunity of the TPS2202AI to electrostatic discharge (ESD). Care should be taken to minimize the inductance of PCB traces between the TPS2202AI and the load. High switching currents can produce large negative-voltage transients, which forward biases substrate diodes, resulting in unpredictable performance.

The TPS2202AI, unlike other PC Card power-interface switches, does not use the 12-V power supply for switching or other chip functions. Instead, an internal charge pump generates the necessary voltage from V_{DD} , allowing the 12-V input supply to be shut down except when the V_{pp} programming or erase voltage is needed. Careful system design using this feature reduces power consumption and extends battery lifetime.

The 3.3-V power input should not be taken higher than the 5-V input. Though doing so is nondestructive, this results in high current flow into the device and could result in abnormal operation. In any case, this occurrence indicates a malfunction of one input voltage or both which should be investigated.

Similarly, no pin should be taken below -0.3 V; forward biasing the parasitic-substrate diode results in substrate currents and unpredictable performance.

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RESET or $\overline{\text{RESET}}$ inputs

To ensure that cards are in a known state after power brownouts or system initialization, the PC Cards should be reset at the same time as the host by applying a low impedance to the V_{CC} and V_{pp} terminals. A low-impedance output state allows discharging of residual voltage remaining on PC Card filter capacitance, permitting the system (host and PC Cards) to be powered up concurrently. The RESET or $\overline{\text{RESET}}$ input will close internal switches S1, S4, S7, and S10 with all other switches left open (see TPS2202AI control-logic table). The TPS2202AI remains in the low-impedance output state until the signal is deasserted and further data is clocked in and latched. RESET or $\overline{\text{RESET}}$ is provided for direct compatibility with systems that use either an active-low or active-high reset voltage supervisor. The unused pin is internally pulled up or down and should be left unconnected.

overcurrent and thermal protection

The TPS2202AI uses sense FETs to check for overcurrent conditions in each of the V_{CC} and V_{pp} outputs. Unlike sense resistors or polyfuses, these FETs do not add to the series resistance of the switch; therefore, voltage and power losses are reduced. Overcurrent sensing is applied to each output separately. When an overcurrent condition is detected, only the power output affected is limited; all other power outputs continue to function normally. The $\overline{\text{OC}}$ indicator, normally a logic high, is a logic low when any overcurrent condition is detected, providing for initiation of system diagnostics and/or sending a warning message to the user.

During power up, the TPS2202AI controls the rise time of the V_{CC} and V_{pp} outputs and limits the current into a faulty card or connector. If a short circuit is applied after power is established (e.g., hot insertion of a bad card), current is initially limited only by the impedance between the short and the power supply. In extreme cases, as much as 10 A to 15 A may flow into the short before the current limiting of the TPS2202AI engages. If the V_{CC} or V_{pp} outputs are driven below ground, the TPS2202AI may latch nondestructively in an off state. Cycling power will reestablish normal operation.

Overcurrent limiting for the V_{CC} outputs is designed to activate, if powered up, into a short in the range of 0.75 A to 1.9 A, typically at about 1.3 A. The V_{pp} outputs limit from 120 mA to 400 mA, typically around 200 mA. The protection circuitry acts by linearly limiting the current passing through the switch rather than initiating a full shutdown of the supply. Shutdown occurs only during thermal limiting.

Thermal limiting prevents destruction of the IC from overheating if the package power-dissipation ratings are exceeded. Thermal limiting disables all power outputs (both A and B slots) until the device has cooled.

calculating junction temperature

The switch resistance, $r_{DS(on)}$, is dependent on the junction temperature, T_J , of the die. The junction temperature is dependent on both $r_{DS(on)}$ and the current through the switch. To calculate T_J , first find $r_{DS(on)}$ from Figures 16, 17, and 18 using an initial temperature estimate about 50°C above ambient. Then calculate the power dissipation for each switch, using the formula:

$$P_D = r_{DS(on)} \times I^2$$

Next, sum the power dissipation and calculate the junction temperature:

$$T_J = \left(\sum P_D \times R_{\theta JA} \right) + T_A, \quad R_{\theta JA} = 108^\circ\text{C/W}$$

Compare the calculated junction temperature with the initial temperature estimate. If the temperatures are not within a few degrees of each other, recalculate using the calculated temperature as the initial estimate.

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logic input and outputs

The serial interface consists of DATA, CLOCK, and LATCH leads. The data is clocked in on the positive leading edge of the clock (see Figure 2). The 9-bit (D0 through D8) serial data word is loaded during the positive edge of the latch signal. The latch signal should occur before the next positive leading edge of the clock.

The shutdown bit of the data word places all V_{CC} and V_{pp} outputs in a high-impedance state and reduces chip quiescent current to 1 μA to conserve battery power.

The TPS2202AI serial interface is designed to be compatible with serial-interface PCMCIA controllers and current PCMCIA and Japan Electronic Industry Development Association (JEIDA) standards.

An overcurrent output (\overline{OC}) is provided to indicate an overcurrent condition in any of the V_{CC} or V_{pp} outputs as previously discussed.

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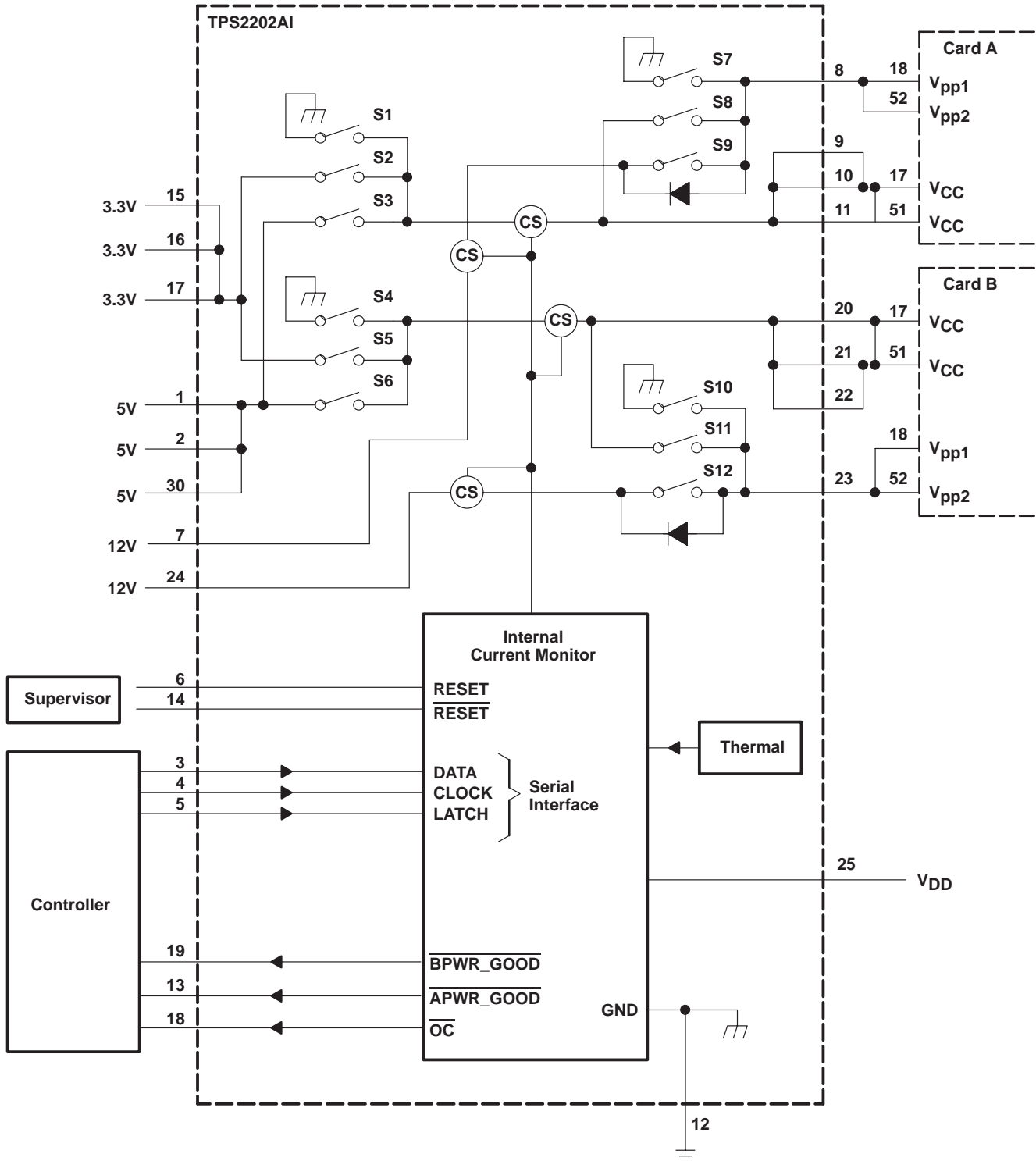


Figure 24. Internal Switching Matrix

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TPS2202AI control logic

AVPP

CONTROL SIGNALS			INTERNAL SWITCH SETTINGS			OUTPUT
D8 SHDN	D0 A_VPP_PGM	D1 A_VPP_VCC	S7	S8	S9	VAVPP
1	0	0	CLOSED	OPEN	OPEN	0 V
1	0	1	OPEN	CLOSED	OPEN	VCC†
1	1	0	OPEN	OPEN	CLOSED	VPP(12 V)
1	1	1	OPEN	OPEN	OPEN	Hi-Z
0	X	X	OPEN	OPEN	OPEN	Hi-Z

BVPP

CONTROL SIGNALS			INTERNAL SWITCH SETTINGS			OUTPUT
D8 SHDN	D4 B_VPP_PGM	D5 B_VPP_VCC	S10	S11	S12	VBVPP
1	0	0	CLOSED	OPEN	OPEN	0 V
1	0	1	OPEN	CLOSED	OPEN	VCC‡
1	1	0	OPEN	OPEN	CLOSED	VPP(12 V)
1	1	1	OPEN	OPEN	OPEN	Hi-Z
0	X	X	OPEN	OPEN	OPEN	Hi-Z

AVCC

CONTROL SIGNALS			INTERNAL SWITCH SETTINGS			OUTPUT
D8 SHDN	D3 A_VCC3	D2 A_VCC5	S1	S2	S3	VAVCC
1	0	0	CLOSED	OPEN	OPEN	0 V
1	0	1	OPEN	CLOSED	OPEN	3.3 V
1	1	0	OPEN	OPEN	CLOSED	5 V
1	1	1	CLOSED	OPEN	OPEN	0 V
0	X	X	OPEN	OPEN	OPEN	Hi-Z

BVCC

CONTROL SIGNALS			INTERNAL SWITCH SETTINGS			OUTPUT
D8 SHDN	D6 B_VCC3	D7 B_VCC5	S4	S5	S6	VBVCC
1	0	0	CLOSED	OPEN	OPEN	0 V
1	0	1	OPEN	CLOSED	OPEN	3.3 V
1	1	0	OPEN	OPEN	CLOSED	5 V
1	1	1	CLOSED	OPEN	OPEN	0 V
0	X	X	OPEN	OPEN	OPEN	Hi-Z

† Output depends on AVCC

‡ Output depends on BVCC

ESD protection

All TPS2202AI inputs and outputs incorporate ESD-protection circuitry designed to withstand a 2-kV human-body-model discharge as defined in MIL-STD-883C, Method 3015. The V_{CC} and V_{pp} outputs can be exposed to potentially higher discharges from the external environment through the PC Card connector. Bypassing the outputs with 0.1-μF capacitors protects the devices from discharges up to 10 kV.

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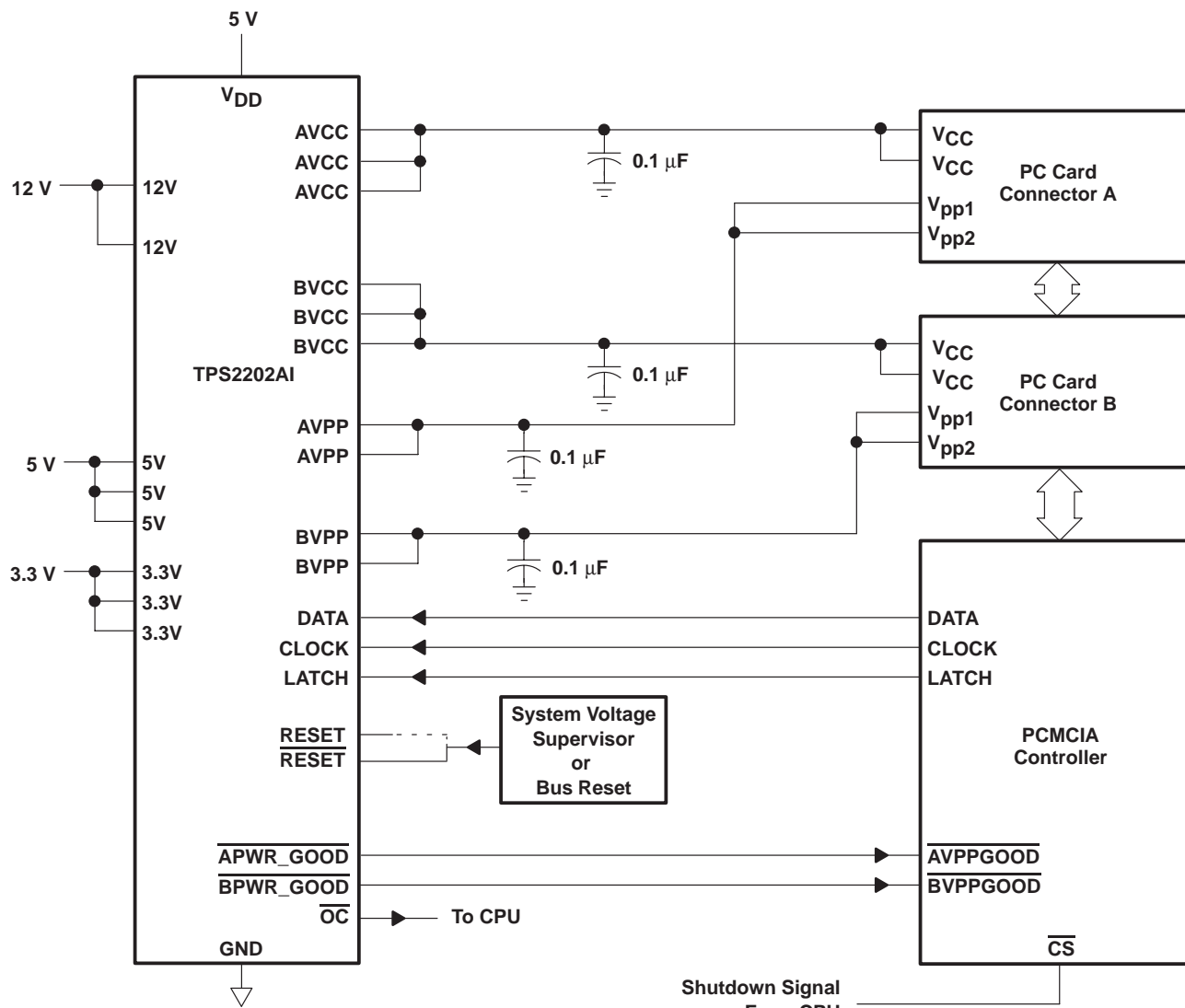


Figure 25. Detailed Interconnections and Capacitor Recommendations

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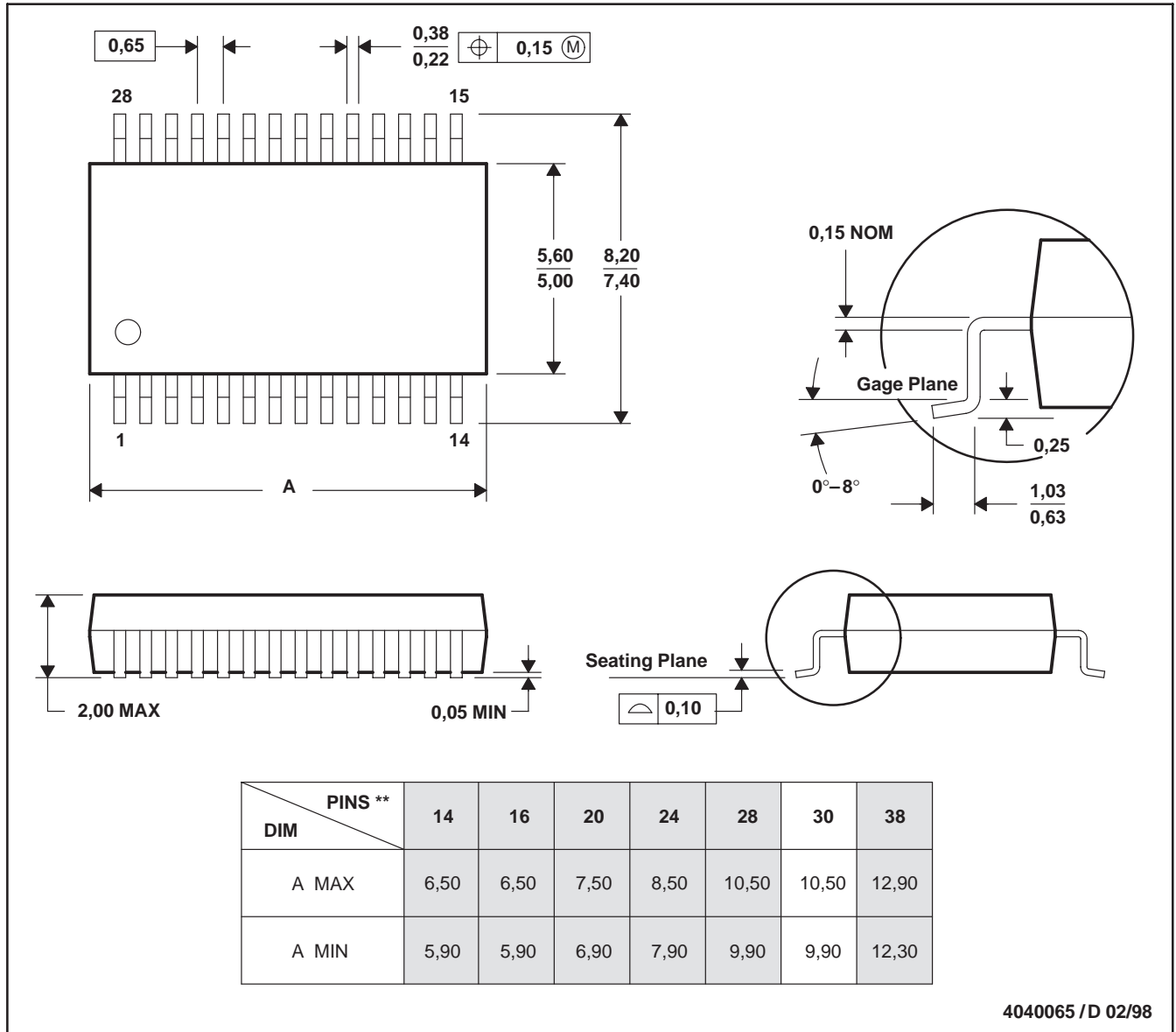
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MECHANICAL DATA

DB (R-PDSO-G)**

PLASTIC SMALL-OUTLINE PACKAGE

28 PIN SHOWN



- NOTES: A. All linear dimensions are in millimeters.
 B. This drawing is subject to change without notice.
 C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
 D. Falls within JEDEC MO-150

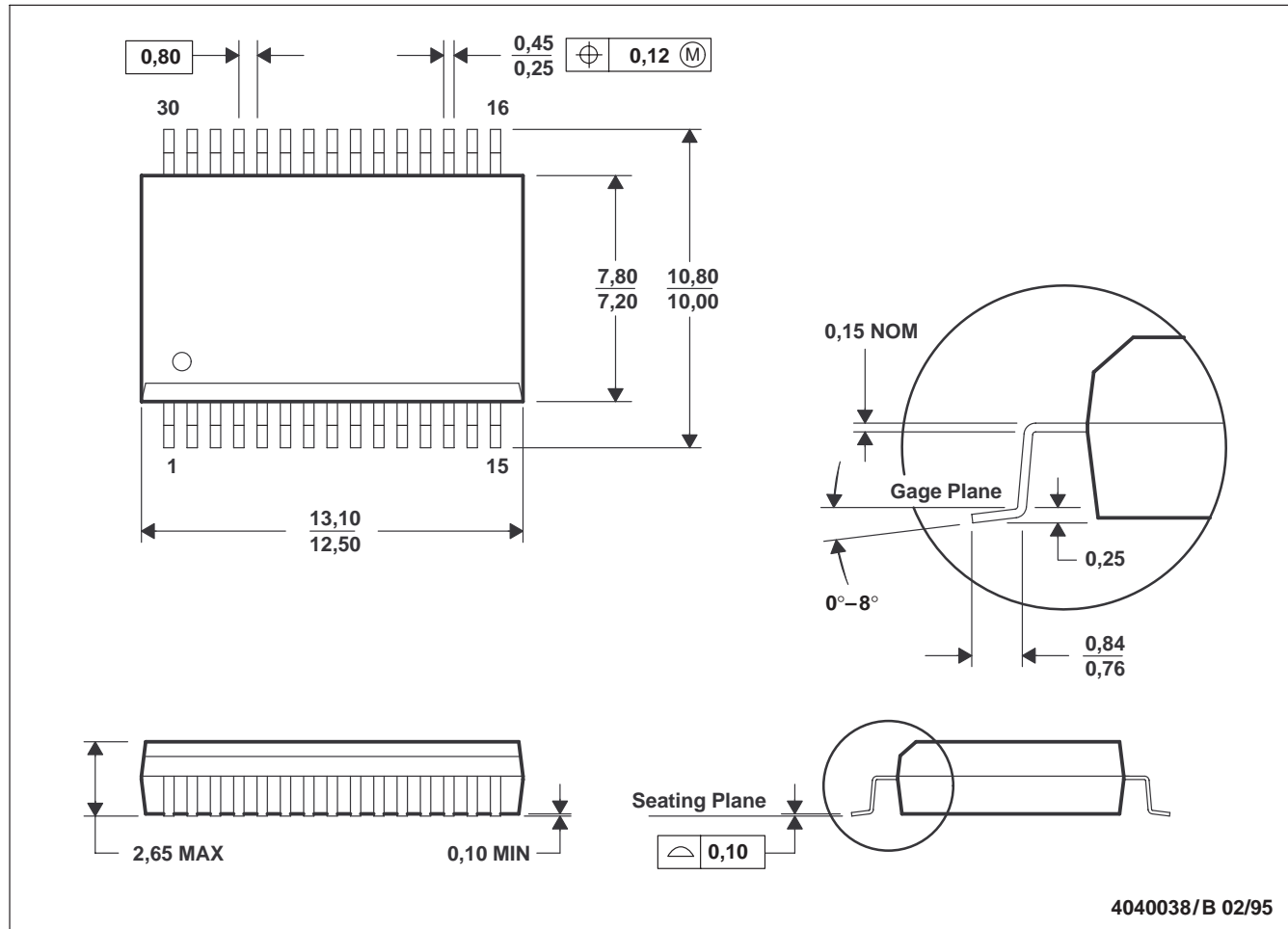
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MECHANICAL DATA

DF (R-PDSO-G30)

PLASTIC SMALL-OUTLINE PACKAGE



4040038/B 02/95

NOTES: A. All linear dimensions are in millimeters.
 B. This drawing is subject to change without notice.

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