

# LT1124/LT1125

# GY Dual/Quad Low Noise, High Speed Precision Op Amps

#### **FEATURES**

■ 100% Tested Low Voltage Noise: 2.7nV/√Hz Typ 4.2nV/√Hz Max

■ Slew Rate: 4.5V/µs Typ

 Gain Bandwidth Product: 12.5MHz Typ
 Offset Voltage, Prime Grade: 70μV Max Low Grade: 100μV Max

High Voltage Gain: 5 Million Min

Supply Current Per Amplifier: 2.75mA Max

Common Mode Rejection: 112dB MinPower Supply Rejection: 116dB Min

Available in 8-Pin SO Package

#### **APPLICATIONS**

Two and Three Op Amp Instrumentation Amplifiers

- Low Noise Signal Processing
- Active Filters
- Microvolt Accuracy Threshold Detection
- Strain Gauge Amplifiers
- Direct Coupled Audio Gain Stages
- Tape Head Preamplifiers
- Infrared Detectors

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### DESCRIPTION

The LT $^{\circ}$ 1124 dual and LT1125 quad are high performance op amps that offer higher gain, slew rate and bandwidth than the industry standard OP-27 and competing OP-270/OP-470 op amps. In addition, the LT1124/LT1125 have lower I<sub>B</sub> and I<sub>OS</sub> than the OP-27; lower V<sub>OS</sub> and noise than the OP-270/OP-470.

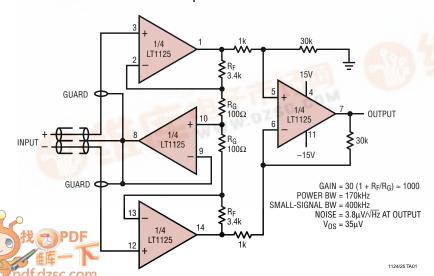
In the design, processing and testing of the device, particular attention has been paid to the optimization of the entire distribution of several key parameters. Slew rate, gain bandwidth and 1kHz noise are 100% tested for each individual amplifier. Consequently, the specifications of even the lowest cost grades (the LT1124C and the LT1125C) have been spectacularly improved compared to equivalent grades of competing amplifiers.

Power consumption of the LT1124 is one half of two OP-27s. Low power and high performance in an 8-pin SO package make the LT1124 a first choice for surface mounted systems and where board space is restricted.

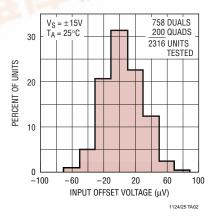
For a decompensated version of these devices, with three times higher slew rate and bandwidth, please see the LT1126/LT1127 data sheet.

## TYPICAL APPLICATION

#### **Instrumentation Amplifier with Shield Driver**



# Input Offset Voltage Distribution (All Packages, LT1124 and LT1125)

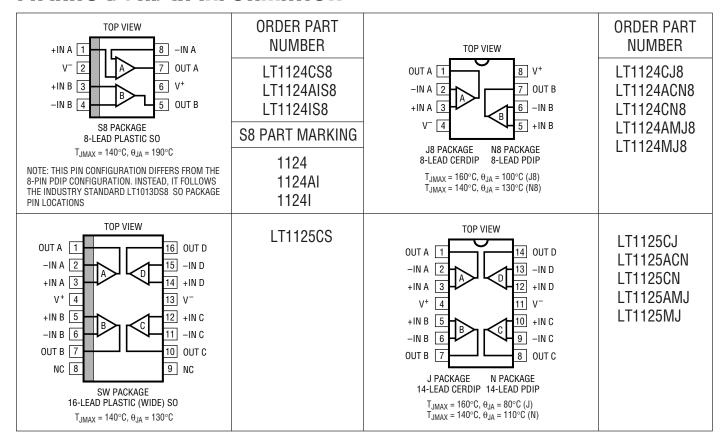


## **ABSOLUTE MAXIMUM RATINGS** (Note 1)

Supply Voltage	±22V
Input Voltages	Equal to Supply Voltage
Output Short-Circuit Duration	Indefinite
Differential Input Current (Note	6) ±25mA
Lead Temperature (Soldering, 1	0 sec) 300°C
Storage Temperature Range	65°C to 150°C

Operating Temperature Range
LT1124AC/LT1124C
LT1125AC/LT1125C (Note 10) ....... -40°C to 85°C
LT1124AI/LT1124I ..... -40°C to 85°C
LT1124AM/LT1124M
LT1125AM/LT1125M ..... -55°C to 125°C

#### PACKAGE/ORDER INFORMATION



# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_S = \pm 15V$ , unless otherwise noted.

				LT1124AC/AI/AM LT1125AC/AM			LT1124/C/I/M LT1125/C/M		
SYMBOL	PARAMETER	CONDITIONS (Note 2)	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	LT1124 LT1125		20 25	70 90		25 30	100 140	μV μV
$\frac{\Delta V_{OS}}{\Delta Time}$	Long Term Input Offset Voltage Stability			0.3			0.3		μV/Mo
I <sub>OS</sub>	Input Offset Current	LT1124 LT1125		5 6	15 20		6 7	20 30	nA nA

# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_S = \pm 15V$ , unless otherwise noted.

				124AC/AI			Γ1124C/I/ Τ1125C/I		
SYMBOL	PARAMETER	CONDITIONS (Note 2)	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
I <sub>B</sub>	Input Bias Current			±7	±20		±8	±30	nA
e <sub>n</sub>	Input Noise Voltage	0.1Hz to 10Hz (Notes 8, 9)		70	200		70		nV <sub>P-P</sub>
	Input Noise Voltage Density	f <sub>0</sub> = 10Hz (Note 4) f <sub>0</sub> = 1000Hz (Note 3)		3.0 2.7	5.5 4.2		3.0 2.7	5.5 4.2	nV/√Hz nV/√Hz
in	Input Noise Current Density	f <sub>0</sub> = 10Hz f <sub>0</sub> = 1000Hz		1.3 0.3			1.3 0.3		pA/√Hz pA/√Hz
V <sub>CM</sub>	Input Voltage Range		±12	±12.8		±12	±12.8		V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$	112	126		106	124		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4V \text{ to } \pm 18V$	116	126		110	124		dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$R_L \ge 10k$ , $V_{OUT} = \pm 10V$ $R_L \ge 2k$ , $V_{OUT} = \pm 10V$	5 2	17 4		3.0 1.5	15 3		V/μV V/μV
V <sub>OUT</sub>	Maximum Output Voltage Swing	$R_L \ge 2k$	±13	±13.8		±12.5	±13.8		V
SR	Slew Rate	$R_L \ge 2k \text{ (Notes 3, 7)}$	3	4.5		2.7	4.5		V/µs
GBW	Gain Bandwidth Product	f <sub>0</sub> = 100kHz (Note 3)	9	12.5		8	12.5		MHz
$\overline{Z_0}$	Open-Loop Output Resistance	$V_{OUT} = 0$ , $I_{OUT} = 0$		75			75		Ω
I <sub>S</sub>	Supply Current per Amplifier			2.3	2.75		2.3	2.75	mA
	Channel Separation	$f \le 10$ Hz (Note 9) $V_{OUT} = \pm 10$ V, $R_L = 2$ k	134	150		130	150		dB

# The ullet denotes the specifications which apply over the $-55^{\circ}C \leq T_A \leq 125^{\circ}C$ temperature range, $V_S = \pm 15V$ , unless otherwise noted.

				_	T1124AN T1125AN			LT1124M LT1125M		
SYMBOL	PARAMETER	CONDITIONS (Note 2)		MIN	TYP	MAX	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	LT1124 LT1125	•		50 55	170 190		60 70	250 290	μV μV
$\frac{\Delta V_{OS}}{\Delta Temp}$	Average Input Offset Voltage Drift	(Note 5)	•		0.3	1.0		0.4	1.5	μV/°C
I <sub>OS</sub>	Input Offset Current	LT1124 LT1125	•		18 18	45 55		20 20	60 70	nA nA
I <sub>B</sub>	Input Bias Current		•		±18	±55		±20	±70	nA
V <sub>CM</sub>	Input Voltage Range		•	±11.3	±12		±11.3	±12		V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 11.3V$	•	106	122		100	120		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4V \text{ to } \pm 18V$	•	110	122		104	120		dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$R_L \ge 10k$ , $V_{OUT} = \pm 10V$ $R_L \ge 2k$ , $V_{OUT} = \pm 10V$	•	3 1	10 3		2.0 0.7	10 2		V/μV V/μV
V <sub>OUT</sub>	Maximum Output Voltage Swing	$R_L \ge 2k$	•	±12.5	±13.6		±12	±13.6		V
SR	Slew Rate	$R_L \ge 2k \text{ (Notes 3, 7)}$	•	2.3	3.8		2	3.8		V/µs
I <sub>S</sub>	Supply Current per Amplifier		•		2.5	3.25		2.5	3.25	mA

# **ELECTRICAL CHARACTERISTICS** The ullet denotes the specifications which apply over the $0^{\circ}C \leq T_A \leq 70^{\circ}C$

temperature range,  $V_S = \pm 15V$ , unless otherwise noted.

				1	LT1124A( LT1125A(			LT1124C LT1125C		
SYMBOL	PARAMETER	CONDITIONS (Note 2)		MIN	TYP	MAX	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	LT1124	•		35	120		45	170	μV
		LT1125	•		40	140		50	210	μV
$\frac{\Delta V_{OS}}{\Delta Temp}$	Average Input Offset Voltage Drift	(Note 5)	•		0.3	1		0.4	1.5	μV/°C
I <sub>OS</sub>	Input Offset Current	LT1124	•		6	25		7	35	nA
		LT1125	•		7	35		8	45	nA
I <sub>B</sub>	Input Bias Current		•		±8	±35		±9	±45	nA
V <sub>CM</sub>	Input Voltage Range		•	±11.5	±12.4		±11.5	±12.4		V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 11.5V$	•	109	125		102	122		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4V \text{ to } \pm 18V$	•	112	125		107	122		dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$R_L \ge 10k$ , $V_{OUT} = \pm 10V$	•	4.0	15		2.5	14		V/µV
		$R_L \ge 2k$ , $V_{OUT} = \pm 10V$	•	1.5	3.5		1.0	2.5		V/µV
V <sub>OUT</sub>	Maximum Output Voltage Swing	$R_L \ge 2k$	•	±12.5	±13.7		±12	±13.7		V
SR	Slew Rate	R <sub>L</sub> ≥ 2k (Notes 3, 7)	•	2.6	4		2.4	4		V/µs
Is	Supply Current per Amplifier		•		2.4	3		2.4	3	mA

The ullet denotes the specifications which apply over the  $-40^{\circ}\text{C} \le T_{A} \le 85^{\circ}\text{C}$  temperature range,  $V_{S} = \pm 15V$ , unless otherwise noted. (Note 10)

					Γ1124AC/ LT1125A(		ı	LT1124C/ LT1125C		
SYMBOL	PARAMETER	CONDITIONS (Note 2)		MIN	TYP	MAX	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	LT1124 LT1125	•		40 45	140 160		50 55	200 240	μV μV
$\frac{\Delta V_{OS}}{\Delta Temp}$	Average Input Offset Voltage Drift	(Note 5)	•		0.3	1		0.4	1.5	μV/°C
I <sub>OS</sub>	Input Offset Current	LT1124 LT1125	•		15 15	40 50		17 17	55 65	nA nA
I <sub>B</sub>	Input Bias Current		•		±15	±50		±17	±65	nA
V <sub>CM</sub>	Input Voltage Range		•	±11.4	±12.2		±11.4	±12.2		V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 11.4V$	•	107	124		101	121		dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4V$ to $\pm 18V$	•	111	124		106	121		dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$\begin{array}{l} R_L \geq 10k, \ V_{OUT} = \pm 10V \\ R_L \geq 2k, \ V_{OUT} = \pm 10V \end{array}$	•	3.5 1.2	12 3.2		2.2 0.8	12 2.3		V/μV V/μV
V <sub>OUT</sub>	Maximum Output Voltage Swing	$R_L \ge 2k$	•	±12.5	±13.6		±12	±13.6		V
SR	Slew Rate	R <sub>L</sub> ≥ 2k (Notes 3, 7)	•	2.4	3.9		2.1	3.9		V/µs
Is	Supply Current per Amplifier		•		2.4	3.25		2.4	3.25	mA

**Note 1:** Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

**Note 2:** Typical parameters are defined as the 60% yield of parameter distributions of individual amplifiers; i.e., out of 100 LT1125s (or 100 LT1124s) typically 240 op amps (or 120) will be better than the indicated specification.

**Note 3:** This parameter is 100% tested for each individual amplifier.

Note 4: This parameter is sample tested only.

**Note 5:** This parameter is not 100% tested.

**Note 6:** The inputs are protected by back-to-back diodes. Current limiting resistors are not used in order to achieve low noise. If differential input voltage exceeds  $\pm 1.4V$ , the input current should be limited to 25mA.

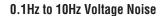
Note 7: Slew rate is measured in  $A_V = -1$ ; input signal is  $\pm 7.5 V$ , output measured at  $\pm 2.5 V$ .

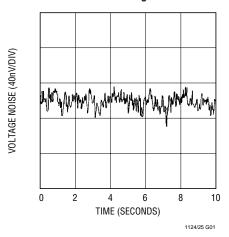
**Note 8:** 0.1Hz to 10Hz noise can be inferred from the 10Hz noise voltage density test. See the test circuit and frequency response curve for 0.1Hz to 10Hz tester in the Applications Information section of the LT1007 or LT1028 data sheets.

**Note 9:** This parameter is guaranteed but not tested.

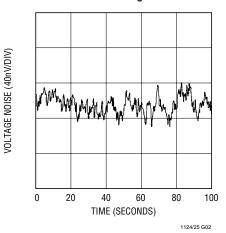
**Note 10:** The LT1124C/LT1125C and LT1124AC/LT1125AC are guaranteed to meet specified performance from 0°C to 70°C and are designed, characterized and expected to meet these extended temperature limits, but are not tested at -40°C and 85°C. The LT1124AI and LT1124I are guaranteed to meet the extended temperature limits.

### TYPICAL PERFORMANCE CHARACTERISTICS

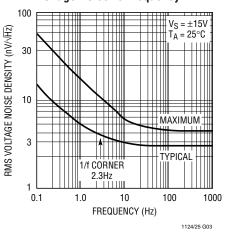




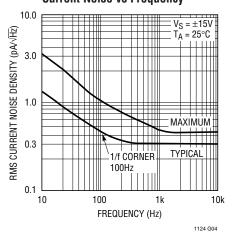
#### 0.01Hz to 1Hz Voltage Noise



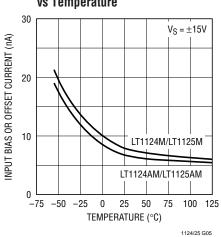
Voltage Noise vs Frequency



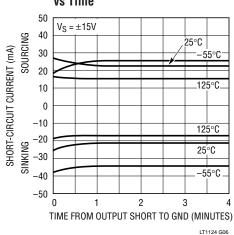
**Current Noise vs Frequency** 



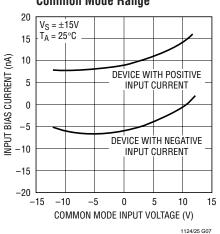
Input Bias or Offset Current vs Temperature



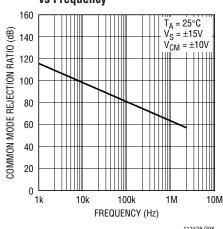
Output Short-Circuit Current vs Time



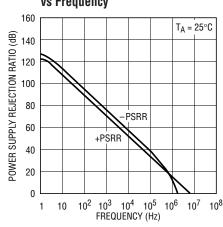
Input Bias Current Over the Common Mode Range



Common Mode Rejection Ratio vs Frequency

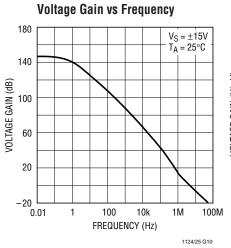


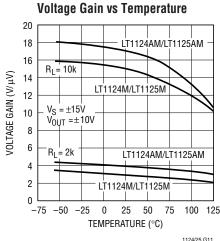
Power Supply Rejection Ratio vs Frequency

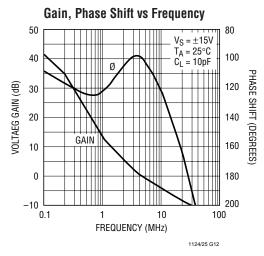


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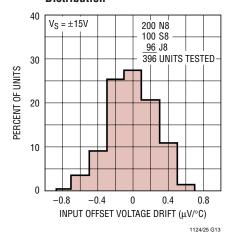
### TYPICAL PERFORMANCE CHARACTERISTICS



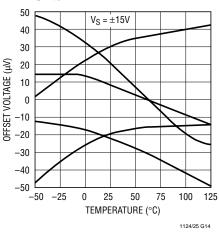




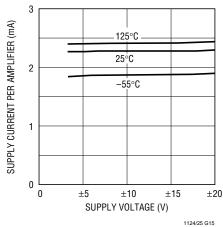
Input Offset Voltage Drift Distribution



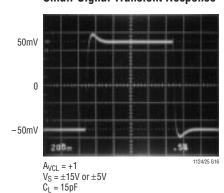
Offset Voltage Drift with Temperature of Representative Units



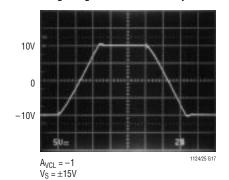
**Supply Current vs Supply Voltage** 



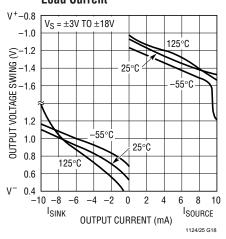
**Small-Signal Transient Response** 



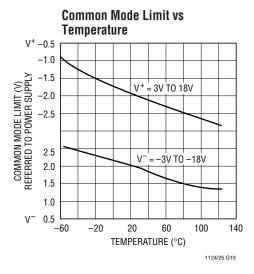
**Large-Signal Transient Response** 

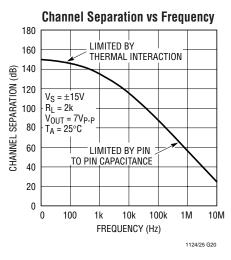


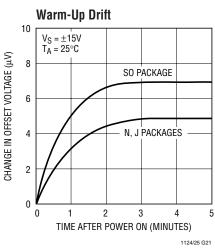
Output Voltage Swing vs Load Current



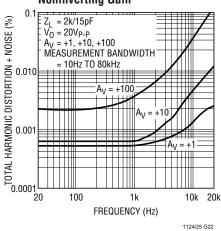
### TYPICAL PERFORMANCE CHARACTERISTICS



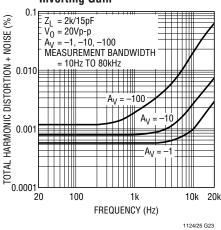




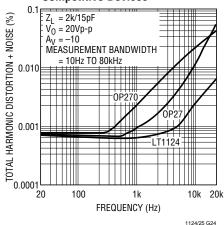
Total Harmonic Distortion and Noise vs Frequency for Noninverting Gain



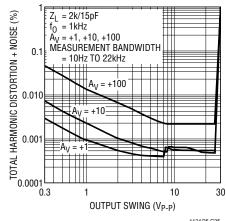
Total Harmonic Distortion and Noise vs Frequency for Inverting Gain



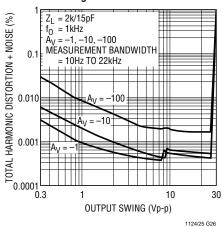
Total Harmonic Distortion and Noise vs Frequency for Competitive Devices



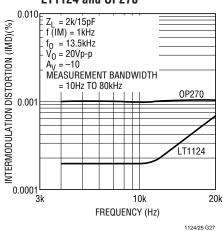
Total Harmonic Distortion and Noise vs Output Amplitude for Noninverting Gain



Total Harmonic Distortion and Noise vs Output Amplitude for Inverting Gain



Intermodulation Distortion (CCIF Method)\* vs Frequency LT1124 and OP270



\*See LT1115 data sheet for definition of CCIF testing

#### APPLICATIONS INFORMATION

The LT1124 may be inserted directly into OP-270 sockets. The LT1125 plugs into OP-470 sockets. Of course, all standard dual and quad bipolar op amps can also be replaced by these devices.

#### **Matching Specifications**

In many applications the performance of a system depends on the matching between two op amps, rather than the individual characteristics of the two devices. The three op amp instrumentation amplifier configuration shown in this data sheet is an example. Matching characteristics are not 100% tested on the LT1124/LT1125.

Some specifications are guaranteed by definition. For example,  $70\mu V$  maximum offset voltage implies that mismatch cannot be more than  $140\mu V$ . 112dB (=  $2.5\mu V/V$ ) CMRR means that worst case CMRR match is 106dB

 $(5\mu V/V)$ . However, Table 1 can be used to estimate the expected matching performance between the two sides of the LT1124, and between amplifiers A and D, and between amplifiers B and C of the LT1125.

#### Offset Voltage and Drift

Thermocouple effects, caused by temperature gradients across dissimilar metals at the contacts to the input terminals, can exceed the inherent drift of the amplifier unless proper care is exercised. Air currents should be minimized, package leads should be short, the two input leads should be close together and maintained at the same temperature.

The circuit shown in Figure 1 to measure offset voltage is also used as the burn-in configuration for the LT1124/LT1125, with the supply voltages increased to  $\pm 16V$ .

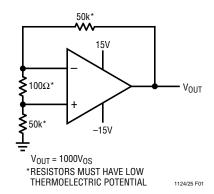


Figure 1. Test Circuit for Offset Voltage and Offset Voltage Drift with Temperature

Table 1. Expected Match

			4AC/AM 5AC/AM		24C/M 25C/M	
PARAMETER		50% YIELD	98% YIELD	50% YIELD	98% YIELD	UNITS
V <sub>OS</sub> Match, ΔV <sub>OS</sub>	LT1124	20	110	30	130	μV
	LT1125	30	150	50	180	μV
Temperature Coeffi	cient Match	0.35	1.0	0.5	1.5	μV/°C
Average Noninvertin	ng I <sub>B</sub>	6	18	7	25	nA
Match of Noninvert	ing I <sub>B</sub>	7	22	8	30	nA
CMRR Match		126	115	123	112	dB
PSRR Match		127	118	127	114	dB

#### APPLICATIONS INFORMATION

#### **High Speed Operation**

When the feedback around the op amp is resistive ( $R_F$ ), a pole will be created with  $R_F$ , the source resistance and capacitance ( $R_S$ ,  $C_S$ ), and the amplifier input capacitance ( $C_{IN} \approx 2pF$ ). In low closed loop gain configurations and with  $R_S$  and  $R_F$  in the kilohm range, this pole can create excess phase shift and even oscillation. A small capacitor ( $C_F$ ) in parallel with  $R_F$  eliminates this problem (see Figure 2). With  $R_S$  ( $C_S + C_{IN}$ ) =  $R_F C_F$ , the effect of the feedback pole is completely removed.

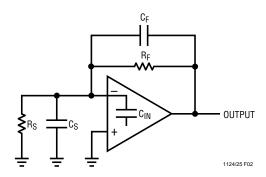


Figure 2. High Speed Operation

#### **Unity Gain Buffer Applications**

When  $R_F \le 100\Omega$  and the input is driven with a fast, large signal pulse (>1V), the output waveform will look as shown in Figure 3.

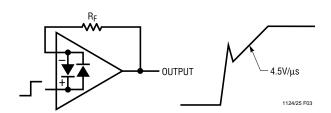


Figure 3. Unity-Gain Buffer Applications

During the fast feedthrough-like portion of the output, the input protection diodes effectively short the output to the input and a current, limited only by the output short circuit protection, will be drawn by the signal generator. With  $R_F \! \geq \! 500\Omega$ , the output is capable of handling the current requirements (I<sub>L</sub>  $\leq 20\text{mA}$  at 10V) and the amplifier stays in its active mode and a smooth transition will occur.

#### **Noise Testing**

Each individual amplifier is tested to  $4.2 \text{nV}/\sqrt{\text{Hz}}$  voltage noise; i.e., for the LT1124 two tests, for the LT1125 four tests are performed. Noise testing for competing multiple op amps, if done at all, may be sample tested or tested using the circuit shown in Figure 4.

$$e_{n \text{ OUT}} = \sqrt{(e_{nA})^2 + (e_{nB})^2 + (e_{nC})^2 + (e_{nD})^2}$$

If the LT1125 were tested this way, the noise limit would be  $\sqrt{4} \cdot (4.2 \text{nV}/\sqrt{\text{Hz}})^2 = 8.4 \text{nV}/\sqrt{\text{Hz}}$ . But is this an effective screen? What if three of the four amplifiers are at a typical  $2.7 \text{nV}/\sqrt{\text{Hz}}$ , and the fourth one was contaminated and has  $6.9 \text{nV}/\sqrt{\text{Hz}}$  noise?

RMS Sum = 
$$\sqrt{(2.7)^2 + (2.7)^2 + (2.7)^2 + (6.9)^2}$$
 = 8.33nV/ $\sqrt{\text{Hz}}$ 

This passes an  $8.4\text{nV}/\sqrt{\text{Hz}}$  spec, yet one of the amplifiers is 64% over the LT1125 spec limit. Clearly, for proper noise measurement, the op amps have to be tested individually.

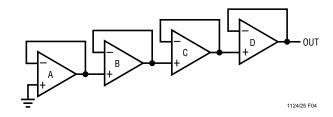


Figure 4. Competing Quad Op Amp Noise Test Method

### PERFORMANCE COMPARISON

Table 2 summarizes the performance of the LT1124/LT1125 compared to the low cost grades of alternate approaches.

The comparison shows how the specs of the LT1124/LT1125 not only stand up to the industry standard OP-27,

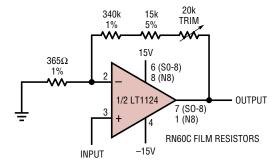
but in most cases are superior. Normally dual and quad performance is degraded when compared to singles, for the LT1124/LT1125 this is not the case.

Table 2. Guaranteed Performance,  $V_S = \pm 15V$ ,  $T_A = 25^{\circ}C$ , Low Cost Devices

PARAMETER/UN	ITS	LT1124CN8 LT1125CN	OP-27 GP	0P-270 GP	OP-470 GP	UNITS
Voltage Noise, 11	кНz	4.2 100% Tested	4.5 Sample Tested	– No Limit	5.0 Sample Tested	nV/√Hz
Slew Rate		2.7 100% Tested	1.7 Not Tested	1.7	1.4	V/µs
Gain Bandwidth I	Product	8.0 100% Tested	5.0 Not Tested	– No Limit	– No Limit	MHz
Offset Voltage	LT1124 LT1125	100 140	100	250 -	_ 1000	μV μV
Offset Current	LT1124 LT1125	20 30	75 -	20 _	- 30	nA nA
Bias Current	•	30	80	60	60	nA
Supply Current/A	ımp	2.75	5.67	3.25	2.75	mA
Voltage Gain, R <sub>L</sub>	= 2k	1.5	0.7	0.35	0.4	V/μV
Common Mode F	Rejection Ratio	106	100	90	100	dB
Power Supply Re	ejection Ratio	110	94	104	105	dB
SO-8 Package		Yes - LT1124	Yes	No	_	

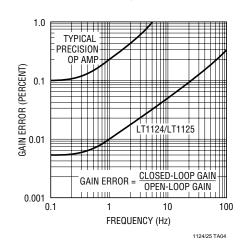
### TYPICAL APPLICATIONS

Gain 1000 Amplifier with 0.01% Accuracy, DC to 1Hz



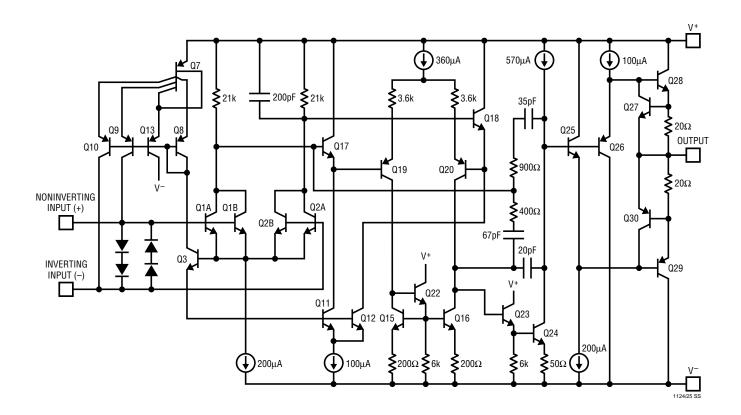
THE HIGH GAIN AND WIDE BANDWIDTH OF THE LT1124/LT1125, IS USEFUL IN LOW FREQUENCY HIGH CLOSED-LOOP GAIN AMPLIFIER APPLICATIONS. A TYPICAL PRECISION OP AMP MAY HAVE AN OPEN-LOOP GAIN OF ONE MILLION WITH 500KHZ BANDWIDTH. AS THE GAIN ERROR PLOT SHOWS, THIS DEVICE IS CAPABLE OF 0.1% AMPLIFYING ACCURACY UP TO 0.3Hz ONLY. EVEN INSTRUMENTATION RANGE SIGNALS CAN VARY AT A FASTER RATE. THE LT1124/LT1125 "GAIN PRECISION — BANDWIDTH PRODUCT" IS 75 TIMES HIGHER, AS SHOWN.

#### Gain Error vs Frequency Closed-Loop Gain = 1000



1124/25 TA03

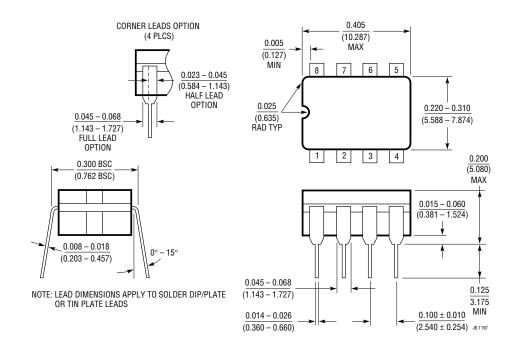
# SCHEMATIC DIAGRAM (1/2 LT1124, 1/4 LT1125)



PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

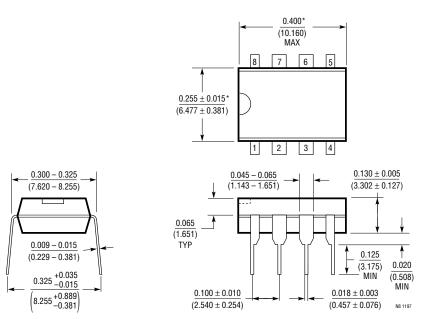
#### J8 Package 8-Lead CERDIP (Narrow 0.300, Hermetic)

(LTC DWG # 05-08-1110)



#### **N8 Package** 8-Lead PDIP (Narrow 0.300)

(LTC DWG # 05-08-1510)

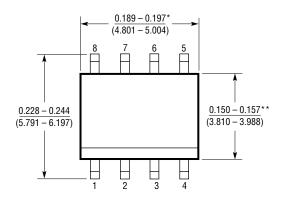


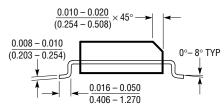
<sup>\*</sup>THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)

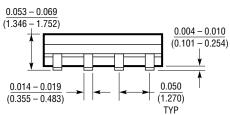
PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

#### S8 Package 8-Lead Plastic Small Outline (Narrow 0.150)

(LTC DWG # 05-08-1610)





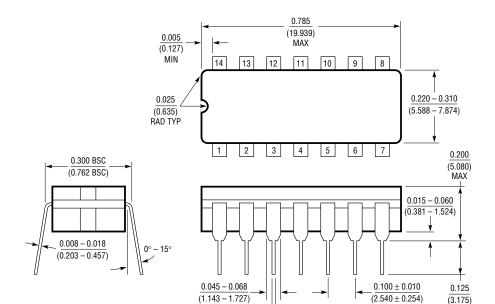


- \*DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE
- \*\*DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

S08 0996

PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

J Package 14-Lead CERDIP (Narrow 0.300, Hermetic) (LTC DWG # 05-08-1110)



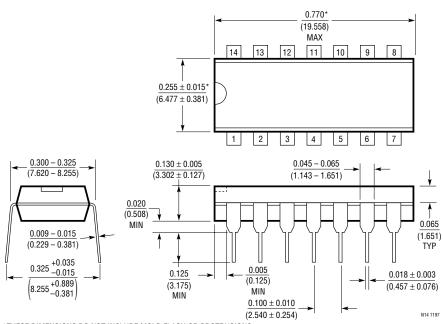
#### N Package 14-Lead PDIP (Narrow 0.300) (LTC DWG # 05-08-1510)

0.014 - 0.026

(0.360 - 0.660)

MIN

J14 1197



<sup>\*</sup>THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)

NOTE: LEAD DIMENSIONS APPLY TO SOLDER DIP/PLATE

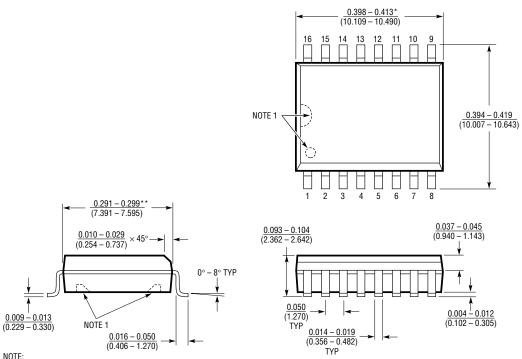
OR TIN PLATE LEADS

S16 (WIDE) 0396

# PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

#### **SW Package** 16-Lead Plastic Small Outline (Wide 0.300)

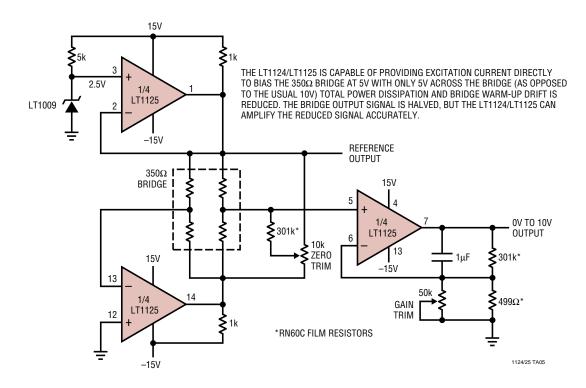
(LTC DWG # 05-08-1620)



- \*DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE
- \*\*DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

# TYPICAL APPLICATION

#### Strain Gauge Signal Conditioner with Bridge Excitation



# **RELATED PARTS**

PART NUMBER	DESCRIPTION	COMMENTS
LT1007	Single Low Noise, Precision Op Amp	2.5nV/√Hz 1kHz Voltage Noise
LT1028/LT1128	Single Low Noise, Precision Op Amps	0.85nV/√Hz Voltage Noise
LT1112/LT1114	Dual/Quad Precision Picoamp Input	250pA Max I <sub>B</sub>
LT1113	Dual Low Noise JFET Op Amp	4.5nV/√Hz Voltage Noise, 10fA/√Hz Current Noise
LT1126/LT1127	Decompensated LT1124/LT1125	11V/μs Slew Rate
LT1169	Dual Low Noise JFET Op Amp	6nV/√Hz Voltage Noise, 1fA/√Hz Current Noise, 10pA Max I <sub>B</sub>
LT1792	Single LT1113	4.2nV/√Hz Voltage Noise, 10fA/√Hz Current Noise
LT1793	Single LT1169	6nV/√Hz Voltage Noise, 1fA/√Hz Current Noise, 10pA Max I <sub>B</sub>