

BU808DFH

HIGH VOLTAGE FAST-SWITCHING NPN POWER DARLINGTON TRANSISTOR

- NEW Fully Plastic TO-220 for HIGH VOLTAGE APPLICATIONS
- NPN MONOLITHIC DARLINGTON WITH INTEGRATED FREE-WHEELING DIODE
- HIGH VOLTAGE CAPABILITY (> 1400 V)
- HIGH DC CURRENT GAIN (TYP. 150)
- LOW BASE-DRIVE REQUIREMENTS
- DEDICATED APPLICATION NOTE AN1184
- FULLY INSULATED PACKAGE (U.L.
- COMPLIANT) FOR EASY MOUNTING CREEPAGE PATH > 4 mm

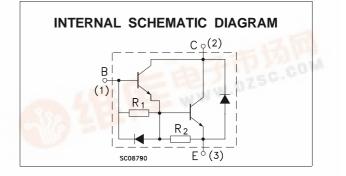
APPLICATIONS

 COST EFFECTIVE SOLUTION FOR HORIZONTAL DEFLECTION IN LOW END TV UP TO 21 INCHES.

DESCRIPTION

The BU808DFH is a NPN transistor in monolithic Darlington configuration. It is manufactured using Multiepitaxial Mesa technology for cost-effective high performance.





ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit V V | |
|------------------|--|------------|----------------|--|
| V _{СВО} | Collector-Base Voltage (I _E = 0) | 1400 | | |
| V _{CEO} | Collector-Emitter Voltage $(I_B = 0)$ | 700 | | |
| V _{EBO} | Emitter-Base Voltage $(I_C = 0)$ | 5 | V | |
| Ι _C | Collector Current | 8 | А | |
| I _{CM} | Collector Peak Current (t _p < 5 ms) | 10 | А | |
| Ι _Β | Base Current | 3 | Α | |
| I _{BM} | Base Peak Current (tp < 5 ms) | 6 | Α | |
| Ptot | Total Dissipation at T _c = 25 °C | 42 | W | |
| Visol | Insulation Withstand Voltage (RMS) from All Three Leads to Exernal Heatsink | 2500 | V | |
| T _{stg} | Storage Temperature | -65 to 150 | °C | |
| Tj | Max. Operating Junction Temperature | 150 | °C | |



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THERMAL DATA

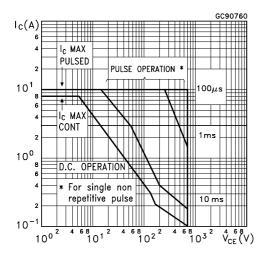
| R _{thj-case} Thermal Resistance Junction-case Max 2.98 °C/V |
|--|
|--|

ELECTRICAL CHARACTERISTICS ($T_{case} = 25 \ ^{\circ}C$ unless otherwise specified)

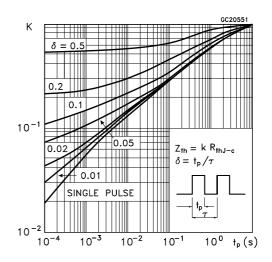
| Symbol | Parameter | Test Conditions | Min. | Тур. | Max. | Unit |
|----------------------------------|--|---|----------|----------|----------|----------|
| ICES | Collector Cut-off Current (V _{BE} = 0) | Vce = 1400 V | | | 400 | μA |
| I _{EBO} | Emitter Cut-off Current $(I_C = 0)$ | V _{EB} = 5 V | | | 100 | mA |
| V _{CE(sat)} * | Collector-Emitter Saturation Voltage | $I_{\rm C} = 5 \text{ A}$ $I_{\rm B} = 0.5 \text{ A}$ | | | 1.6 | V |
| $V_{BE(sat)}*$ | Base-Emitter Saturation Voltage | $I_{\rm C} = 5 \text{ A}$ $I_{\rm B} = 0.5 \text{ A}$ | | | 2.1 | V |
| h _{FE} * | DC Current Gain | | 60 20 | | 230 | |
| t _s t _f | INDUCTIVE LOAD Storage Time Fall Time | | | | 3 0.8 | μs μs |
| ts t _f | INDUCTIVE LOAD Storage Time Fall Time | | | 2 0.8 | | μs μs |
| VF | Diode Forward Voltage | I _F = 5 A | | | 3 | V |

* Pulsed: Pulse duration = 300 $\mu s,$ duty cycle 1.5 %

Safe Operating Area

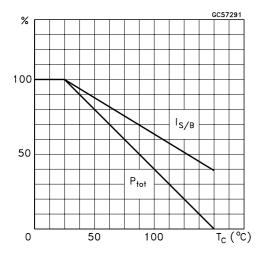


Thermal Impedance

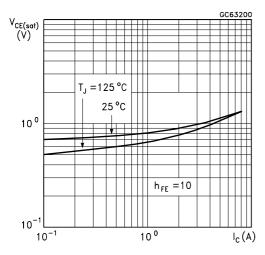


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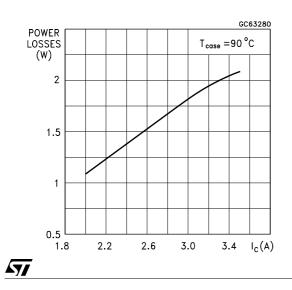
Derating Curve



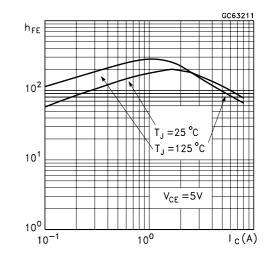
Collector Emitter Saturation Voltage



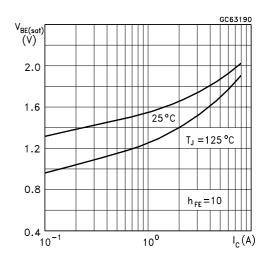
Power Losses at 16 KHz



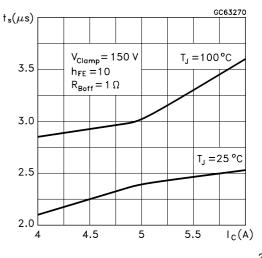
DC Current Gain



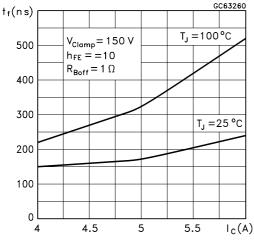
Base Emitter Saturation Voltage



Switching Time Inductive Load at 16KHz



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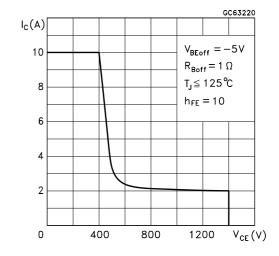
Switching Time Inductive Load at 16KHZ

BASE DRIVE INFORMATION

In order to saturate the power switch and reduce conduction losses, adequate direct base current I_{B1} has to be provided for the lowest gain h_{FE} at 100 °C (line scan phase). On the other hand, negative base current I_{B2} must be provided to turn off the power transistor (retrace phase).

Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of I_{B2} which minimizes power losses, fall time t_f and, consequently, T_j . A new set of curves have been defined to give total power losses, t_s and t_f as a function of I_{B2} at both 16 KHz scanning frequencies for choosing the optimum negative

Reverse Biased SOA



drive. The test circuit is illustrated in figure 1. Inductance L_1 serves to control the slope of the negative base current I_{B2} to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.

The values of L and C are calculated from the following equations:

$$\frac{1}{2}L(I_{C})^{2} = \frac{1}{2}C(V_{CEfly})^{2} \qquad \omega = 2\pi f = \frac{1}{\sqrt{LC}}$$

Where I_{C} = operating collector current, V_{CEfly} = flyback voltage, f= frequency of oscillation during retrace.

L1

Figure 1: Inductive Load Switching Test Circuits.

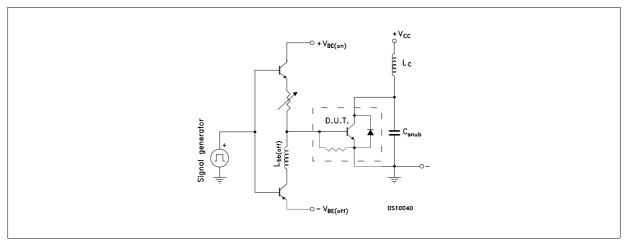
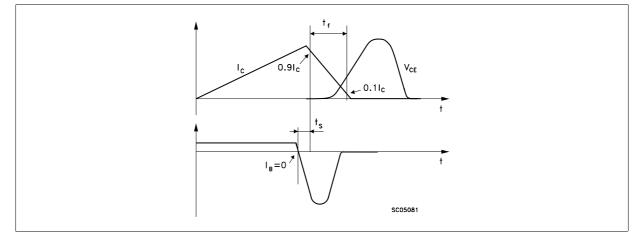
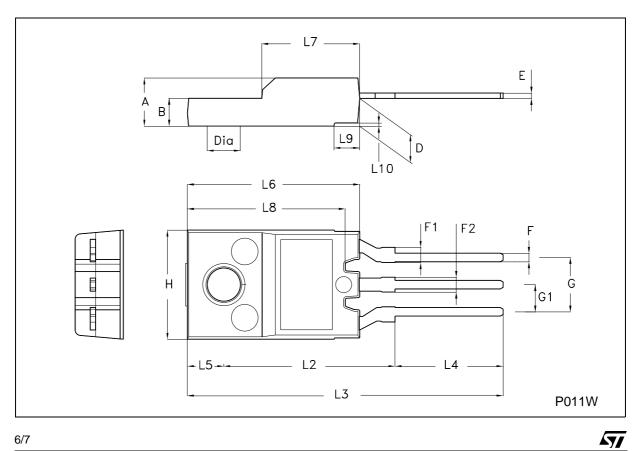


Figure 2: Switching Waveforms in a Deflection Circuit



| DIM. | | mm | | | inch | |
|------|------|------|------|-------|-------|-------|
| | MIN. | TYP. | MAX. | MIN. | TYP. | MAX. |
| А | 4.4 | | 4.6 | 0.173 | | 0.181 |
| В | 2.5 | | 2.7 | 0.098 | | 0.106 |
| D | 2.5 | | 2.75 | 0.098 | | 0.108 |
| Е | 0.45 | | 0.7 | 0.017 | | 0.027 |
| F | 0.75 | | 1 | 0.030 | | 0.039 |
| F1 | 1.3 | | 1.8 | 0.051 | | 0.070 |
| F2 | 1.3 | | 1.8 | 0.051 | | 0.070 |
| G | 4.95 | | 5.2 | 0.195 | | 0.204 |
| G1 | 2.4 | | 2.7 | 0.094 | | 0.106 |
| Н | 10 | | 10.4 | 0.393 | | 0.409 |
| L2 | | 16 | | | 0.630 | |
| L3 | 28.6 | | 30.6 | 1.126 | | 1.204 |
| L4 | 9.8 | | 10.6 | 0.385 | | 0.417 |
| L5 | | 3.4 | | | 0.134 | |
| L6 | 15.9 | | 16.4 | 0.626 | | 0.645 |
| L7 | 9 | | 9.3 | 0.354 | | 0.366 |
| L8 | 14.5 | | 15 | 0.570 | | 0.590 |



TO-220FH (Fully plastic High voltage) MECHANICAL DATA

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