－Distributes One Differential Clock Input to Three LVPECL Differential Clock Outputs
－Programmable Output Divider for Two LVPECL Outputs
－Low－Output Skew 15 ps（Typical）
－ $\mathrm{V}_{\mathrm{CC}}$ Range $3 \mathrm{~V}-3.6 \mathrm{~V}$
－Signaling Rate Up to $800-\mathrm{MHz}$ LVPECL
－Differential Input Stage for Wide Common－Mode Range
－Provides VBB Bias Voltage Output for Single－Ended Input Signals
－Receiver Input Threshold $\pm 75 \mathrm{mV}$
－24－Pin MLF Package（ $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ ）
－Accepts Any Differential Signaling：LVDS， HSTL，CML，VML，SSTL－2，and Single－Ended：LVTTL／LVCMOS

## description


$\dagger$ PowerPad must be connected to $V_{S s}$ ．

The CDCP1803 clock driver distributes one pair of differential clock inputs to three pairs of LVPECL differential clock outputs $\mathrm{Y}[2: 0]$ and $\overline{\mathrm{Y}[2: 0]}$ ，with minimum skew for clock distribution．The CDCP1803 is specifically designed for driving $50-\Omega$ transmission lines．
The CDCP1803 has three control pins，S0，S1，and S2，to select different output mode settings，see Table 1 for details．The CDCP1803 is characterized for operation from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ ．For use in single－ended driver applications，the CDCP1803 also provides a VBB output pin that can be directly connected to the unused input as a common－mode voltage reference．

## CDCP1803

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## functional block diagram



Terminal Functions

| NAME | NO. | 1/0 | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| EN | 1 | $\begin{gathered} \hline \text { I } \\ \text { (with } 60-\mathrm{k} \Omega \text { pullup) } \end{gathered}$ | ENABLE: Enables or disables all outputs simultaneously. $\mathrm{EN}=1$ : outputs on according to $\mathrm{S} 0, \mathrm{~S} 1$, and S 2 setting $\mathrm{EN}=0$ : outputs $\mathrm{Y}[2: 0]$ off (high impedance) See Table 1 for details. |
| IN, $\overline{\mathrm{IN}}$ | 3, 4 | I (differential) | Differential input clock: Input stage is sensitive and has a wide common-mode range. Therefore, almost any type of differential signal can drive this input (LVPECL, LVDS, CML, HSTL). Since the input is high impedance, it is recommended to terminate the PCB transmission line before the input (e.g. with $100-\Omega$ across input). Input can also be driven by single ended signal if the complementary input is tight to VBB. A more advanced scheme for single-ended signal is given in the application section near the end of this document. <br> The inputs deploy an ESD structure protecting the inputs in case of an input voltage exceeding the rails by more than $\sim 0.7 \mathrm{~V}$. Reverse biasing of the IC through these inputs is possible and must be prevented by limiting the input voltage $<\mathrm{V}_{\mathrm{DD}}$. |
| NC | 12 |  | No connect. Leave this pin open or tie to ground |
| S0, S1, S2 | $\begin{gathered} 18,19, \\ 24 \end{gathered}$ | $\begin{gathered} \hline \text { I } \\ \text { (with } 60-\mathrm{k} \Omega \text { pullup) } \end{gathered}$ | Select mode of operation: Defines the output configuration of $\mathrm{Y}[2: 0]$. See Table 1 for configuration. |
| $\frac{\mathrm{Y}[2: 0]}{\mathrm{Y}[2: 0]}$ | $\begin{gathered} 9,10, \\ 15,16, \\ 21,22 \end{gathered}$ | O (LVPECL) | LVPECL clock outputs: These outputs provide low-skew copies of IN pair or down divided copies of clock IN based on selected mode of operation S[2:0]; If an output is unused, the output can simply be left open to save power and minimize noise impact to the remaining outputs. |
| VBB | 6 | 0 | Bias voltage output can be used to bias unused complementary input $\overline{\mathrm{IN}}$ for single ended input signals. <br> The output voltage of VBB is $\mathrm{V}_{\mathrm{DD}}-1.3 \mathrm{~V}$. When driving a load, the output current drive is limited to about 1.5 mA . |
| VSS | 7, 13 | Supply | Device ground |
| V ${ }_{\text {DD }}$ PECL | 2, 5 | Supply | Supply voltage PECL input + internal logic |
| $\mathrm{V}_{\mathrm{DD}}$ [0-2] | $\begin{gathered} 8,11,14, \\ 17,20, \\ 23 \end{gathered}$ | Supply | PECL output supply voltage for output $\mathrm{Y}[0-2]$ : Each output can be disabled by pulling the corresponding $\mathrm{V}_{\mathrm{DD}} \mathrm{x}$ to GND . <br> CAUTION: In this mode, no voltage from outside may be forced, because internal diodes could be forced in forward direction; Thus, it is recommended to disconnect the output if it is not being used. |

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## control pin settings

The CDCP1803 has three control pins (S0, S1, and S2) and an enable pin (EN) to select different output mode settings.


Figure 1. Control Pin Setting for Example
Table 1. Selection Mode Table

|  |  |  |  |  | LVPECL |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MODE | EN | S2 | S1 | S0 | Y0 | Y1 | Y2 |
| 0 | 0 | X | X | X |  | Off (high-z) |  |
| 1 | 1 | 0 | 0 | 0 | $\div 1$ | $\div 1$ | $\div 1$ |
| 2 | 1 | 0 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | Off (high-z) | Off (high-z) |
| 3 | 1 | 0 | 0 | 1 | $\div 1$ | $\div 1$ | Off (high-z) |
| 4 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 2$ | Off (high-z) |
| 5 | 1 | 0 | VDD/2 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | Off (high-z) |
| 6 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 8$ | Off (high-z) |
| 7 | 1 | 0 | 1 | 0 | $\div 1$ | Off (high-z) | $\div 1$ |
| 8 | 1 | 0 | 1 | 1 | $\div 1$ | $\div 2$ | $\div 1$ |
| 9 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | $\div 1$ | $\div 4$ | $\div 1$ |
| 10 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 8$ | $\div 1$ |
| 11 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | $\div 1$ | Off (high-z) | $\div 2$ |
| 12 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 1$ | $\div 2$ |
| 13 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 2$ | $\div 2$ |
| 14 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 4$ | $\div 2$ |
| 15 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | $\div 1$ | $\div 8$ | $\div 2$ |
| 16 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | Off (high-z) | $\div 4$ |
| 17 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | $\div 1$ | $\div 1$ | $\div 4$ |
| 18 | 1 | 1 | 0 | 0 | $\div 1$ | $\div 2$ | $\div 4$ |
| 19 | 1 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | $\div 4$ |
| 20 | 1 | 1 | 0 | 1 | $\div 1$ | $\div 8$ | $\div 4$ |
| 21 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | Off (high-z) | $\div 8$ |
| 22 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | $\div 8$ |


| 23 | 1 | 1 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 2$ | $\div 8$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 24 | 1 | 1 | 1 | 0 | $\div 1$ | $\div 4$ | $\div 8$ |
| 25 | 1 | 1 | 1 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 8$ | $\div 8$ |
| 26 | 1 | 1 | 1 | 1 | $\div 1$ | Off (high-z) | $\div 16$ |
| 27 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 0 | 0 | 0 | $\div 1$ | $\div 1$ | $\div 16$ |
| 28 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 0 | 0 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 2$ | $\div 16$ |
| 29 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 0 | 0 | 1 | $\div 1$ | $\div 4$ | $\div 16$ |
| 30 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 8$ | $\div 16$ |
| Rsv | $\mathrm{V}_{\mathrm{DD} / 2}$ | 1 | $\mathrm{~V}_{\mathrm{DD}} / 2$ | 1 | Reserved | Reserved | Reserved |
| Rsv | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | 0 | $\mathrm{~N} / \mathrm{A}$ | Low | Low |

NOTE: The LVPECL outputs are open emitter stages. Thus, if you leave the unused LVPECL outputs Y0, Y1, or Y2 unconnected, then the current consumption is minimized and noise impact to remaining outputs is neglectable. Also, each output can be individually disabled by connecting the corresponding $\mathrm{V}_{\mathrm{DD}}$ input to GND.

## absolute maximum ratings over operating free-air temperature (unless otherwise noted) $\dagger$

| Supply voltage, $\mathrm{V}_{\text {DD }}$ | -0.3 V to 3.8 V |
| :---: | :---: |
| Input voltage, $\mathrm{V}_{\text {I }}$ | -0.2 V to (VDD +0.2 V ) |
| Output voltage, $\mathrm{V}_{\mathrm{O}}$ | -0.2 V to ( $\left.\mathrm{V}_{\mathrm{DD}}+0.2 \mathrm{~V}\right)$ |
| Differential short circuit current, Yn, Yn, IOSD | Continuous |
| Electrostatic discharge (HBM $1.5 \mathrm{k} \Omega, 100 \mathrm{pF}$ ), ESD | >2000 V |
| Moisture level 24-pin MLF package (solder reflow te |  |
| Storage temperature, $\mathrm{T}_{\text {stg }}$ | $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ |
| Maximum junction temperature, $\mathrm{T}_{\mathrm{J}}$ | $125^{\circ} \mathrm{C}$ |

$\dagger$ Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
recommended operating conditions

|  | MIN | TYP | MAX |
| :--- | ---: | ---: | :---: |
| UNIT |  |  |  |
| Supply voltage, $\mathrm{V}_{\mathrm{DD}}$ | 3 | 3.3 | 3.6 |
| Operating free-air temperature, $\mathrm{T}_{\mathrm{A}}$ | -40 |  | 85 |

electrical characteristics over recommended operating free-air temperature range (unless otherwise noted)

LVPECL input IN, $\overline{\mathrm{IN}}$

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {f }}$ Ik | Input frequency |  | 0 |  | 800 | MHz |
| $\mathrm{V}_{\mathrm{CM}}$ | High-level input common mode |  | 1 |  | $\mathrm{V}_{\mathrm{DD}}-0.3$ | V |
| VIN | Input voltage swing between IN and $\overline{\mathrm{N}}$, see Note 1 |  | 500 |  | 1300 | mV |
| $\mathrm{V}_{\text {IN }}$ | Input voltage swing between IN and $\overline{\mathrm{N}}$, see Note 2 |  | 150 |  | 1300 | mV |
| IIN | Input current | $\mathrm{V}_{\mathrm{I}}=\mathrm{V}_{\text {DD }}$ or 0 V |  |  | $\pm 10$ | $\mu \mathrm{A}$ |
| RIN | Input impedance |  | 300 |  |  | $\mathrm{k} \Omega$ |
| $\mathrm{C}_{1}$ | Input capacitance at IN, $\overline{\mathrm{IN}}$ |  |  | 1 |  | pF |

NOTES: 1. Is required to maintain ac specifications
2. Is required to maintain device functionality

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LVPECL output driver Y[2:0], $\overline{\mathrm{Y}[2: 0]}$

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {f }}$ ¢1k | Output frequency, see Figure 3 |  | 0 |  | 800 | MHz |
| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | Termination with $50 \Omega$ to $\mathrm{V}_{\text {DD }}-2 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{DD}}-1.18$ |  | $\mathrm{V}_{\mathrm{DD}}-0.81$ | V |
| $\mathrm{V}_{\mathrm{OL}}$ | Low-level output voltage | Termination with $50 \Omega$ to $\mathrm{V}_{\text {DD }}-2 \mathrm{~V}$ | $\mathrm{V}_{\text {DD }}$-1.98 |  | $\mathrm{V}_{\mathrm{DD}}$-1.55 | V |
| Vo | Output voltage swing between Y and $\overline{\mathrm{Y}}$, see Figure 3 | Termination with $50 \Omega$ to $\mathrm{V}_{\mathrm{DD}}-2 \mathrm{~V}$ | 500 |  |  | mV |
| IOZL | Output 3-state | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=0 \mathrm{~V}$ |  |  | 5 | $\mu \mathrm{A}$ |
| IOZH | Output 3-state | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=\mathrm{V}_{\mathrm{DD}}-0.8 \mathrm{~V}$ |  |  | 10 | $\mu \mathrm{A}$ |
| $\mathrm{tr}_{\mathrm{r}} / \mathrm{t}_{\mathrm{f}}$ | Rise and fall time | $20 \%$ to $80 \%$ of $\mathrm{V}_{\text {OUTPP, }}$ see Figure 7 | 200 |  | 350 | ps |
| $t_{\text {skpecl }}(0)$ | Output skew between any LVPECL output $\mathrm{Y}[2-0]$ and $\overline{\mathrm{Y}[2-0]}$ | See Note A in Figure 6 |  | 15 | 30 | ps |
| tDuty | Output duty cycle distortion, see Note 3 | Crossing point-to-crossing point distortion | -50 |  | 50 | ps |
| $\mathrm{t}_{\text {sk(pp) }}$ | Part-to-part skew | Any Y, See Note B in Figure 6 |  | 50 |  | ps |
| $\mathrm{C}_{\mathrm{O}}$ | Output capacitance | $\mathrm{V}_{\mathrm{O}}=\mathrm{V}_{\text {D }}$ or GND |  | 1 |  | pF |
| LOAD | Expected output load |  |  | 50 |  | $\Omega$ |

NOTES: 3. For a $800-\mathrm{MHz}$ signal, the 50 -ps error would result into a duty cycle distortion of $\pm 4 \%$ when driven by an ideal clock input signal.
LVPECL input-to-LVPECL output parameter

|  | PARAMETER | TEST CONDITIONS | MIN | TYP |
| :---: | :--- | ---: | ---: | :---: |
| $\mathrm{t}_{\text {pd }}(\mathrm{lh})$ | MAX | UNIT |  |  |
| $\mathrm{t}_{\text {pd }}(\mathrm{hl})$ | Propagation delay rising edge | VOX to VOX | 320 | 600 |
| $\mathrm{t}_{\text {sk }}(\mathrm{p})$ | LVPECL pulse skew | VOX to VOX | 320 | 600 |

electrical characteristics over recommended operating free-air temperature range (unless otherwise noted) (continued)
jitter characteristics

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| tjitterLVPECL | Additive phase jitter from input to LVPECL output [Y2-0], see Figure 2 | 12 kHz to 20 MHz , $\mathrm{f}_{\text {out }}=250 \mathrm{MHz}$ to 800 MHz , divide by 1 mode |  |  | 0.15 | ps rms |
|  |  | $\begin{array}{\|l\|} \hline 50 \mathrm{kHz} \text { to } 40 \mathrm{MHz}, \\ \text { fout }=250 \mathrm{MHz} \text { to } 800 \mathrm{MHz}, \\ \text { divide by } 1 \text { mode } \\ \hline \end{array}$ |  |  | 0.25 | ps rms |



Figure 2.


Figure 3.
supply current electrical characteristics over recommended operating free-air temperature range (unless otherwise noted)

| PARAMETER |  |  | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IDD | Supply current | Full load | All outputs enabled and terminated with $50 \Omega$ to $V_{D D}-2 \mathrm{~V}$ on LVPECL outputs, $f=800 \mathrm{MHz}$ for LVPECL outputs $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ |  | 140 |  | mA |
|  |  | No load | Outputs enabled, no output load, $\mathrm{f}=800 \mathrm{MHz}$ for LVPECL outputs $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ |  |  | 90 |  |
| IDD | Supply current saving per LVPECL output stage disabled, no load |  | $\mathrm{f}=800 \mathrm{MHz}$ for LVPECL output, $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ |  | 10 |  | mA |
| ${ }^{\text {I D D }}$ | Supply current, tri-state |  | All outputs 3-state by control logic, $f=0 \mathrm{~Hz}$, $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ |  |  | 0.5 | mA |



Figure 4.
package thermal resistance

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\theta$ JA-1 | MLF-24 package thermal resistance, See Note 1 | 4-layer JEDEC test board (JESD51-7), airflow $=0 \mathrm{ft} / \mathrm{min}$ |  | 106.6 |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\theta$ JA-2 | MLF-24 package thermal resistance with thermal vias in PCB, See Note 1 | 4-layer JEDEC test board (JESD51-7) with four thermal vias of 22 -mil diameter each, airflow $=0 \mathrm{ft} / \mathrm{min}$ |  | 55.4 |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

NOTE 1: It is recommended to provide four thermal vias to connect the thermal pad of the package effectively with the PCB and ensure a good heat sink.

## Example:

calculation of the junction-lead temperature with a 4-layer JEDEC test board using four thermal vias:
$\mathrm{T}^{\text {Chassis }}=85^{\circ} \mathrm{C}$ (temperature of the chassis)
$P_{\text {effective }}=I_{\max } \times \mathrm{V}_{\max }=90 \mathrm{~mA} \times 3.6 \mathrm{~V}=324 \mathrm{~mW}$ (max power consumption inside the package)
$\theta \mathrm{T}_{\text {Junction }}=\theta_{\mathrm{JA}-2} \times \mathrm{P}_{\text {effective }}=55.45^{\circ} \mathrm{C} / \mathrm{W} \times 324 \mathrm{~mW}=17.97^{\circ} \mathrm{C}$
$T_{\text {Junction }}=\theta \mathrm{T}_{\text {Junction }}+\mathrm{T}_{\text {Chassis }}=17.97^{\circ} \mathrm{C}+85^{\circ} \mathrm{C}=103^{\circ} \mathrm{C}$ (the maximum junction temperature of $\mathrm{T}_{\text {die-max }}=$ $125^{\circ} \mathrm{C}$ is not violated)
control input characteristics over recommended operating free-air temperature range

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {su }}$ | Setup time, S0, S1, S2, and EN pin before clock IN |  | 25 |  |  | ns |
| th | Hold time, S0, S1, S2, and EN pin after clock IN |  | 0 |  |  | ns |
| ${ }^{\text {t }}$ (disable) | Time between latching the EN low transition and when all outputs are disabled (how much time is required until the outputs turn off) |  |  | 10 |  | ns |
| ${ }^{\text {t}}$ (enable) | Time between latching the EN low-to-high transition and when outputs are enabled based on control settings (how much time passes before the outputs carry valid signals) |  |  | 1 |  | $\mu \mathrm{S}$ |
| Rpullup | Internal pullup resistor on S[2:0] and EN input |  | 42 | 60 | 78 | $\mathrm{k} \Omega$ |
| $\mathrm{V}_{\mathrm{IH}(\mathrm{H})}$ | Three level input high, S0, S1, S2, and EN pin, see Note 1 |  | 0.9 xV VD |  |  | V |
| $\mathrm{V}_{\mathrm{IL}(\mathrm{L})}$ | Three level low, S0, S1, S2, and EN pin |  |  |  | VD | V |
| IIH | Input current, S0, S1, S2, and EN pin | $\mathrm{V}_{1}=\mathrm{V}_{\text {DD }}$ |  |  | -5 | $\mu \mathrm{A}$ |
| 1 IL | Input current, S0, S1, S2, and EN pin | $\mathrm{V}_{\mathrm{I}}=\mathrm{GND}$ | 38 |  | 85 | $\mu \mathrm{A}$ |

NOTES: 1. Leaving this pin floating automatically pulse the logic level high to $\mathrm{V}_{\mathrm{DD}}$ through an internal pullup resistor of $60 \mathrm{k} \Omega$.
bias voltage VBB over recommended operating free-air temperature range

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :--- | :---: | :---: | ---: | ---: | :---: |
| VBB $\quad$ Output reference voltage | $\mathrm{V}_{\mathrm{DD}}=3 \mathrm{~V}-3.6 \mathrm{~V}, \mathrm{I}_{\mathrm{BB}}=-0.2 \mathrm{~mA}$ | $\mathrm{~V}_{\mathrm{DD}}-1.4$ | $\mathrm{~V}_{\mathrm{DD}}-1.2$ | V |  |



Figure 5.

## PARAMETER MEASUREMENT INFORMATION



NOTES: A. Output skew, $\mathrm{t}_{\mathrm{sk}(\mathrm{o})}$, is calculated as the greater of:

- The difference between the fastest and the slowest $t_{p d(L H) n}(n=0 \ldots 2)$
- The difference between the fastest and the slowest $t_{p d}(\mathrm{HL}) \mathrm{n}(\mathrm{n}=0 \ldots 2)$
B. Part-to-part skew, $\mathrm{t}_{\mathrm{sk}}(\mathrm{pp})$, is calculated as the greater of:
- The difference between the fastest and the slowest $t_{p d}(\mathrm{LH}) \mathrm{n}(\mathrm{n}=0 \ldots 2)$ for LVPECL across multiple devices
- The difference between the fastest and the slowest $t_{p d}(\mathrm{HL}) n(n=0 \ldots 2)$ for LVPECL across multiple devices
C. Pulse skew, $\mathrm{t}_{\mathrm{sk}(\mathrm{p})}$, is calculated as the magnitude of the absolute time difference between the high-to-low ( $\mathrm{tpd}_{\mathrm{pl}}(\mathrm{HL})$ and the low-to-high
$\left(t_{p d}(\mathrm{LH})\right)$ propagation delays when a single switching input causes one or more outputs to switch, $\mathrm{t}_{\mathrm{sk}}(\mathrm{p})=\left|\mathrm{t}_{\mathrm{pd}}(\mathrm{HL})-\mathrm{t}_{\mathrm{pd}}(\mathrm{LH})\right|$. Pulse skew is sometimes referred to as pulse width distortion or duty cycle skew.

Figure 6. Waveforms for Calculation of $\mathrm{t}_{\mathbf{s k}(\mathrm{o})}$ and $\mathrm{t}_{\mathrm{sk}(\mathrm{pp})}$

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## PARAMETER MEASUREMENT INFORMATION



Figure 7. LVPECL Differential Output Voltage and Rise/Fall Time

## PCB design for thermal functionality

It is recommended to take special care of the PCB design for good thermal flow from the MLF-24 pin package to the PCB.

Due to the three LVPECL outputs, the current consumption of the CDCP1803 is fixed.
JEDEC JESD51-7 specifies thermal conductivity for standard PCB boards.
Modeling the CDCP1803 with a standard 4-layer JEDEC board results into a $59.5^{\circ} \mathrm{C}$ max temperature with a $\theta \mathrm{JA}$ of $106.62^{\circ} \mathrm{C} / \mathrm{W}$ for $25^{\circ} \mathrm{C}$ ambient temperature.
When deploying four thermal vias (one per quadrant), the thermal flow improves significantly, yielding $42.9^{\circ} \mathrm{C}$ max temperature with a $\theta_{\mathrm{JA}}$ of $55.4^{\circ} \mathrm{C} / \mathrm{W}$ for $25^{\circ} \mathrm{C}$ ambient temperature.
To ensure sufficient thermal flow, it is recommended to design with four thermal vias in applications enabling all four outputs at ones.

## PARAMETER MEASUREMENT INFORMATION



Figure 8. Recommended Thermal Via Placement
See the SCBA017 and the SLUA271 application notes for further package related information.

## APPLICATION INFORMATION

## LVPECL receiver input termination

The input of the CDCP1803 has a high impedance and comes with a large common-mode voltage range.
For optimized noise performance, it is recommended to properly terminate the PCB trace (transmission line). If a differential signal drives the CDCP1803, then a $100-\Omega$ termination resistor is recommended to be placed as close as possible across the input pins. An even better approach is to install $2 \times 50 \Omega$, with the center tap connected to a capacitor ( C ) to terminate odd-mode noise and make up for transmission line mismatches. The VBB output can also be connected to the center tap to bias the input signal to ( $\mathrm{V}_{\mathrm{DD}}-1.3 \mathrm{~V}$ ) (see Figure 9 ).


Figure 9. Recommended AC-Coupling LVPECL Receiver Input Termination


Figure 10. Recommended DC-Coupling LVPECL Receiver Input Termination

## APPLICATION INFORMATION

The CDCP1803 can also be driven by single-ended signals. Typically, the input signal becomes connected to one input, while the complementary input must be properly biased to the center voltage of the incoming input signal. For LVCMOS signals, this would be $\mathrm{V}_{\mathrm{CC}} / 2$, realized by a simple voltage divider (e.g. two $10-\mathrm{k} \Omega$ resistors). The best options (especially if the dc offset of the input signal might vary) are to ac-couple the input signal and then rebias the signal using the VBB reference output. See Figure 11.


NOTE:
$\mathrm{C}_{\mathrm{AC}}-\mathrm{AC}$-coupling capacitor (e.g., 10 nF )
CCT - Capacitor keeps voltage at $\overline{\mathrm{IN}}$ constant (e.g., 10 nF )
$\mathrm{R}_{\mathrm{dc}}$ - Load and correct duty cycle (e.g., $50 \Omega$ )
$V_{B B}$ - Bias voltage output
Figure 11. Typical Application Setting for Single-Ended Input Signals Driving the CDCP1803

## APPLICATION INFORMATION

## device behavior during RESET and control pin switching

output behavior from enabling the device ( $\mathrm{EN}=0 \Rightarrow 1$ )
In disable mode ( $\mathrm{EN}=0$ ), all output drivers are switched in high-Z mode. The $\mathrm{S}[0: 2]$ control inputs are also switched off. In the same mode, all flip-flops are reset. The typical current consumption is below $500 \mu \mathrm{~A}$.

When the device is enabled again, it takes typically $1 \mu$ s for the settling of the reference voltage and currents. During this time, the outputs $\mathrm{Y}[0: 2]$ and $\mathrm{Y}[0: 2]$ drive a high signal. After the settle time, the outputs go into the low state. Due to the synchronization of each output driver signal with the input clock, the state of the waveforms after enabling the device looks like shown in Figure 12. The inverting input and output signal is not included. The $Y: / 1$ waveform is the undivided output driver state.


Signal State After the Device is Enabled (IN = Low)


Signal State After the Device is Enabled (IN = High)
Figure 12. Waveforms

## APPLICATION INFORMATION

enabling a single output stage
If a single output stage becomes enabled:

- $\mathrm{Y}[0: 2]$ will either be low or high (undefined).
- $\overline{Y[0: 2] ~ w i l l ~ b e ~ t h e ~ i n v e r t e d ~ s i g n a l ~ o f ~} \mathrm{Y}[0: 2]$.

With the first positive clock transition the undivided output becomes the input clock state. The divided output states are equal to the actual internal divider. The internal divider doesn't get reset while enabling single output drivers.


Figure 13. Signal State After an Output Driver Becomes Enabled While IN =0


Figure 14. Signal State After an Output Driver Becomes Enabled While IN =1

RTH (S-PQFP-N24)


NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. QFN (Quad Flatpack No-Lead) Package configuration.

[^0]
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[^0]:    (D) The Package thermal performance may be enhanced by bonding the thermal die pad to an external thermal plane. This pad may be electrically connected to ground.

