



# FAN8902(KA3902) DC FAN Motor Controller

DZSC.CO

### **Features**

- Built-in PWM Current Control Circuit
- Built-in 5V Regulator
- Low Supply Current
- Stalled Motor Current Limitation
- Built-in Over Voltage Protection (OVP)
- Built-in Over Current Protection (OCP)
- Built-in Load Dump Protection
- Built-in Thermal Shutdown (TSD) Circuit
- Built-in Under Voltage Lockout (UVLO) Circuit

### Description

The FAN8902 is a monolithic integrated circuit, designed for the PWM control of a DC fan motor current in an automotive systems. It allows the fan motor speed to be controlled linearly and efficiently.

14-DIP-300





### **Typical Application**

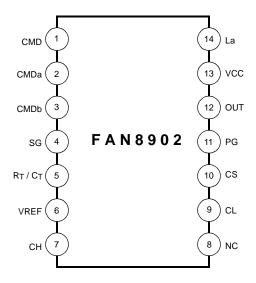
DC for Motor Control for Automotive and Con

### **Ordering Information**

Device Package		Operating Temperature		
FAN8902	14-DIP-300	-40°C ~ +90°C		



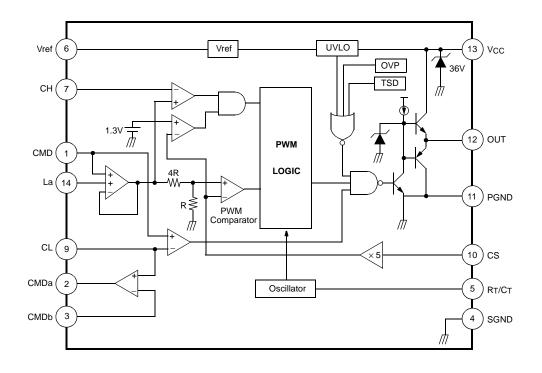
## **Pin Assignments**



### **Pin Definitions**

Pin Number	Pin Name	Pin Function Description		
1	CMD	Motor Current Command Input		
2	CMDa	Optional OP Amplifier Output		
3	CMDb Optional OP Amplifier (-) Input			
4	SGND	Signal GND		
5	5 RT / CT Oscillator Time Constant			
6	6 VREF Voltage Reference (5V)			
7	СН	Maximum Current Reference Input		
8	NC	No Connection		
9	CL	Minimum Current Reference Input		
10	CS	Motor Current Sense Voltage Input		
11	PGND	Power GND		
12	OUT	Drive Output		
13	Vcc	Vcc		
14	La	Motor Current Maximum Reference Input		

## Internal Block Diagram



## Absolute Maximum Ratings

Parameter	Symbol	Value	Unit	
Supply Voltage	Vcc	32	V	
CMD Input Voltage	VCMD	6	V	
Peak Output Current	IOPK	±0.8	A	
Power Dissipation	PD	1	W	

## **Operating Voltage**

Parameter	Symbol	Min.	Тур.	Мах	Unit
Power Supply Voltage	Vcc	9.0	12.0	32.0	V

## **Temperature Characteristics**

Parameter	Symbol	Temp	Value	Unit
Vref Temperature Stability	Vst	-40 ~ +90°C	200	°C
Frequency Stability	FST	-40 ~ +90°C	20 ~ 30	°C
Operating Temperature	TOPR	-	-40 ~ +90	°C
Storage Temperature	TSTG	-	-60 ~ +150	°C

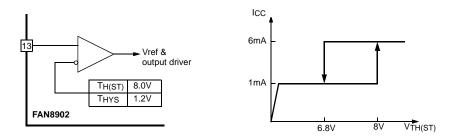
### **Electrical Characteristics**

(Unless otherwise, Ta=25°C, VCC=5V, VM=12V)

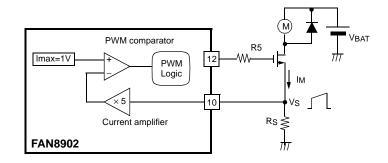
Parameter	Symbol	Conditions	Min.	Тур.	Max.	Unit
REFERENCE						<u>.                                    </u>
Reference Voltage	e Voltage Vref Iref=1mA		4.75	5.0	5.25	V
Line Regulation	∆Vref1	Vcc=9V ~ 32V	-	50	150	mV
Load Regulation	∆Vref2	Iref=1mA ~ 10mA	-	10	50	mV
UNDER VOLTAGE LOCKOUT (UVLC	)			•		
Start Threshold Voltage	VTH(ST)	-	7.5	8.0	8.5	V
Threshold Hysteresis	VHYS	-	1.0	1.2	1.4	V
PROTECTION			•			
Over Voltage	OVP	-	33	36	-	V
OSCILLATOR (RT=75kΩ, CT=1nF)			•			
Frequency	fosc	-	20	25	30	kHz
Duty Cycle	Duty	-	90	95	-	%
CURRENT SENSING INPUT				•		
Threshold Voltage	VTH(ST)	VCMD = 5V	0.19	0.20	0.21	V
OUTPUT DRIVER				•		
Output Voltage Switching Limit	Volim	VCC = 18V, Cld =1nF	-	15	-	V
	VOL1	lout = 20mA	-	-	0.4	V
Low Output Voltage	VOL2	lout = 200mA	-	-	2.2	V
Lisk Ordered Maltane	VOH1	lout = -20mA	10.0	-	-	V
High Output Voltage	VOH2	lout = -200mA	9.0	-	-	V
Rising Time	Tr	Cld = 1nF	-	100	200	ns
Falling Time	Tf	Cld = 1nF	-	100	200	ns
TOTAL STANDBY CURRENT						·
Start-up Current	Start-up Current IST		-	1.0	1.5	mA
Operating Supply Current	ICC	VCC = 9V	-	6.0	8.0	mA

### **Application Information**

#### 1. Under Voltage Lockout (UVLO)



#### 2. Current Sensing Circuit



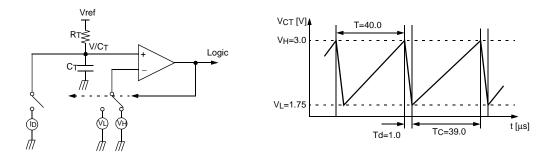
The peak current,  $I_{M(MAX)}=V_S/R_S$ For example, if a required maximum current,  $I_{M(MAX)}=20[A]$ 

$$\mathsf{R}_{\mathsf{S}} = \frac{\mathsf{1}\mathsf{V}/\mathsf{5}}{\mathsf{20}\mathsf{A}} = \mathsf{10}[\mathsf{m}\Omega]$$

#### 3. Thermal Shutdown (Tsd)

When the chip, temperature rises up to 150°C, the thermal shutdown (TSD) circuit is activated and the output driver turn off, and then turn on again at 125°C.

### 4. Oscillator Component Selection



The oscillator timing components can be calculated as follows:

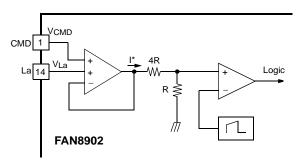
$$\begin{split} \mathbf{T}_{C} &= \mathbf{R}_{T} \times \mathbf{C}_{T} \times \text{In}[(\text{Vref} - \text{V}_{L})/(\text{Vref} - \text{V}_{H})] \\ \mathbf{T}_{D} &= \mathbf{C}_{T} \times [(\text{V}_{H} - \text{V}_{L})/\text{I}_{D}] \\ \text{fosc} &= 1/(\text{T}_{C} + \text{T}_{D}) \\ &= 1.875/(\text{R}_{T} \times \text{C}_{T}) \\ \text{Duty} &= \text{T}_{C} \times \text{fosc} \times 100 \end{split}$$

For example, if fosc = 25kHz and duty = 95%

$$\begin{split} C_{T} &= (T_{D} \times I_{D}) / (V_{H} - V_{L}) \\ &= 1000 [pF] \\ R_{T} &= 1.875 / (fosc \times C_{T}) \\ &= 1.875 / (25 kHz \times 1000 pF) \\ &= 75 [k\Omega] \end{split}$$

### 5. Current Command Input Section

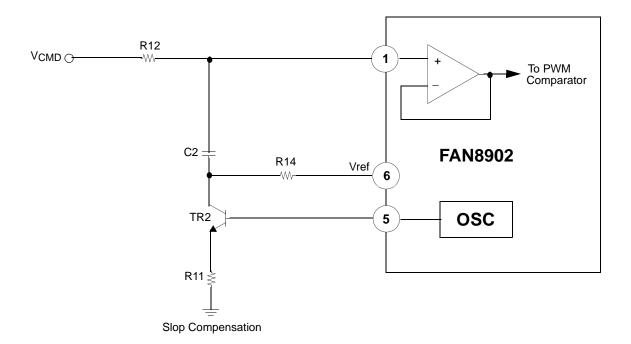
The current command I\* selects the lower value between  $V_{CMD}$  and  $V_{La}$ .



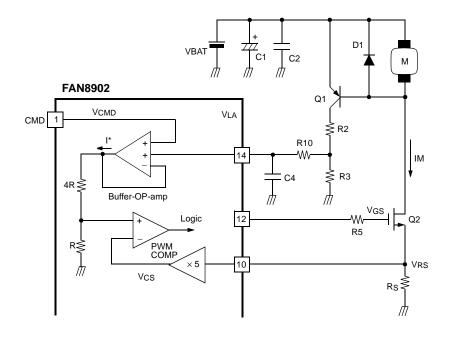
#### 6. Slope Compensation

An unconditional instability of the inner current loop exists for any fixed frequency current-mode converter operating above 50% duty cycle. Therefore, to guarantee current loop stability, the slope of the compensation ramp must be greater than one-half of the down slope of the current waveform. The ramp voltage for slope compensation is as follow,

$$V_{RAMP} = \frac{R14}{R11} \times \Delta V_{OSC}$$



#### 7. Motor Stall Current Limitation



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In the steady state, the terminal voltage on a motor is consisted of a back EMF and the voltage drop on the armarture resistors. When the motor happens to be stalled, the back EMF becomes zero, and the motor current  $(I_M)$  is quickly increased until a maximum values.

Therefore the duty of the pin #12 output becomes lower because of the increase of the sense voltage ( $V_{RS}$ ). Also it makes the voltage ( $V_{La}$ ) be lowered, then it makes the duty become lower again.

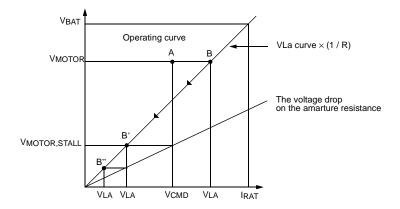
This mechanism makes the motor current hold very low value in the stalled motor state.

The voltage on pin #14 (VLa) ia calculated as follows:

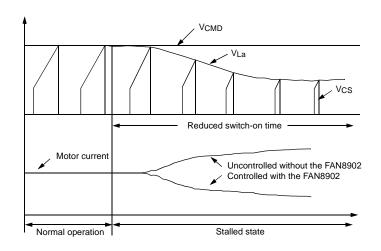
 $V_{La} = V_{BAT} \times D \times \frac{R3}{R2 + R3}$  Assumed the saturation voltage of Q1 is zero.

We can choose the ratio of the resistors, R2 and R3, as follows:

- Applied the rated voltage on motor, and then measured the current IRAT
- Matched the maximum command current, VCMD,MAX to IRAT. VCMD,MAX = VLa,MAX = RS × IRAT × 5 × 5 for example, if RS = 10m $\Omega$  and IRAT = 20[A] at VBAT = 13[V], VCMD,MAX = VLa,MAX = 10m $\Omega$  × 20 × 25 = 5V
- V<sub>La,MAX</sub> = 5V = V<sub>BAT</sub> × 1 × R3 / (R2 + R3) Ratio = R3 / (R2 + R3) = V<sub>CMD,MAX</sub> / V<sub>BAT</sub> = 5 / 13 Therefore, R2 : R3 = 8 : 5



The buffer OP-amp selects the lower command between  $V_{CMD}$  and  $V_{La}$  so as to limit the stalled motor current to very low in the above figure. Because of much larger  $V_{La}$  than  $V_{CMD}$ , the motor operating point stays at A. But the point gradually moves toward B' and then B" through the curve from the instance of stall as the below figure.



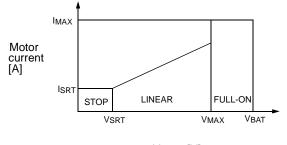
#### 8. Operational Mode Selection

The FAN8902 has three operation modes as follows:

- STOP: Turned-off the power MOSFET
- LINEAR: Linearly controlled the power MOSFET
- FULL-ON: Fully turned-on the power MOSFET

The voltage, VSRT (PIN #9) and VMAX (PIN #7), in the application circuit are as follows:

- VSRT (PIN #9) = Vref  $\times$  R7 / (R5 + R6 + R7)
- $V_{MAX}$  (PIN #7) = Vref × (R6 + R7) / (R5 + R6 + R7)



VCMD [V]

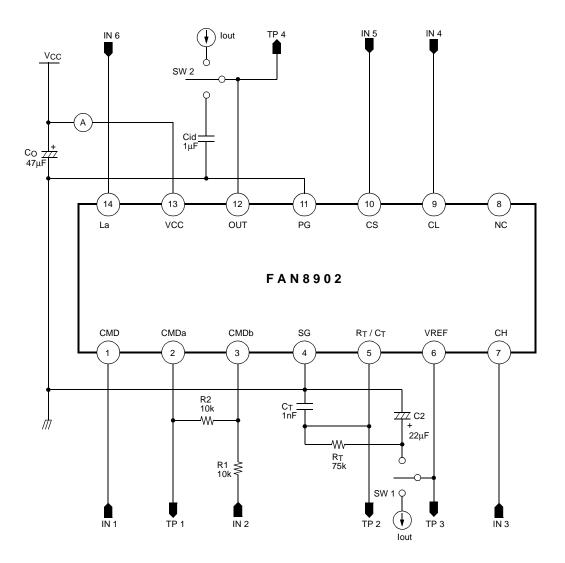
#### 9. Over Voltage Protector (Ovp)

If the voltage,  $V_{BAT} \ge 36[V]$ , the output (pin #12) is grounded, and the switching device (power MOSFET) is turned-off, and the motor is stopped. Then if the voltage,  $V_{BAT} \rightarrow 36[V]$ , the switching device is turned-on again, and the motor is operated.

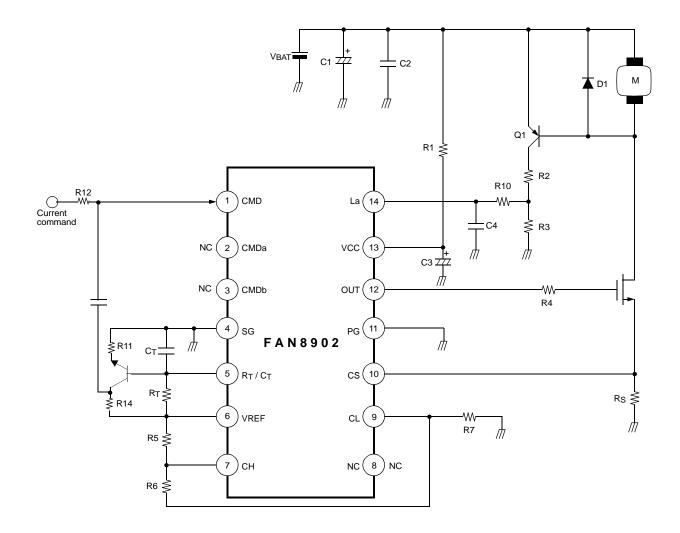
#### 10. Totem-pole Output

The FAN8902 has a single totem-pole output driver which can be drive current to peak  $\pm 0.8$ [A].

### **Test Circuit**



## **Typical Application**



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