



FAN8902(KA3902) DC FAN Motor Controller

DZSC.CO

Features

- Built-in PWM Current Control Circuit
- Built-in 5V Regulator
- Low Supply Current
- Stalled Motor Current Limitation
- Built-in Over Voltage Protection (OVP)
- Built-in Over Current Protection (OCP)
- Built-in Load Dump Protection
- Built-in Thermal Shutdown (TSD) Circuit
- Built-in Under Voltage Lockout (UVLO) Circuit

Description

The FAN8902 is a monolithic integrated circuit, designed for the PWM control of a DC fan motor current in an automotive systems. It allows the fan motor speed to be controlled linearly and efficiently.

14-DIP-300





Typical Application

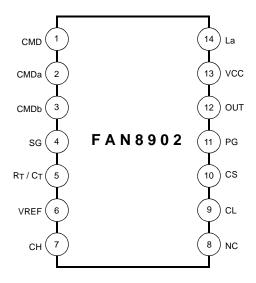
DC for Motor Control for Automotive and Con

Ordering Information

Device Package		Operating Temperature		
FAN8902	14-DIP-300	-40°C ~ +90°C		



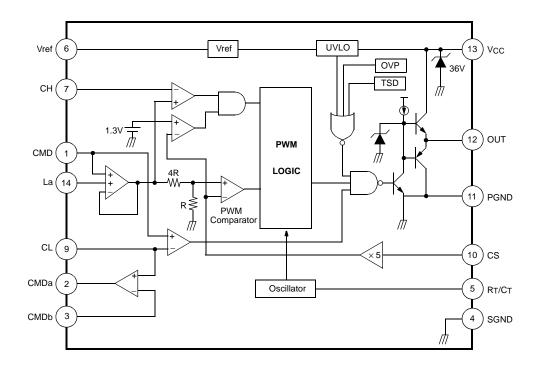
Pin Assignments



Pin Definitions

Pin Number	Pin Name	Pin Function Description		
1	CMD	Motor Current Command Input		
2	CMDa	Optional OP Amplifier Output		
3	CMDb Optional OP Amplifier (-) Input			
4	SGND	Signal GND		
5	5 RT / CT Oscillator Time Constant			
6	6 VREF Voltage Reference (5V)			
7	СН	Maximum Current Reference Input		
8	NC	No Connection		
9	CL	Minimum Current Reference Input		
10	CS	Motor Current Sense Voltage Input		
11	PGND	Power GND		
12	OUT	Drive Output		
13	Vcc	Vcc		
14	La	Motor Current Maximum Reference Input		

Internal Block Diagram



Absolute Maximum Ratings

Parameter	Symbol	Value	Unit	
Supply Voltage	Vcc	32	V	
CMD Input Voltage	VCMD	6	V	
Peak Output Current	IOPK	±0.8	A	
Power Dissipation	PD	1	W	

Operating Voltage

Parameter	Symbol	Min.	Тур.	Мах	Unit
Power Supply Voltage	Vcc	9.0	12.0	32.0	V

Temperature Characteristics

Parameter	Symbol	Temp	Value	Unit
Vref Temperature Stability	Vst	-40 ~ +90°C	200	°C
Frequency Stability	FST	-40 ~ +90°C	20 ~ 30	°C
Operating Temperature	TOPR	-	-40 ~ +90	°C
Storage Temperature	TSTG	-	-60 ~ +150	°C

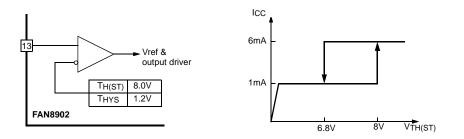
Electrical Characteristics

(Unless otherwise, Ta=25°C, VCC=5V, VM=12V)

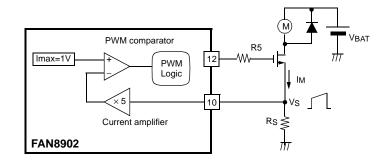
Parameter	Symbol	Conditions	Min.	Тур.	Max.	Unit
REFERENCE						<u>. </u>
Reference Voltage	e Voltage Vref Iref=1mA		4.75	5.0	5.25	V
Line Regulation	∆Vref1	Vcc=9V ~ 32V	-	50	150	mV
Load Regulation	∆Vref2	Iref=1mA ~ 10mA	-	10	50	mV
UNDER VOLTAGE LOCKOUT (UVLC)			•		
Start Threshold Voltage	VTH(ST)	-	7.5	8.0	8.5	V
Threshold Hysteresis	VHYS	-	1.0	1.2	1.4	V
PROTECTION			•			
Over Voltage	OVP	-	33	36	-	V
OSCILLATOR (RT=75kΩ, CT=1nF)			•			
Frequency	fosc	-	20	25	30	kHz
Duty Cycle	Duty	-	90	95	-	%
CURRENT SENSING INPUT				•		
Threshold Voltage	VTH(ST)	VCMD = 5V	0.19	0.20	0.21	V
OUTPUT DRIVER				•		
Output Voltage Switching Limit	Volim	VCC = 18V, Cld =1nF	-	15	-	V
	VOL1	lout = 20mA	-	-	0.4	V
Low Output Voltage	VOL2	lout = 200mA	-	-	2.2	V
Lisk Ordered Maltane	VOH1	lout = -20mA	10.0	-	-	V
High Output Voltage	VOH2	lout = -200mA	9.0	-	-	V
Rising Time	Tr	Cld = 1nF	-	100	200	ns
Falling Time	Tf	Cld = 1nF	-	100	200	ns
TOTAL STANDBY CURRENT						·
Start-up Current	Start-up Current IST		-	1.0	1.5	mA
Operating Supply Current	ICC	VCC = 9V	-	6.0	8.0	mA

Application Information

1. Under Voltage Lockout (UVLO)



2. Current Sensing Circuit



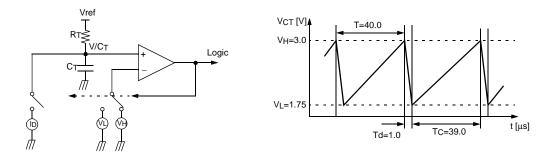
The peak current, $I_{M(MAX)}=V_S/R_S$ For example, if a required maximum current, $I_{M(MAX)}=20[A]$

$$\mathsf{R}_{\mathsf{S}} = \frac{\mathsf{1}\mathsf{V}/\mathsf{5}}{\mathsf{20}\mathsf{A}} = \mathsf{10}[\mathsf{m}\Omega]$$

3. Thermal Shutdown (Tsd)

When the chip, temperature rises up to 150°C, the thermal shutdown (TSD) circuit is activated and the output driver turn off, and then turn on again at 125°C.

4. Oscillator Component Selection



The oscillator timing components can be calculated as follows:

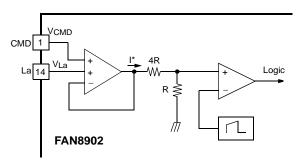
$$\begin{split} \mathbf{T}_{C} &= \mathbf{R}_{T} \times \mathbf{C}_{T} \times \text{In}[(\text{Vref} - \text{V}_{L})/(\text{Vref} - \text{V}_{H})] \\ \mathbf{T}_{D} &= \mathbf{C}_{T} \times [(\text{V}_{H} - \text{V}_{L})/\text{I}_{D}] \\ \text{fosc} &= 1/(\text{T}_{C} + \text{T}_{D}) \\ &= 1.875/(\text{R}_{T} \times \text{C}_{T}) \\ \text{Duty} &= \text{T}_{C} \times \text{fosc} \times 100 \end{split}$$

For example, if fosc = 25kHz and duty = 95%

$$\begin{split} C_{T} &= (T_{D} \times I_{D}) / (V_{H} - V_{L}) \\ &= 1000 [pF] \\ R_{T} &= 1.875 / (fosc \times C_{T}) \\ &= 1.875 / (25 kHz \times 1000 pF) \\ &= 75 [k\Omega] \end{split}$$

5. Current Command Input Section

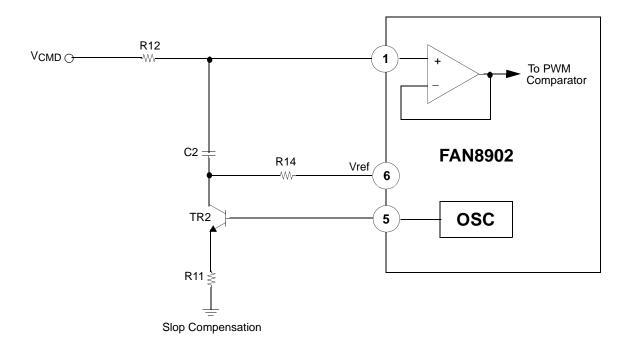
The current command I* selects the lower value between V_{CMD} and V_{La} .



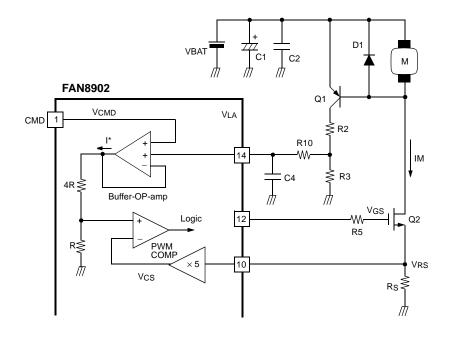
6. Slope Compensation

An unconditional instability of the inner current loop exists for any fixed frequency current-mode converter operating above 50% duty cycle. Therefore, to guarantee current loop stability, the slope of the compensation ramp must be greater than one-half of the down slope of the current waveform. The ramp voltage for slope compensation is as follow,

$$V_{RAMP} = \frac{R14}{R11} \times \Delta V_{OSC}$$



7. Motor Stall Current Limitation



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In the steady state, the terminal voltage on a motor is consisted of a back EMF and the voltage drop on the armarture resistors. When the motor happens to be stalled, the back EMF becomes zero, and the motor current (I_M) is quickly increased until a maximum values.

Therefore the duty of the pin #12 output becomes lower because of the increase of the sense voltage (V_{RS}). Also it makes the voltage (V_{La}) be lowered, then it makes the duty become lower again.

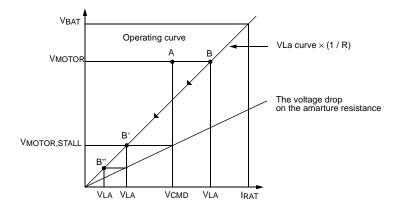
This mechanism makes the motor current hold very low value in the stalled motor state.

The voltage on pin #14 (VLa) ia calculated as follows:

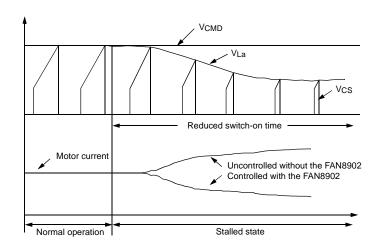
 $V_{La} = V_{BAT} \times D \times \frac{R3}{R2 + R3}$ Assumed the saturation voltage of Q1 is zero.

We can choose the ratio of the resistors, R2 and R3, as follows:

- Applied the rated voltage on motor, and then measured the current IRAT
- Matched the maximum command current, VCMD,MAX to IRAT. VCMD,MAX = VLa,MAX = RS × IRAT × 5 × 5 for example, if RS = 10m Ω and IRAT = 20[A] at VBAT = 13[V], VCMD,MAX = VLa,MAX = 10m Ω × 20 × 25 = 5V
- V_{La,MAX} = 5V = V_{BAT} × 1 × R3 / (R2 + R3) Ratio = R3 / (R2 + R3) = V_{CMD,MAX} / V_{BAT} = 5 / 13 Therefore, R2 : R3 = 8 : 5



The buffer OP-amp selects the lower command between V_{CMD} and V_{La} so as to limit the stalled motor current to very low in the above figure. Because of much larger V_{La} than V_{CMD} , the motor operating point stays at A. But the point gradually moves toward B' and then B" through the curve from the instance of stall as the below figure.



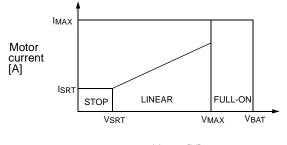
8. Operational Mode Selection

The FAN8902 has three operation modes as follows:

- STOP: Turned-off the power MOSFET
- LINEAR: Linearly controlled the power MOSFET
- FULL-ON: Fully turned-on the power MOSFET

The voltage, VSRT (PIN #9) and VMAX (PIN #7), in the application circuit are as follows:

- VSRT (PIN #9) = Vref \times R7 / (R5 + R6 + R7)
- V_{MAX} (PIN #7) = Vref × (R6 + R7) / (R5 + R6 + R7)



VCMD [V]

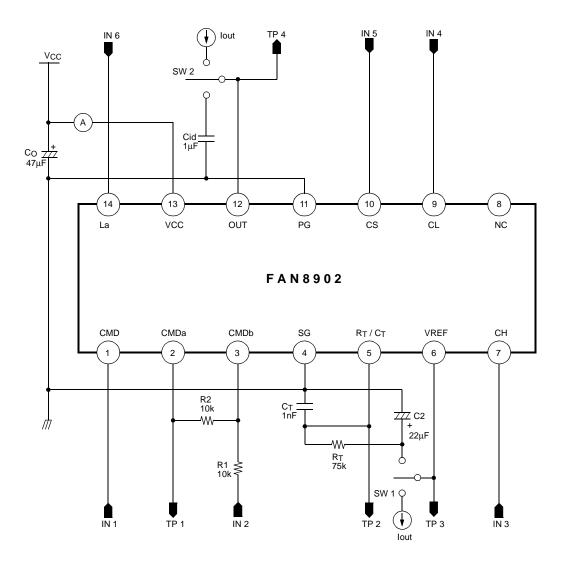
9. Over Voltage Protector (Ovp)

If the voltage, $V_{BAT} \ge 36[V]$, the output (pin #12) is grounded, and the switching device (power MOSFET) is turned-off, and the motor is stopped. Then if the voltage, $V_{BAT} \rightarrow 36[V]$, the switching device is turned-on again, and the motor is operated.

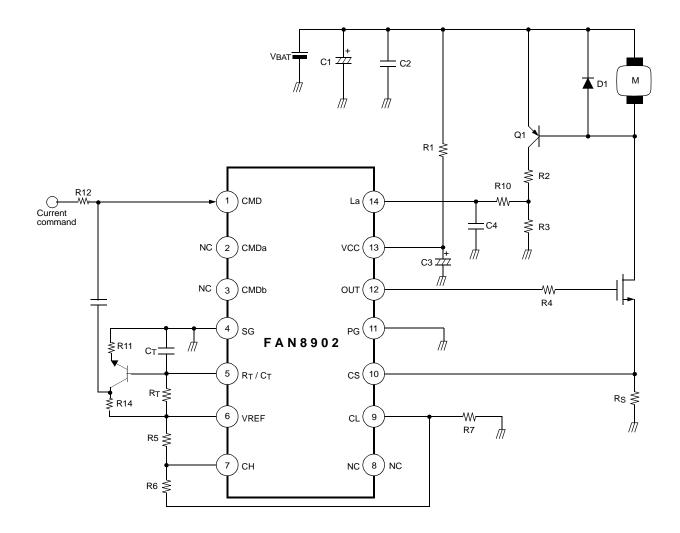
10. Totem-pole Output

The FAN8902 has a single totem-pole output driver which can be drive current to peak ± 0.8 [A].

Test Circuit



Typical Application



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