Monolithic Linear IC

**LA1245** 



# **AM Electronic Tuner**

#### Overview

LA1245 is a high performance IC to be used as an AM electronic tuner. It provides an automatic search-stop signal, local oscillator buffer-output, and the low level local oscillation, as well as providing all other functions required of an AM tuner. Moreover, the stable local oscillation from LW to SW facilitates the use of many band.

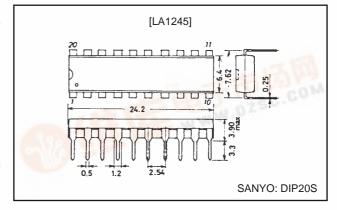
#### **Functions**

- RF amplifier MIX • OSC (with ALC) • Detection
- IF amplifier • AGC • Local oscillation buffer-output
- Signal meter driving output (also used as an automatic search stop-signal)
- · etc.

# Package Dimensions www.ozse.com

unit: mm

#### 3021B-DIP20S



#### **Features**

 Narrow-band signal meter : Available as an automatic search-stop signal (also available as a wide-band signal

meter). Signal meter output=1/2 frequency  $\pm 1.5$ kHz typ.

: Facilitates the design of electronic tuning systems and frequency representation. · Local oscillation buffer-output

• OSC (with ALC) : The oscillation output is stabilized at a low level (350 mVrms) for a varactor

diode, and tracking error is minimized.

• RF amplifier : Excellent in usable sensitivity by incorporating low-noise transistors in cascode

circuit (45dB/m typ).

• MIX : Double balanced differential MIX prevents the influence of spurious radiation and IF interferences (IF interference = 85dB typ).

: Excellent in S/N for intermediate input (57dB typ). · Low noise

: Allows little gain fluctuation and little distoriton fluctuation (8 to 16 V). Compensation for V<sub>CC</sub> fluctuation

· Low shock noise : Able to decrease the shock noise by selecting AGC time constant when changing V<sub>CC</sub>-on and/or switching the mode.



# **Specifications**

# **Maximum Ratings** at Ta=25°C

Parameter	Symbol	Conditions	Ratings	Unit
Supply voltage	V <sub>CC</sub> max	Pin 8, 14	16	V
Output voltage	Vo	Pin 5, 7	24	V
Input voltage	VI	Pin 3	5.6	V
Supply current	I <sub>CC</sub> max	Pin 5+7+8+14	32	mA
Output high drive current	I <sub>18</sub>	Pin 18	5	mA
	120	Pin 20	2	mA
Allowable power dissipation	Pd max	See Figure 2	700	mA
Operating temperature	Topr		-20 to +70	°C
Storage temperature	Tstg		-40 to +125	°C

# **Recommended Operating Conditions** at Ta=25°C

Parameter	Symbol	Conditions	Ratings	Unit
Recommended supply voltage	$V_{CC}$		12	V

# **Operating Characteristics** at Ta=25°C, V<sub>CC</sub>=12V, f<sub>r</sub>=1MHz, f<sub>m</sub>=400Hz, at specified test circuit (based on application circuit).

Parameter	Symbol	Conditions	Ratings			Unit
T diameter	Symbol		min	typ	max	O'III
Current drain	I <sub>CC</sub> 1	quiescent	16.0	25.0	35.0	mA
	I <sub>CC</sub> 2	107 dBµ input	19.0	29.0	40.0	mA
Detection output	V <sub>o</sub> 1	23 dBµ input, mod. 30%	-27.5	-23.0	-18.5	dBm
	V <sub>o</sub> 2	80 dBµ input, mod. 30%	-15.5	-12.5	-9.5	dBm
Signal to noise ratio	S/N1	23 dBµ input, mod. 30%	16	20		dB
	S/N2	80 dBµ input, mod. 30%	52	57		dB
Total harmonic distortion	THD1	80 dBµ input, mod. 30%		0.4	1.0	%
	THD2	107 dBµ input, mod. 30%		0.3	1.0	%
Signal meter output	V <sub>SM</sub> 1	quiescent		0	0.5	V
	V <sub>SM</sub> 3	107 dBµ input	3.0	4.5	7.0	V
Input at signal meter output=1V	V <sub>IN</sub> 1	V <sub>SM</sub> output=1V	19.0	25.0	31.0	dΒμ
Local oscillation-buffer output	V <sub>osc</sub>		250	350		mVrms

### **Reference Characteristics**

Parameter	Symbol	Conditions	Ratings			Unit
i arameter	Oyinboi	Conditions	min	min typ max		Offic
Signal meter output	V <sub>SM</sub> 2	40 dBμ input		2.5		V
Total harmonic distortion	THD3	112 dBµ input, mod.30%		2		%
Local oscillation fluctuation	$\Delta V_{OSC}$	V <sub>osc</sub> L (522kHz) to V <sub>osc</sub> H		10		mVrms
within a band		(1647kHz)				
Signal meter band width*	V <sub>SM-BW1</sub>	80 dBµ input, 1/2 output frequency		±1.5		kHz
	V <sub>SM-BW2</sub>	80 dBµ input, 1/10 output frequency		-4.5/+7		kHz
Selectivity		±10kHz at 30% mod.		45		dB
IF interference		f <sub>r</sub> =600kHz		85		dB
Image frequency interference		f <sub>r</sub> =1400kHz		40		dB
ratio						

<sup>\*</sup> BFB450C4 N (Murata, Co.,) was used as a narrow band filter. (Note) 0 dBm=775mV, 0 dBu=1  $\mu V.$ 

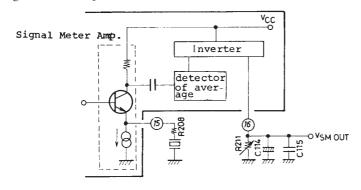
#### Using the automatic search-stop signal

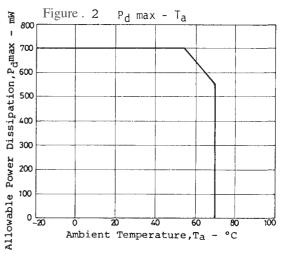
Signal Meter-driving output circuit is equivalent to Figure. 1, signal meter driving output (abbreviated as  $V_{SM}$ ) is narrowed in band width and can be used as an automatic search-stop signal when a narrow band series resonator is connected to pin 15.  $V_{SM}$  can be adjusted with  $R_{208}$  and  $R_{211}$  both in wide band and narrow band since  $R_{208}$  is inversely proportional to  $V_{SM}$ , while  $R_{211}$  is proportional to  $V_{SM}$ .  $R_{208}$  is related to the Q of narrow band signal meter. When the resistance of  $R_{208}$  is increased, the Q will be damped and the band width increased. On the other hand,  $R_{211}$  used as the output impeadance of  $V_{SM}$  and affects the cut-off frequency and time constant of low pass filter for  $V_{SM}$  and the meter drive impedance. The time constant  $\tau$  and the cut-off frequency fc can be expressed as follows:

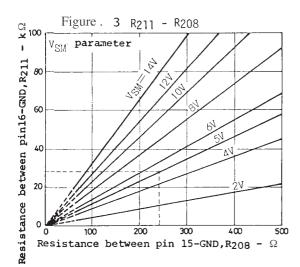
$$\left\{ \begin{array}{l} \tau = (C_{114} + C_{115} + C_S) \ (R_{211} / / R_{in}) \\ f_c = \frac{1}{2\pi\tau} \end{array} \right.$$

A semi-fixed resistor is recommended to be used as  $R_{211}$  to cope with the fluctuation of  $V_{SM}$ . Refer to Figure. 3 for the value of the semi-fixed resistor since this depends upon  $V_{SM}$  and  $R_{208}$ . Figure. 3 shows the lowest limit of the semi-fixed resistor in relation to  $R_{208}$  with the parameter of  $V_{SM}$  set point, and the value of the semi-fixed resistor will be equal to or greater than that shown in Figure. 3. For example, when  $V_{SM}$ =5V and  $R_{208}$ =240 $\Omega$ ,  $R_{211}$  becomes  $28k\Omega$ . Thus, the value of the semi-fixed resistor is determined to be about  $30k\Omega$ . When the value of  $V_{SM}$  is too large, it is limited and saturated to the source voltage so it is recommended to follow the condition of  $V_{SM} \le V_{CC}$ -2(V). When a narrow band serial resonator is used, include the resonant impedance to determine the value of  $R_{208}$ .

Figure . 1 Signal Meter Detector Circuit

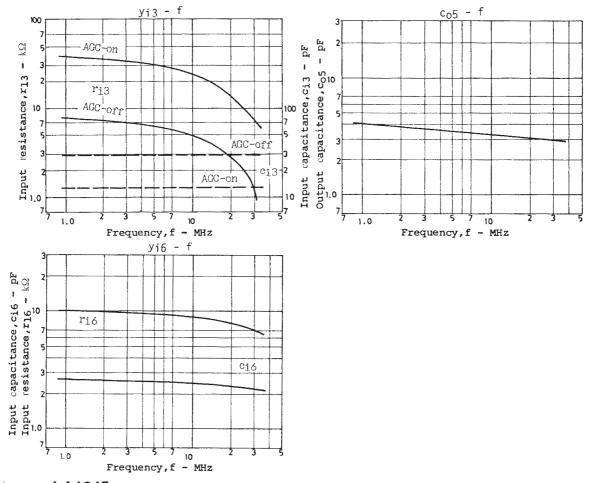






Input/Output Admittance

	Parameter	Frequency	_	AGC-off	AGC -on
DII	УіЗ	1 MHz	r <sub>i</sub> c <sub>i</sub>	8 kΩ 30 pF	40 kΩ 13 pF
RF	У05	1 MHz	r <sub>0</sub> c <sub>0</sub>	— 4 pF	_
MIX	Уіб	MHz	r <sub>i</sub> c <sub>i</sub>	10 kΩ 2.6 pF	_
MITV	У07	500 kHz	r <sub>o</sub> c <sub>o</sub>	— kΩ 2 pF	_
1st IF	yi9	500 kHz	r <sub>i</sub> c <sub>i</sub>	3 kΩ 7 pF	3.2 kΩ 3 pF
	У010	500 kHz	r <sub>0</sub> c <sub>0</sub>	45 Ω 20 pF	42 Ω 20 pF
2nd IF	УіП	500 kHz	r <sub>i</sub> c <sub>i</sub>	80 Ω -150 pF	_



### Notes on LA1245 usage

1. When suddenly tuned to a broadcasting station of intermediate or high field strength, a large current of high frequency flows into the signal meter circuit, causing the local oscillator malfunctions and abnormal noises.

To eliminate this:

- · Use  $R_{208} \ge 240\Omega$  for manual tuning type.
- · Use  $R_{208} \ge 82\Omega$ , and use the local oscillation coil at the 1/3 tap (except SW) for electronic tuning type (which uses a narrow band filter).
- 2. Use the bias on the condition RF  $V_{CC} \le IF V_{CC}$ , since abnormal noise levels might be caused when detuning a strong input on the codition RF  $V_{CC} > IF V_{CC}$ .
- 3. Use the signal meter driving output ( $V_{SM}$ ) at  $V_{SM} \le V_{CC} 2$  (V) to avoid saturation caused by  $V_{CC}$ .
- 4. Use 1/2 or more tap of LW and MW oscillation coil to improve S/N and the detuning characteristics of the distortion ratio.
- 5. Use the full-tap of SW oscillation coil, to allow the sag in oscillation power by the decreasing of Q.
- 6. Avoid the coupling of the antenna tuning circuit and the local oscillating circuit so as not to leak the local oscillation into the antenna tuning circuit.
- 7. Connect the detection capacitor  $C_{113}$  between pin 13 (output) and pin 14 ( $V_{CC}$ ) to avoid the leakage of the IF signal into the GND line. Connection between pin 13 and pin 12 (GND) increases the tweet interference and deteriorates the usable sensitivity.

Moreover, depending on the positions of  $C_{113}$  and the bar antenna, higher harmonics having twice or three times the frequency of the IF signal may pass into the antenna and cause tweet interference, and in extreme cases oscillation might be cause. To prevent this:

- · Shorter lead wires and connect them near 13 and 14 pins.
- $\cdot$  Place  $C_{113}$  far from the antenna.

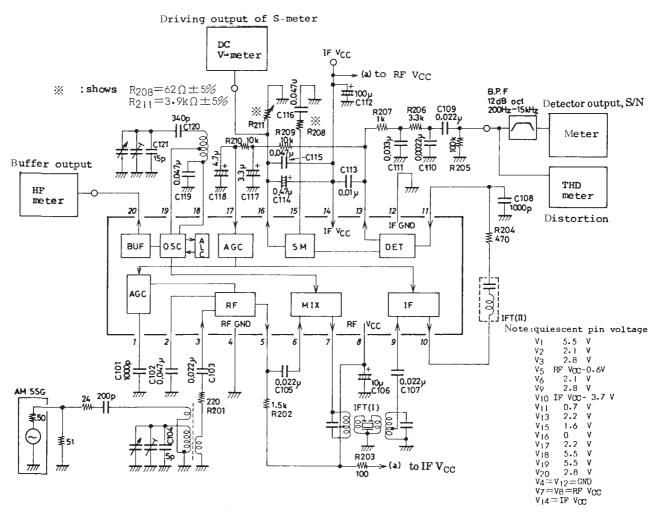
- 8. When a cable or something similar is connected to a local oscillation buffer (pin 20), which is equivalent to connecting a capacitor of about 20pF, the output from the buffer will be of sawtooth waves, causing the level low at the short wave band. To prevent this, connect a resistor between pin 20 and GND, which will increase the operating current of the buffer amplifier. Since the maximum current obtained from pin 20 is 2mA, the suitable resistance between pin 20 and GND is  $1.5k\Omega$ .
- 9. Use a semi-fixed resistor for  $R_{211}$  to allow the fluctuation of  $V_{SM}$ .
- 10. When changing an IFT or using an RF tuner, select a filter and related circuits according to the following conditions. The input levels of each terminal where 30% modulated detection output of –25dBm is obtained are as follows:

Pin 11	l input	when Rg= $520\Omega$ ( $470\Omega + 50\Omega$ )	75dBµ
Pin 9	input input	when $Rg=50\Omega$	$53 dB\mu$
Pin 6	5 input	when $Rg=50\Omega$	$48 dB\mu$
Pin 3	3 input	when Rg= $50\Omega$	$22dB\mu$

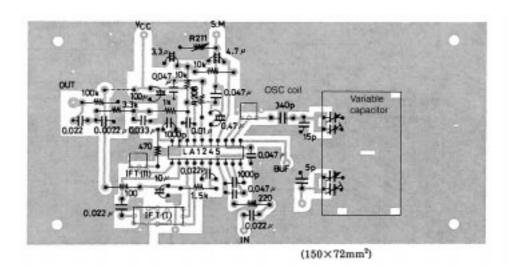
Slight change in IFT, however, will be covered by changing the constant of resistors R<sub>202</sub> and R<sub>204</sub>.

11. When the coupling coefficient of the local oscillation coil is small and an anti-resonance point of about 100MHz is present or the stray capacitance between pin 19 and pin 20 is large, the buffer output (pin 20) may be subject to parasitic oscillation of about 100MHz. In this case, connect a capacitor of about 30pF between pin 20 and GND. To observe parasitic oscillation, connect a capacitor of 5pF in series with the probe. If the probe is connected direct to pin 20, the input capacitance of the probe causes parasitic oscillation to stop, which makes it impossible to observe.

## **Sample Application Circuit 1**

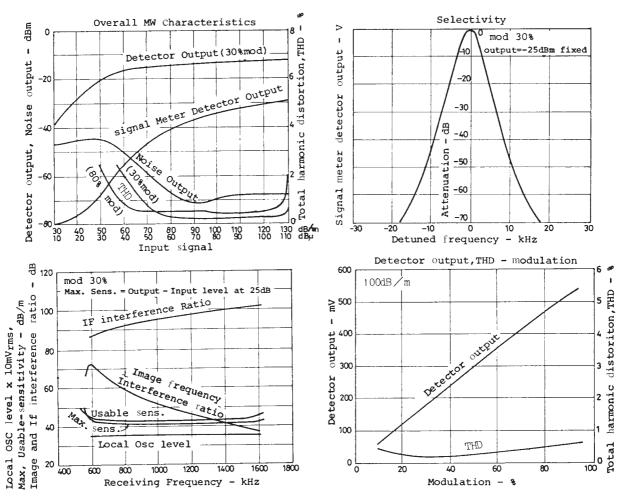


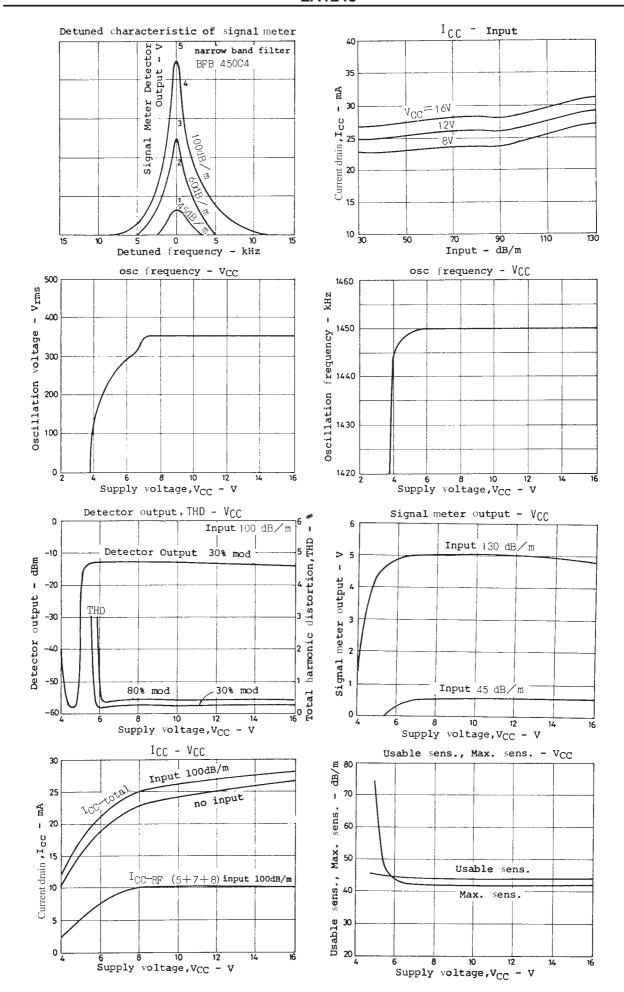
Unit (resistance :  $\Omega$ , capacitance : F)

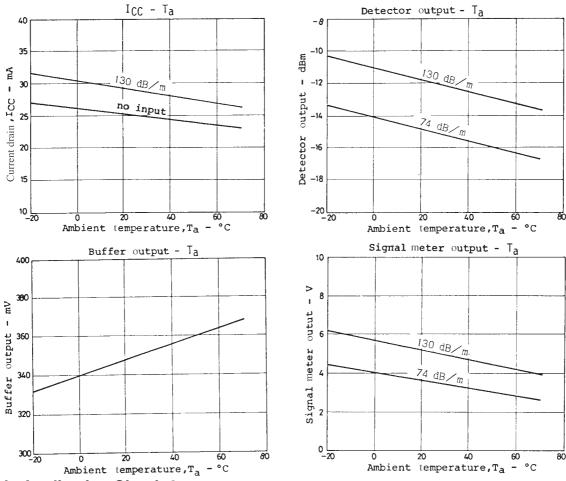


An Example of Printed Pattern (150x72mm<sup>2</sup>, bottom view)

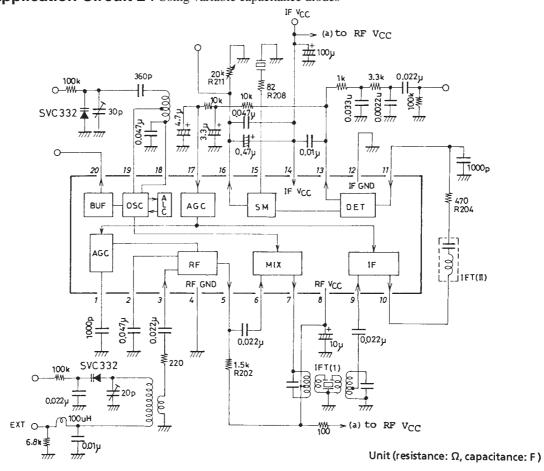
Unit (resistance:  $\Omega$ , capacitance: F)

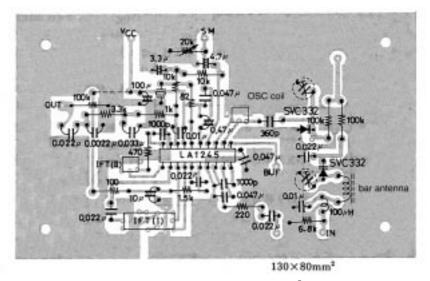






Sample Application Circuit 2: Using variable capacitance diodes





An Example of Printed Pattern (130x80mm², bottom view)

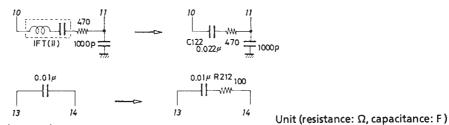
Overall MW characteristics

Unit (resistance: Ω, capacitance: F)

The control of the

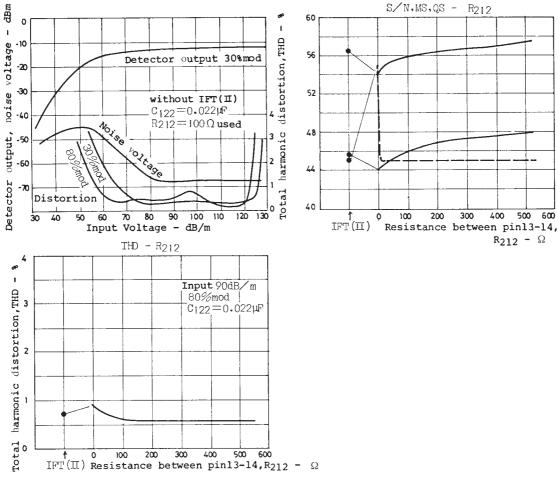
# Sample Application Circuit 3: Rejecting IFT (II)

Following 2 changes are recommended as C-conpling without IFT (II)



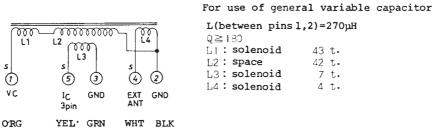
Comparison of characteristics varying parts.

Using IFT(II) dBm dBm 0 distoriton, THD distortion, THD -10 Detector output, noise voltage noise voltage Detector output 30% mod Detector output 30%mod 45.5 dB/m QS 45.0 dB/m Input 90 dB/m S/N 56.5 dB Without IFT(II) C-conpled harmonic harmonic output, 101690 Detector Total Distortion 60 70 80 90 100 110 Input voltage - dB/m 50 40 Input voltage - dB/m

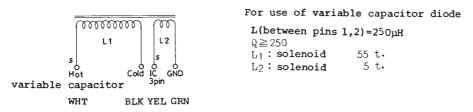


# Peripheral Parts

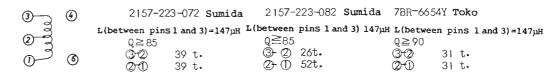
(1) Bar Antenna (34H-052-869 Sumida Co.,)



(2) Bar Antenna (C-4698 Coil Snake Co.,)



(3) Osc coil

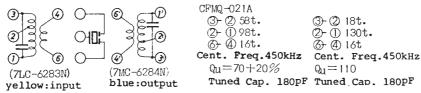


(4) Variable Capacitor (C123A Alps Co.,)

c max 326.8 pF c min 6.7 pF

(5) Variable Capacitor Diode (SVC332 Sanyo)

(6) IFT (I) (CMFQ-021A Toko Co.,)



(7) IFT (II)

(3) (4) (2) (5) (6) (6)

2|50-208-033 Sumida Co., 7LC-4 Cent. Freq. 455kHz Cent  $\mathbb{Q} \ge 95$   $\mathbb{Q} \ge 75$  between 2 and 3 170t. between Tuned Cap. 180pF

7LC-4751B Toko Co., Cent Freq. 455kHz Q≥75 between 2 and 3 146t. Tuned Cap. 180pF

(8) Narrow Band Resonator (BFB450C4 N Murata Co.,)

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