



Monolithic Linear IC

**LA1265****FM/AM Tuner of Electronic Tuning Type****Functions**

FM : IF amplifier, quadrature detector, AF preamplifier, signal meter, tuning indicator drive output (common with stop signal, muting drive output).

AM : RF amplifier, MIX, OSC (with ALC), IF amplifier, detector, AGC, signal meter, tuning indicator drive output (common with stop signal).

**Features**

- Minimum number of external parts required.
- Excellent S/N.
- Local OSC with ALC.
- Local OSC buffer.
- Tuning indicator pin (common with narrow-band stop signal and muting drive output).
- Variable stop sensitivity (variable separately for FM, AM)
- Low whistle.
- Signal meter pin.

**Specifications**

**Maximum Ratings** at Ta=25°C, See specified Test Circuit.

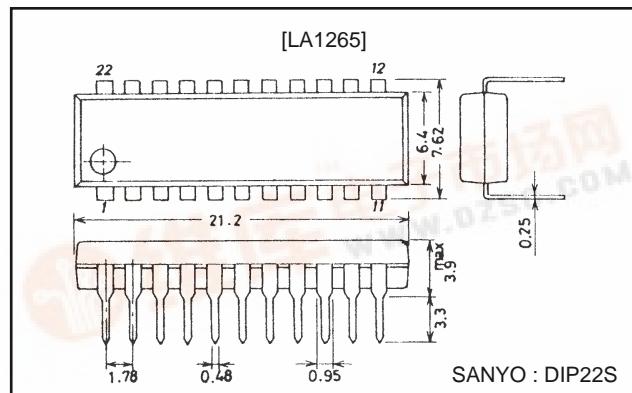
Parameter	Symbol	Conditions	Ratings	Unit
Maximum supply voltage	V <sub>CC</sub> max	Pins 7, 8, 17	16	V
Flow-in current	I <sub>8</sub>	Pin 8	20	mA
Flow-out current	I <sub>20</sub>	Pin 20	1	mA
	I <sub>22</sub>	Pin 22	2	mA
Allowable power dissipation	P <sub>d</sub> max	T <sub>a</sub> ≤60°C	650	mW
Operating temperature	T <sub>opr</sub>		-20 to +70	°C
Storage temperature	T <sub>stg</sub>		-40 to +125	°C

**Operating Conditions** at Ta=25°C

Parameter	Symbol	Conditions	Ratings	Unit
Recommended operating voltage	V <sub>CC</sub>		8.5	V
Operating voltage range	V <sub>CC</sub> op		6 to 14	V

**Package Dimensions**

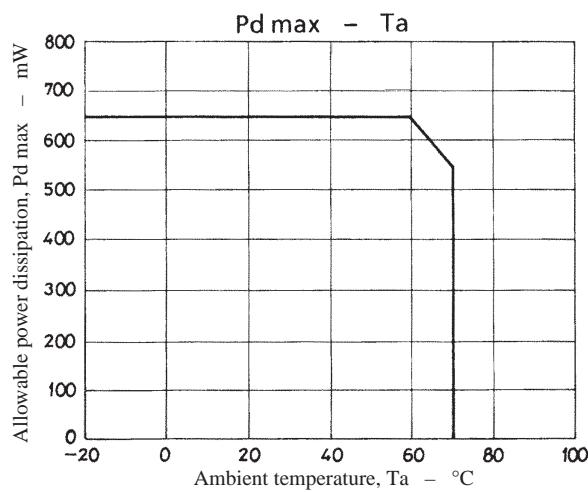
unit : mm

**3059-DIP22S**

## LA1265

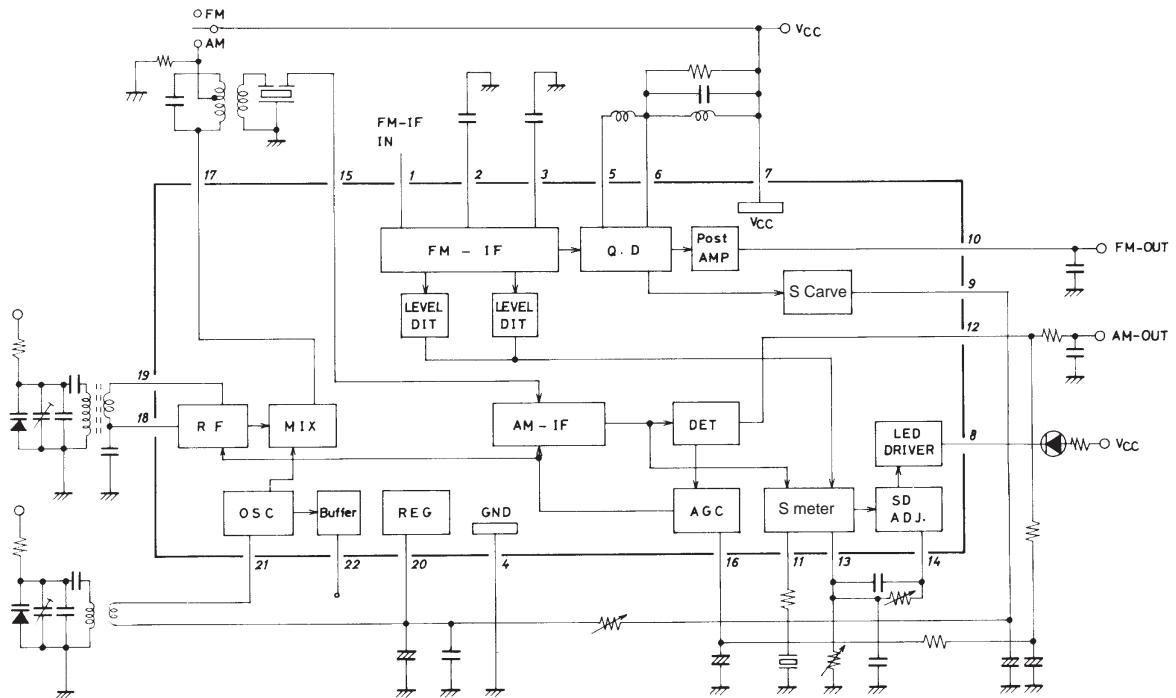
**Operating Characteristics** at  $T_a=25^\circ\text{C}$ ,  $V_{CC}=8.5\text{V}$ , See specified Test Circuit

Parameter	Symbol	Conditions	Ratings			Unit
			min	typ	max	
<b>[AM : f=1MHz]</b>						
Quiescent current	I <sub>cco</sub>	No input		18	26	mA
Detection output	V <sub>O1</sub>	$V_{IN}=20\text{dB}\mu$ , 400Hz, 30% mod.	30	50	90	mV
	V <sub>O2</sub>	$V_{IN}=80\text{dB}\mu$ , 400Hz, 30% mod.	110	160	220	mV
S/N	S/N1	$V_{IN}=20\text{dB}\mu$	16	20		dB
	S/N2	$V_{IN}=80\text{dB}\mu$	49	54		dB
Total harmonic distortion	THD1	$V_{IN}=80\text{dB}\mu$ , 400Hz, 30% mod.		0.3	1.0	%
	THD2	$V_{IN}=107\text{dB}\mu$ , 400Hz, 30% mod.		0.5	2.0	%
Signal meter output	V <sub>SM 1</sub>	No input	0	0	0.2	V
	V <sub>SM 2</sub>	$V_{IN}=80\text{dB}\mu$	2.4	2.8	3.1	V
LED lighting sensitivity	V <sub>LED</sub> on	$I_{LED}=1\text{mA}$	15	24	33	$\text{dB}\mu$
Local OSC buffer output	V <sub>osc</sub>	$f_{OSC}=1.45\text{MHz}$	220	275	330	mV
<b>[FM : f=10.7MHz]</b>						
Quiescent current	I <sub>cco</sub>	No input		20	28	mA
Input limiting sensitivity	-3dBLS.	3dB down, 400Hz, 100% mod.		31	37	$\text{dB}\mu$
Demodulation output	V <sub>O</sub>	$V_{IN}=10\text{dB}\mu$ , 400Hz, 100% mod.	240	330	460	mV
S/N	S/N	$V_{IN}=100\text{dB}\mu$	78	84		dB
Total harmonic distortion	THD	$V_{IN}=100\text{dB}\mu$ , 400Hz, 100% mod.		0.03	0.3	%
Signal meter output	V <sub>SM 1</sub>	No input	0	0	0.2	V
	V <sub>SM 2</sub>	$V_{IN}=100\text{dB}\mu$	1.5	2.7	3.1	V
LED lighting sensitivity	LED-on	$I_{LED}=1\text{mA}$	35	50	65	$\text{dB}\mu$
LED lighting bandwidth	LED-BW	$V_{IN}=100\text{dB}$ , $I_{LED}=1\text{mA}$	90	120	160	kHz
AM rejection ratio	AMR	$V_{IN}=100\text{dB}\mu$ , FM=400Hz 100% mod. AM=1kHz 30% mod.	45	60		dB



# LA1265

## Equivalent Circuit Block Diagram

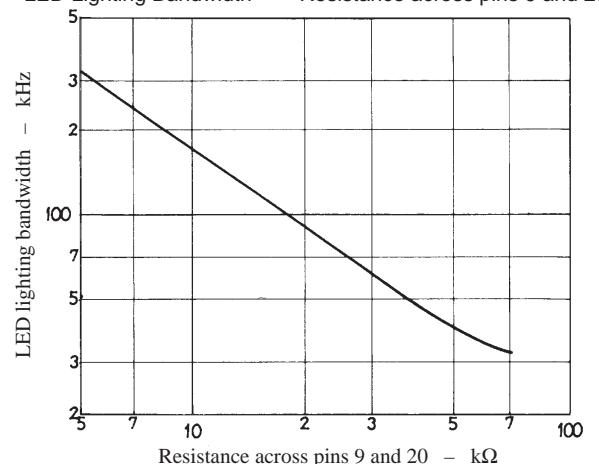


## How to use the LA1265

1. LED lighting, muting drive output, stop signal (SD).
  - For LED lighting, muting drive output, stop signal, the output at pin 8 is used.
  - The voltage on pin 8, when tuned, turns from "H" to "L". (Active-Low)
  - Signal bandwidth at pin 8.
    - For AM, the bandwidth depends on the CF (BFU450CN) at pin 11. If a capacitor is connected in place of the CF, the bandwidth will get wider.
    - For FM, the bandwidth depends on the resistance across pins 9 and 20. If the resistance is increased, the bandwidth will get narrower.  $R=15\text{k}\Omega$  makes the bandwidth approximately 120kHz.
  - Sensitivity adjustment of LED, muting, stop signal.
    - For FM, the semifixed variable resistor across pin 13 and GND is used.
    - For AM, the semifixed variable resistor across pins 13 and 14 is used. Be sure to start adjustment for FM, and then make adjustment for AM. For the stop signal sensitivity and FM stop signal bandwidth, the variations should be considered and it is recommended to use the semifixed variable resistor for adjustment.
  - LED lighting sensitivity setting for AM.
 

For the LED lighting sensitivity setting for AM, it is desirable that the IC input be 30dB $\mu$  (antenna input : approximately 50dB/m). In this case, the value of VR1 is 30k $\Omega$ .

LED Lighting Bandwidth – Resistance across pins 9 and 20



# LA1265

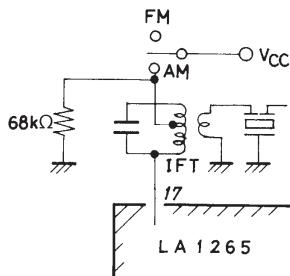
## • LED lighting sensitivity setting for FM.

- For the LED lighting sensitivity setting for FM, the IC input may be  $45\text{dB}\mu$  to  $60\text{dB}\mu$ . With the variations in the front end considered, it is ideal that the IC input in a standard receiving set be  $51\text{dB}\mu$  to  $54\text{dB}\mu$ . The lower value of VR2 for the LED lighting sensitivity setting is as illustrated right. Since the variations in the front end cause the IC input setting sensitivity to vary, it is recommended to use a value of VR2 at an input voltage lower than a standard setting by  $6\text{dB}$  or greater. For example, if IC input  $53\text{dB}\mu$  is taken as a standard, use  $\text{VR2} \leq 100\text{k}\Omega$  at IC input  $47\text{dB}\mu$ .

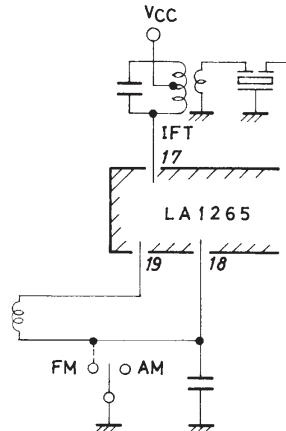
## 2. AM/FM changeover

- Two selections are available for changeover as shown below
  - (A) pin 17-used method and (B) pin 18-used method.
- For (A), the voltage on pin 17 relative to  $V_{CC}$  (pin 7) must be within the range of  $-0.8\text{V}$  to  $+0.1\text{V}$ . If not within this range, distortion and selectivity will get worse.
- For (A), a resistance of  $68\text{k}\Omega$  at the IFT cold terminal, which is used to prevent the changeover circuit from malfunctioning, must be connected.

(A) pin 17-use method for AM/FM changeover



(B) Pin 18-used method for AM/FM changeover



## 3. Local OSC buffer output

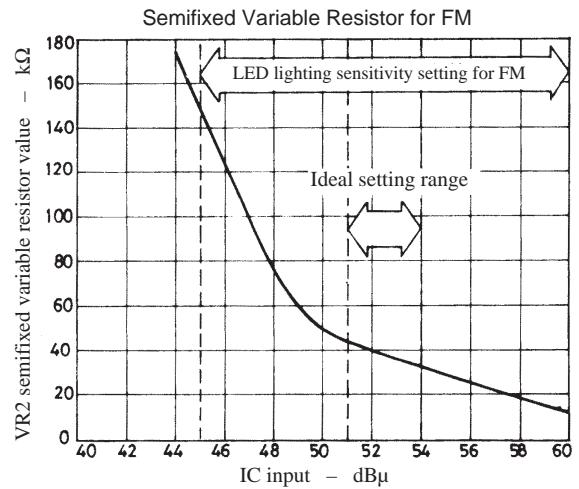
- When local OSC buffer output wave form is saw-toothed at the SW mode, connect a resistance of  $1.2\text{k}\Omega$  or thereabouts across pin 22 and GND.

## 4. AM input pin

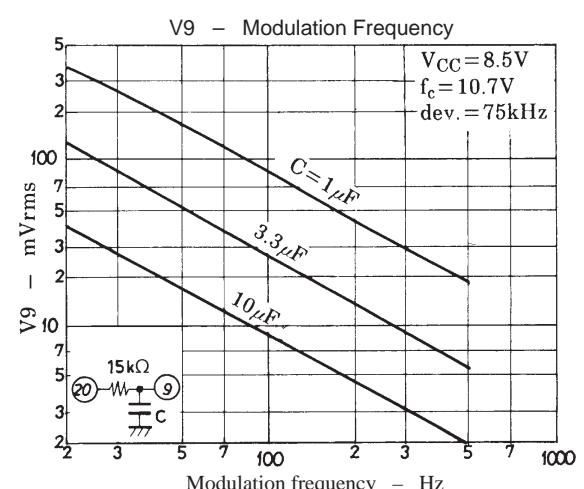
- It is desirable that the AM input pin (pin 19) be L-coupled to pin 18.
- Inputting to pin 19 can be done by DC-cutting with a capacitor. However, an unbalance in the RF amplifier (differential amplifier) causes gain drop and whistle worsening.

## 5. Capacitance across pin 9 and GND.

A large capacitance across pin 9 and GND may cause a misstop at an adjacent channel when the channel select speed is made faster at the automatic channel select mode. In this case, decrease the capacitance across pin 9 and GND. However, if too decreased, the LED will flutter at low modulation frequencies at the time of detuning. Therefore, it is recommended to fix the capacitance across pin 9 and GND to be  $3.3\mu\text{F}$  to  $10\mu\text{F}$ . The relation between modulation frequency and demodulation output voltage on pin 9 with the capacitance across pin 9 and GND as a parameter is shown right.



(B) Pin 18-used method for AM/FM changeover



## LA1265

6. If the coupling coefficient of the local OSC coil is small and an antiresonance point of approximately 100MHz is present or the stray capacitance across pins 22 and 21 is large, a parasitic oscillation of approximately 100MHz may occur in the buffer output (pin 22). In this case, connect a capacitance of approximately 30pF across pin 22 and GND.

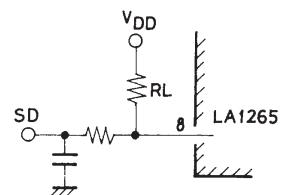
### 7. AM OSC coil

Generally speaking, the following should be noted. Avoid winding with loose coupling between primary side and secondary side (especially SW1, SW2). To put it concretely, the pot core type is better than the screw core type which is loose in coupling. This prevents the local OSC frequency from turning third resonance frequency related to the coupling coefficient.

### 8. Resistance across pin 8 and V<sub>DD</sub>.

If pin 8 is used for the stop signal (SD) only, without using LED, it is recommended to fix resistance R<sub>L</sub> across pin 8 and GND to be 51kΩ to 100kΩ.

### 9. To prevent whistle from worsening, make the pattern of AM output pin 12 as short as possible.



## Input/Output Admittance

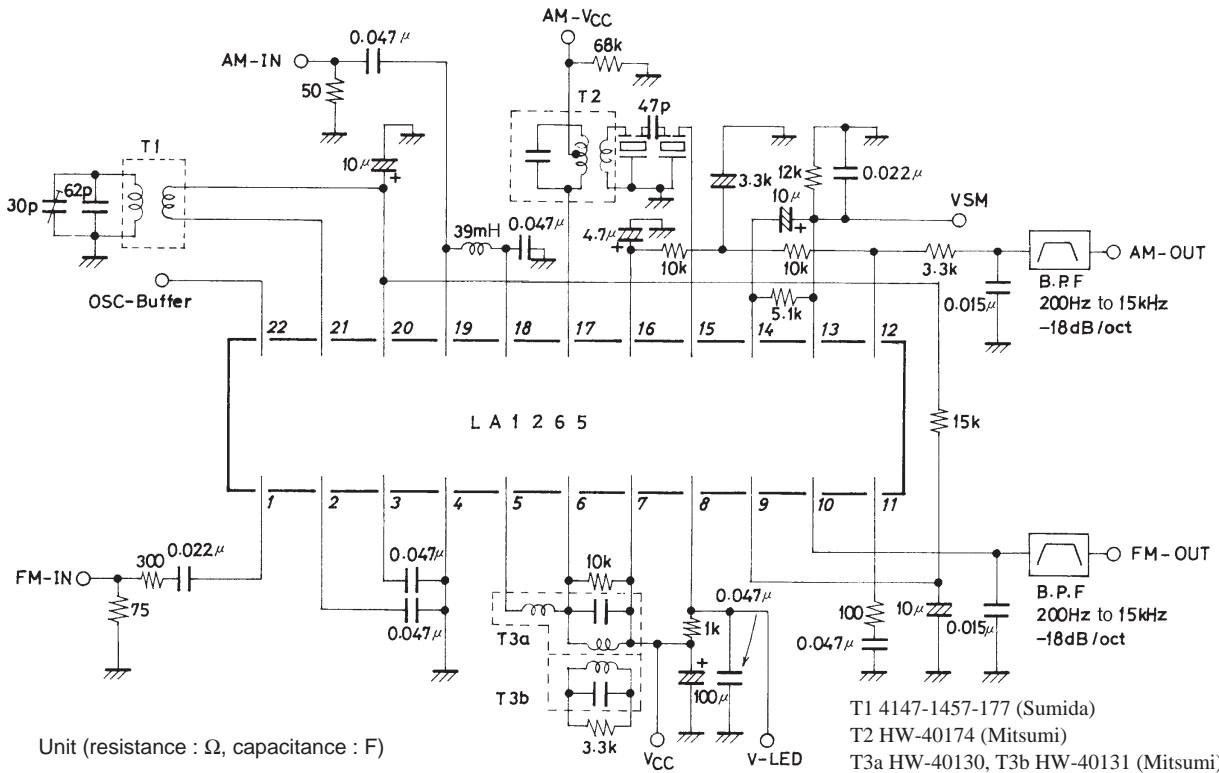
FM

—	Parameter	Frequency	—	Admittance	Unit
IF	γ <sub>i1</sub>	10.7MHz	r <sub>i</sub>	330	Ω
			c <sub>i</sub>	20	pF

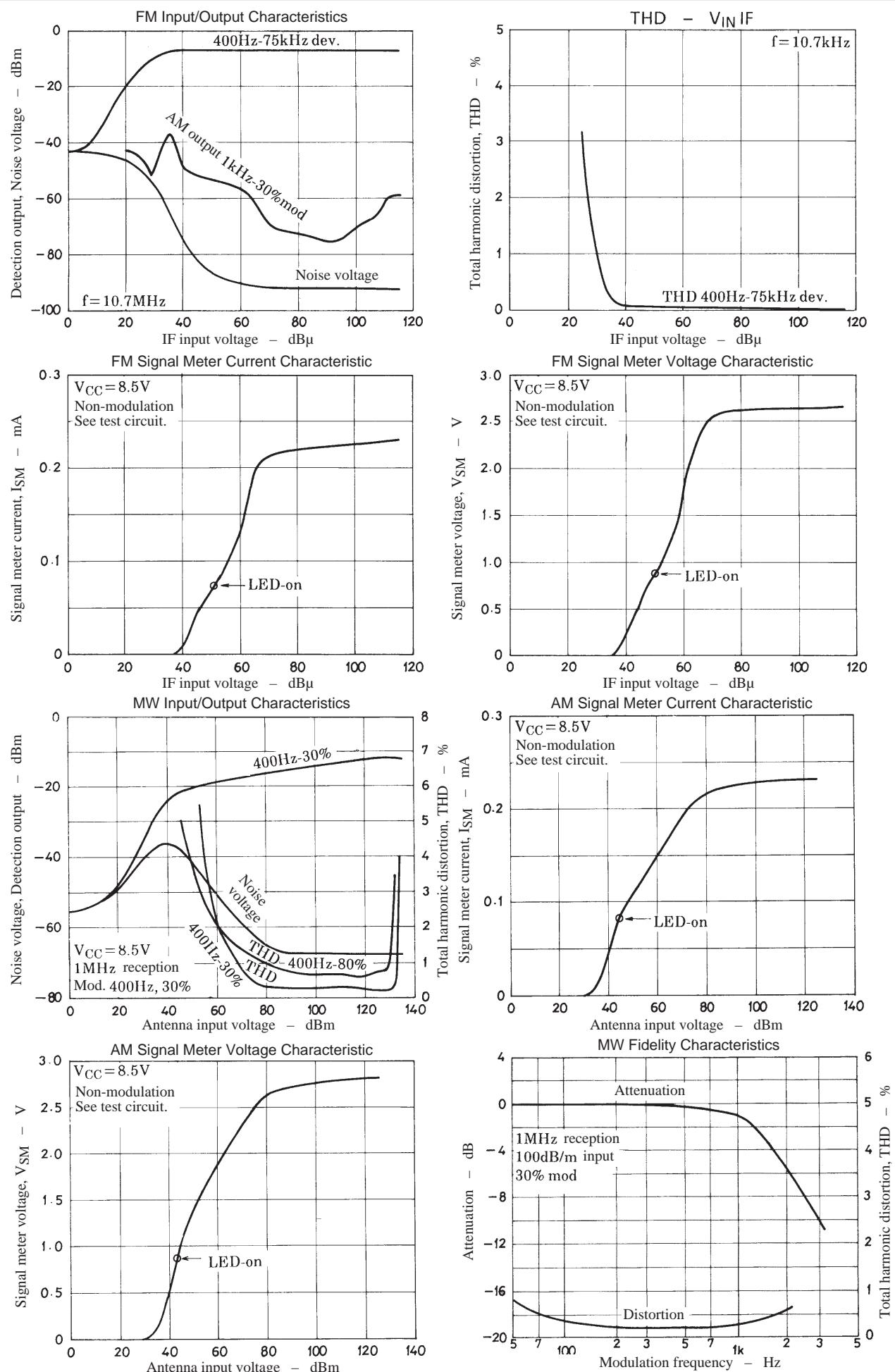
AM

—	Parameter	Frequency	—	Admittance		Unit
				AGC-off (V <sub>16</sub> =1.4V)	AGC-on (V <sub>16</sub> =2.5V)	
RF	γ <sub>i19</sub>	1MHz	r <sub>i</sub>	15	16	kΩ
			c <sub>i</sub>	4	4	pF
MIX	γ <sub>o17</sub>	500kHz	r <sub>o</sub>	—	—	kΩ
			c <sub>o</sub>	3	3	pF
IF	γ <sub>i15</sub>	500kHz	r <sub>i</sub>	2	2	kΩ
			c <sub>o</sub>	10	8	pF

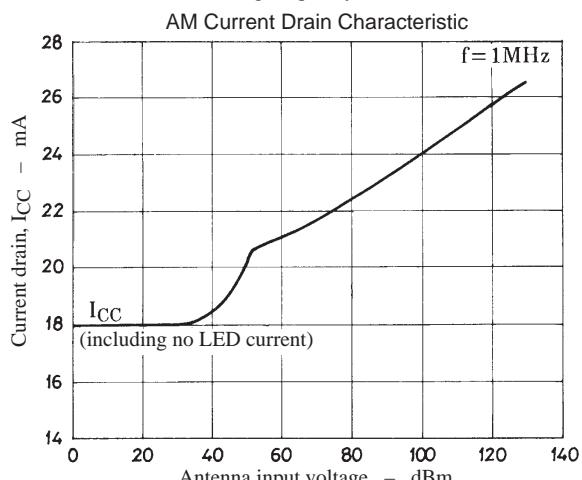
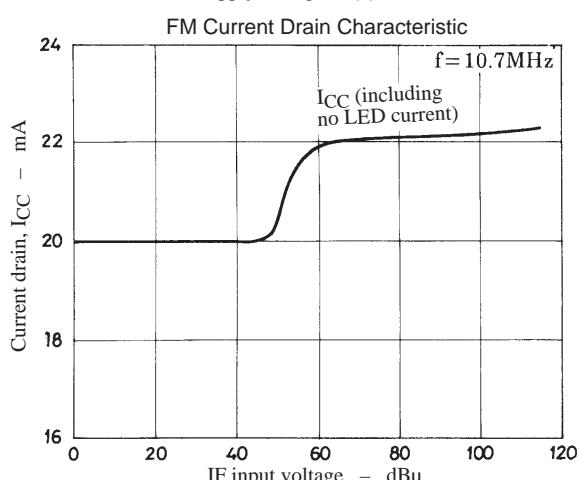
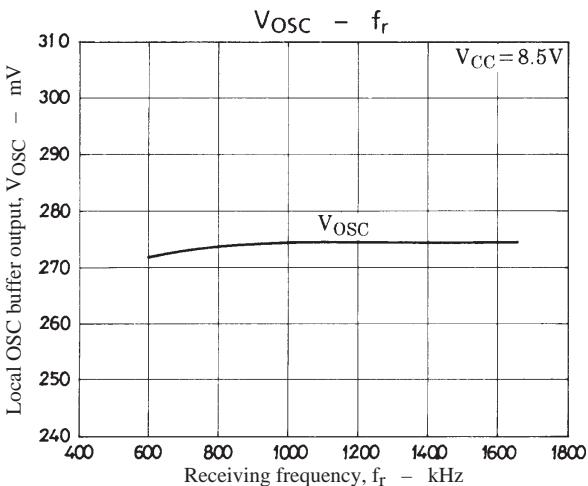
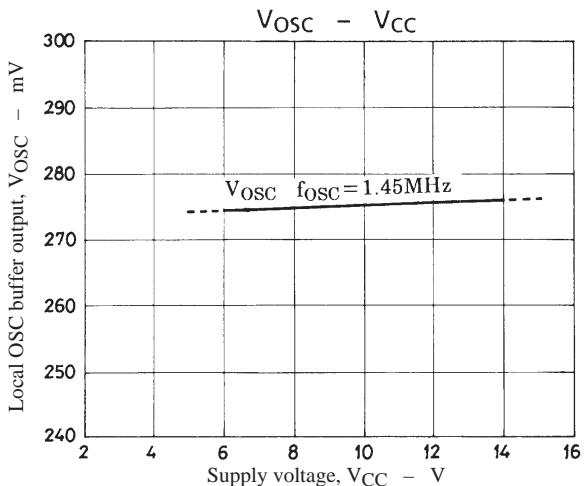
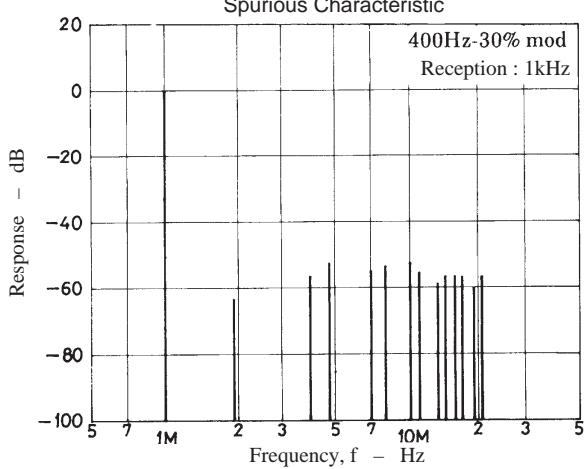
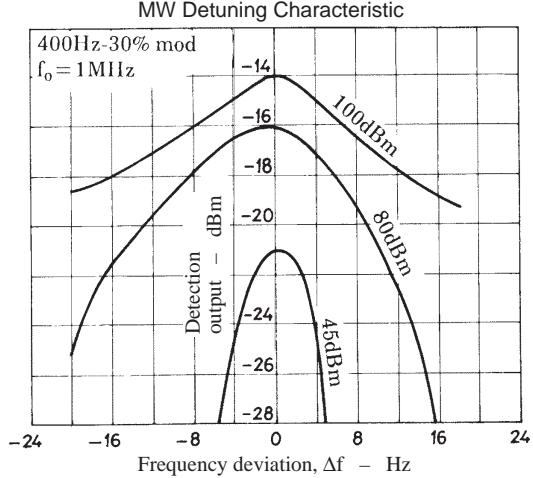
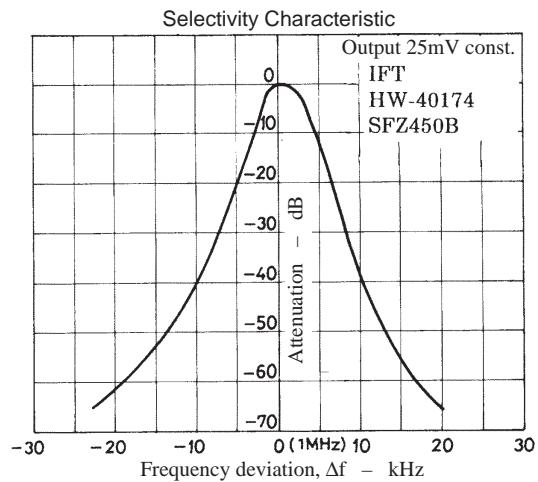
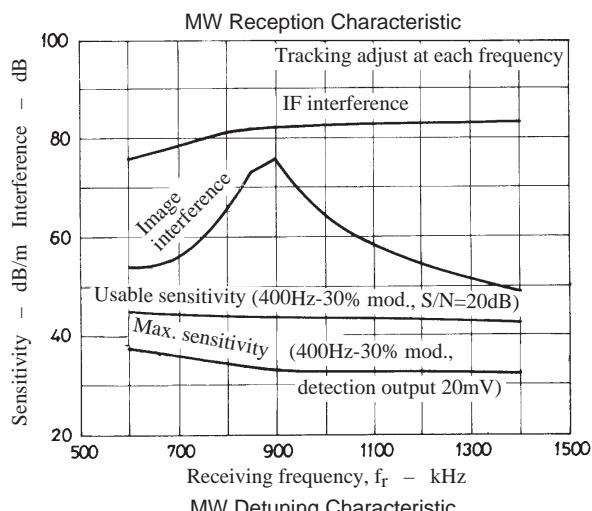
## Test Circuit : FM, AM-MW



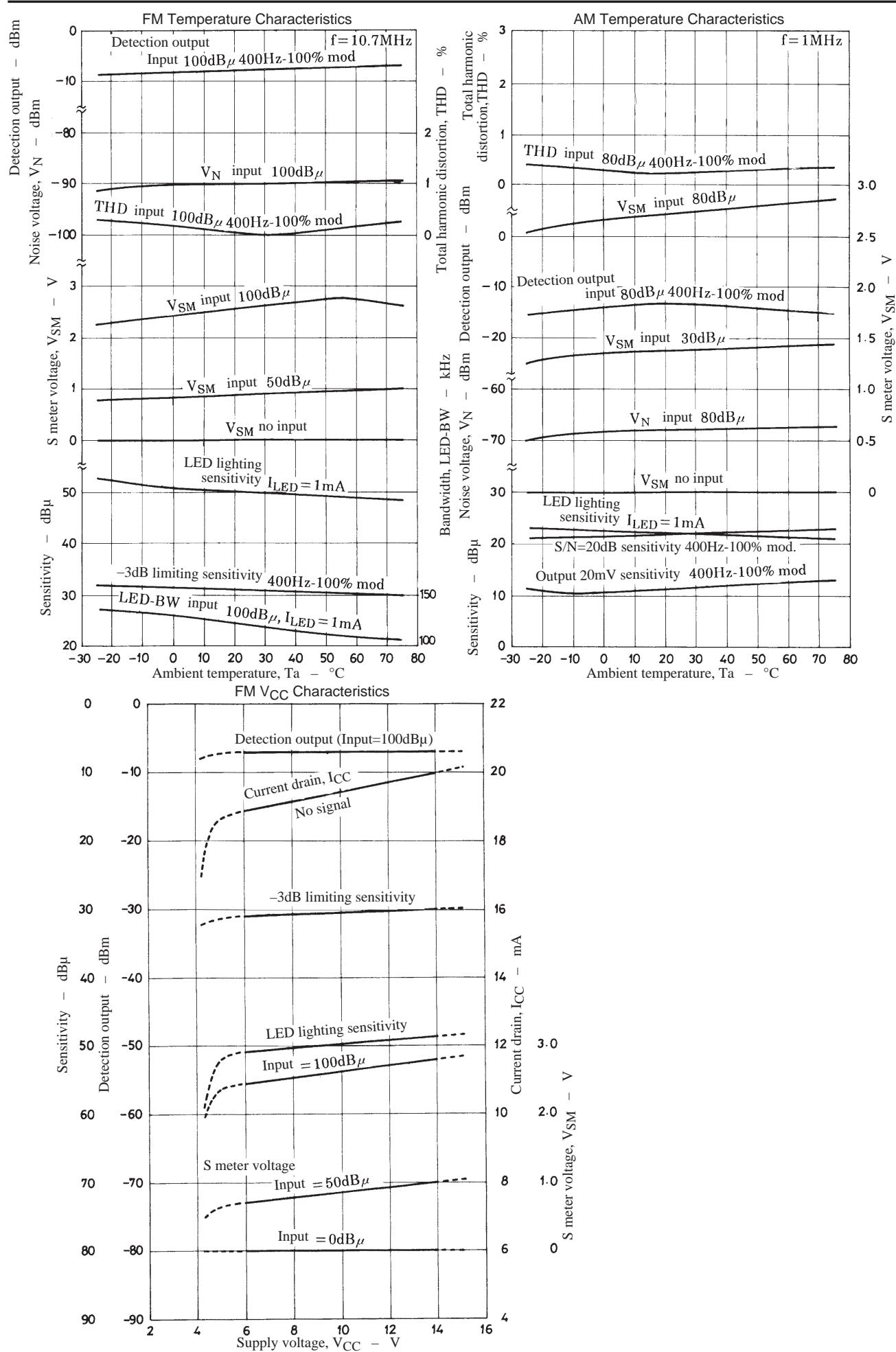
# LA1265



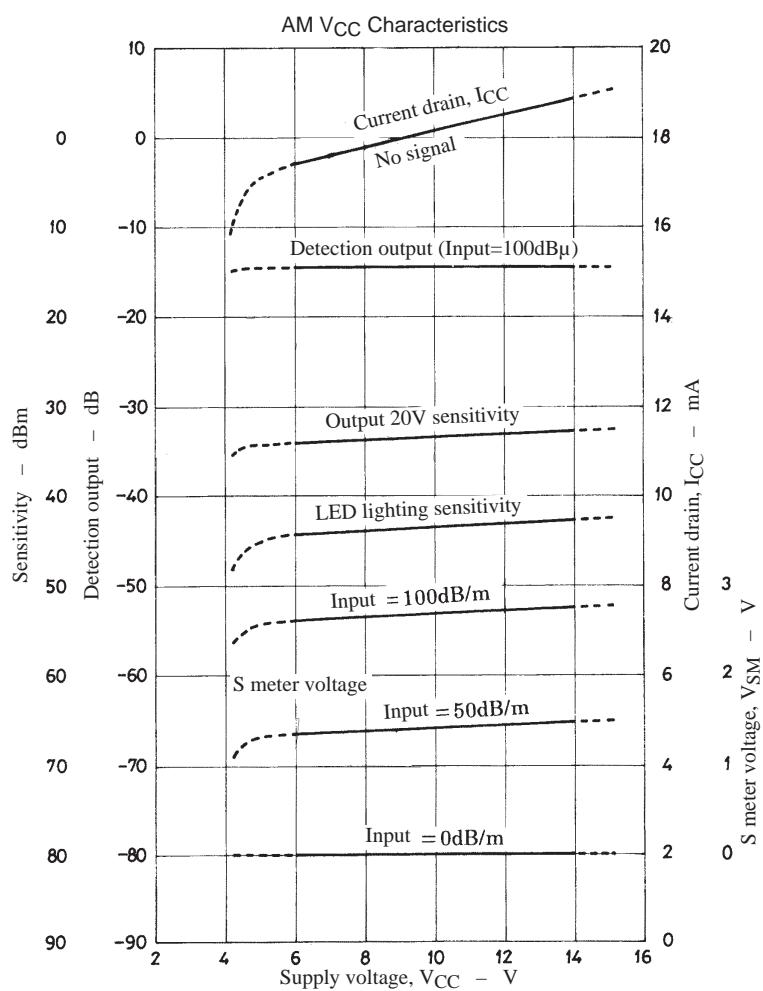
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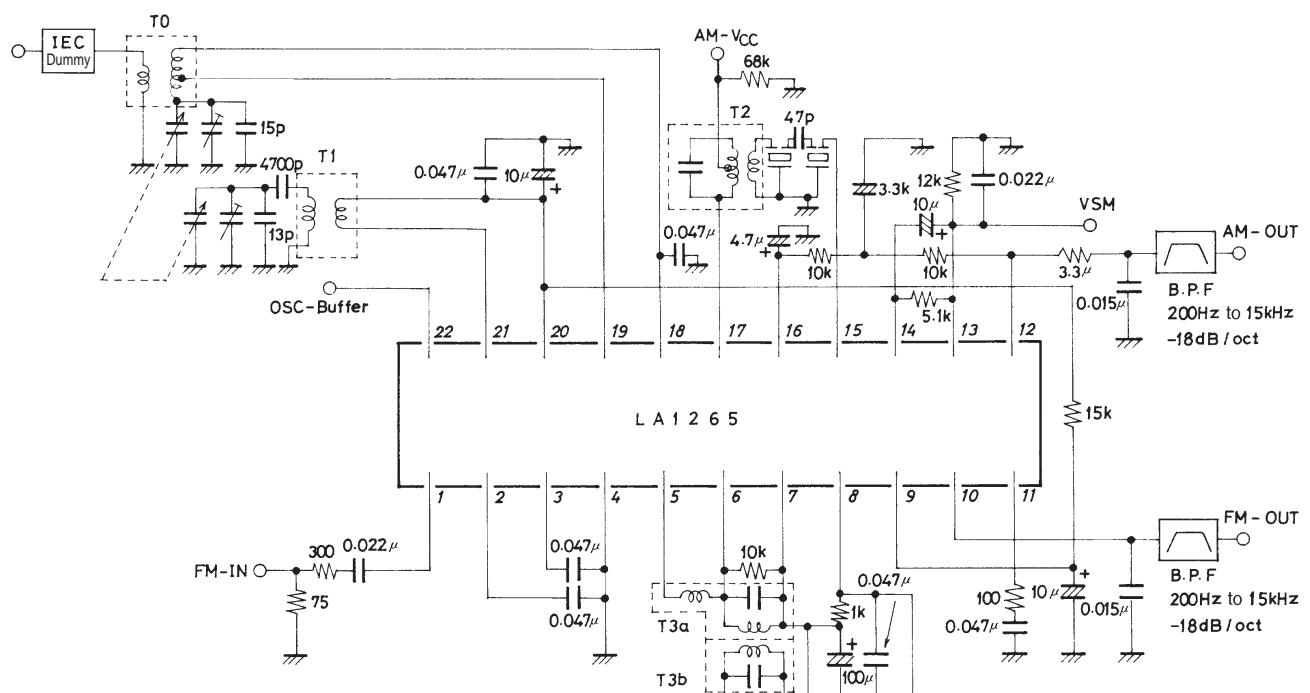
# LA1265



# LA1265



**Test Circuit : SW2**



T0 : YT-30177 (Mitsumi)

T1 : HW-40184 (Mitsumi)

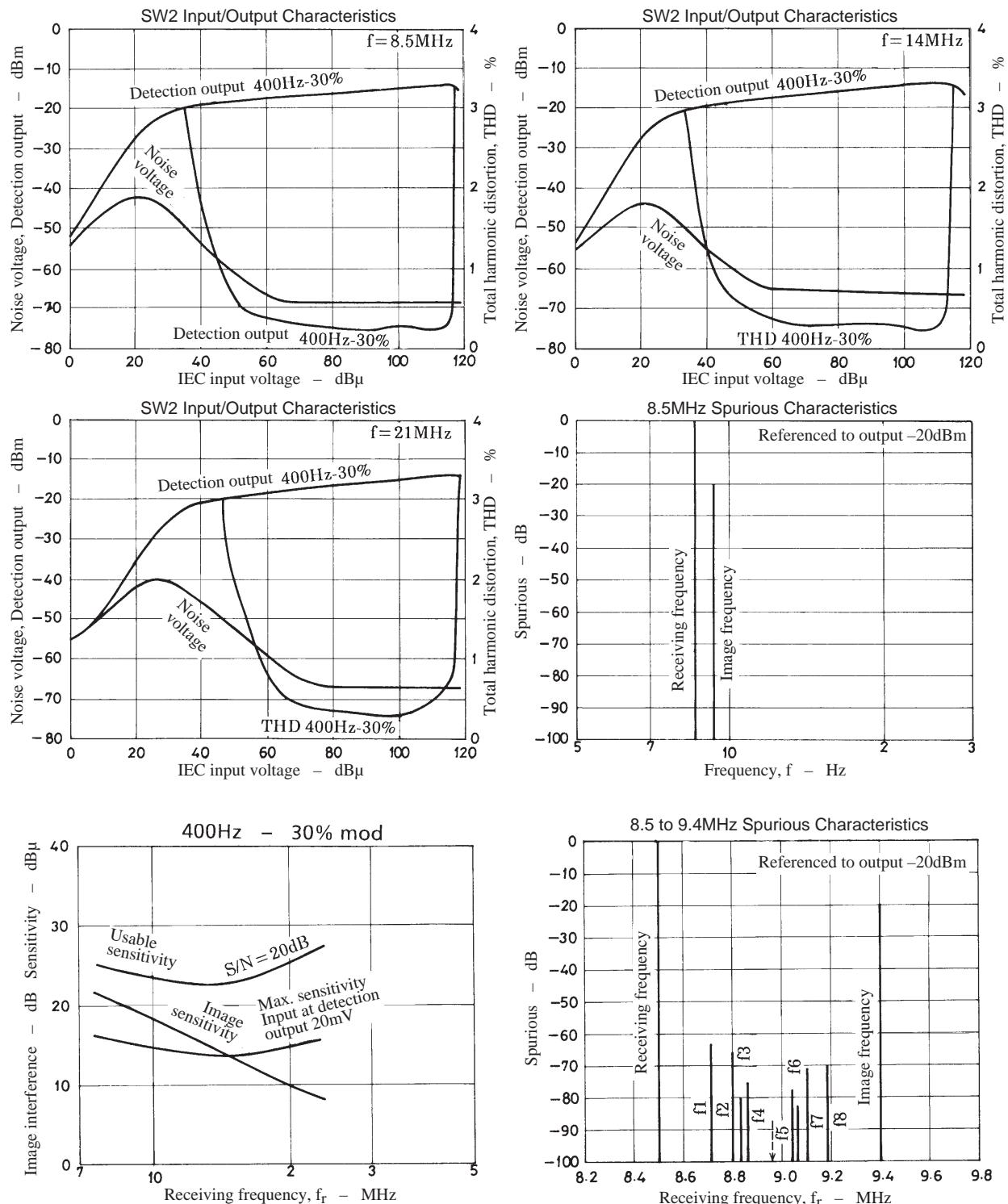
T2 : HW-40174 (Mitsumi)

T3a : HW-40130, T3b : HW-40131 (Mitsumi)

Variable capacitor PVC 22KTL (Mitsumi)

Unit (resistance : Ω, capacitance : F)

## LA1265



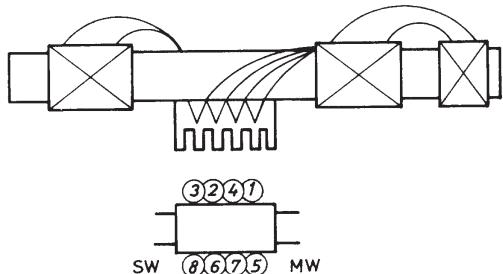
$f_1 : 8.724\text{MHz} \rightarrow 2f_{\text{OSC}} - 2f_1 = 455\text{kHz}$   
 $f_2 : 8.799\text{MHz} \rightarrow 3f_{\text{OSC}} - 3f_2 = 455\text{kHz}$   
 $f_3 : 8.836\text{MHz} \rightarrow 4f_{\text{OSC}} - 4f_3 = 455\text{kHz}$   
 $f_4 : 8.859\text{MHz} \rightarrow 5f_{\text{OSC}} - 5f_4 = 455\text{kHz}$   
 $f_5 : 9.038\text{MHz} \rightarrow 5f_5 - 5f_{\text{OSC}} = 455\text{kHz}$   
 $f_6 : 9.061\text{MHz} \rightarrow 4f_6 - 4f_{\text{OSC}} = 455\text{kHz}$   
 $f_7 : 9.098\text{MHz} \rightarrow 3f_7 - 3f_{\text{OSC}} = 455\text{kHz}$   
 $f_8 : 9.173\text{MHz} \rightarrow 2f_8 - 2f_{\text{OSC}} = 455\text{kHz}$

## Coil Specifications

MW antenna

Bar antenna (for PVC22KTL)

- TN-10896 (Mitsumi)



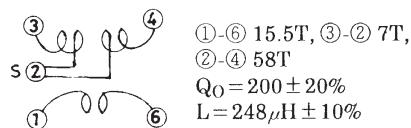
- ①-② 22T + 49T, ③-④ 10T  
Tight solenoid direct winding
- ⑤-⑥ 17T 0.5φ space winding
- ⑦-⑧ 4T tight solenoid winding
- ①-② L = 260μH, Q<sub>0</sub> = 330 ( $\geq 200$ )
- ⑤-⑥ L = 15μH, Q<sub>0</sub> = 250 ( $\geq 150$ )

Loop antenna (for SVC321)

- LA300 (Korin Giken)

Loop antenna matching coil

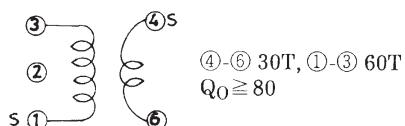
- KT-412



MW OSC

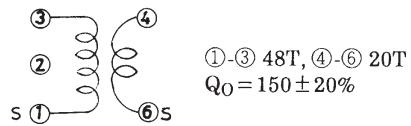
- 4147-1457-177 (Sumida)

For PVC22KTL



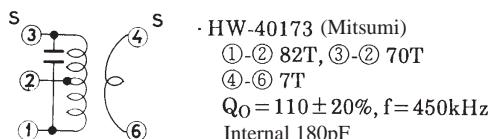
- KO-387 (Korin Giken)

For SVC321



AM-IFT

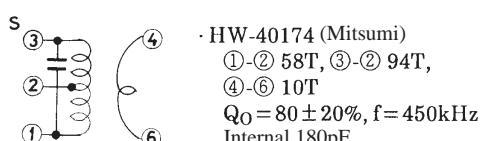
Matching coil for SFU450B (1-element type)



- 2150-2162-197 (Sumida)

①-② 103T, ③-② 71T,  
④-⑥ 8T  
 $Q_0 \geq 80$ , f = 450kHz  
Internal 180pF

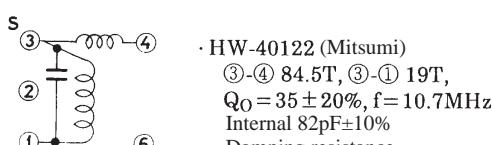
Matching coil for SFZ450B (2-element type)



- 2150-2061-049 (Sumida)

①-② 54T, ③-② 120T,  
④-⑥ 12T  
 $Q_0 \geq 40$   
Internal 180pF

FM single tuning detection coil

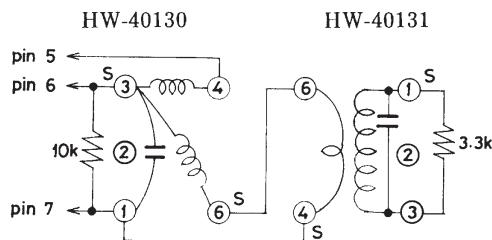


- 2231-016 (Sumida)

③-④ 73.5T, ③-① 19T,  
 $Q_0 = 30 \pm 20\%$ , f = 10.7MHz  
Internal 82pF±10%  
Damping resistance

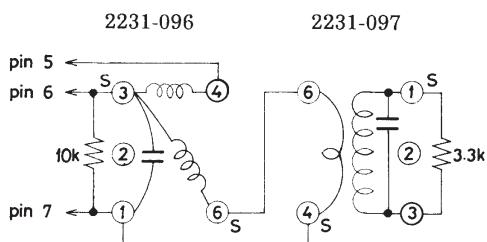
## LA1265

FM double tuning detection coil



- HW-40130 (Mitsumi)
  - ③-④ 86.5T
  - ③-⑥ 13.5T
  - $Q_0 = 50 \pm 20\%$
  - Internal 100pF $\pm 10\%$

- HW-40131 (Mitsumi)
  - ④-⑥ 1T
  - ①-③ 19T
  - $Q_0 = 35 \pm 20\%$
  - Internal 100pF $\pm 10\%$



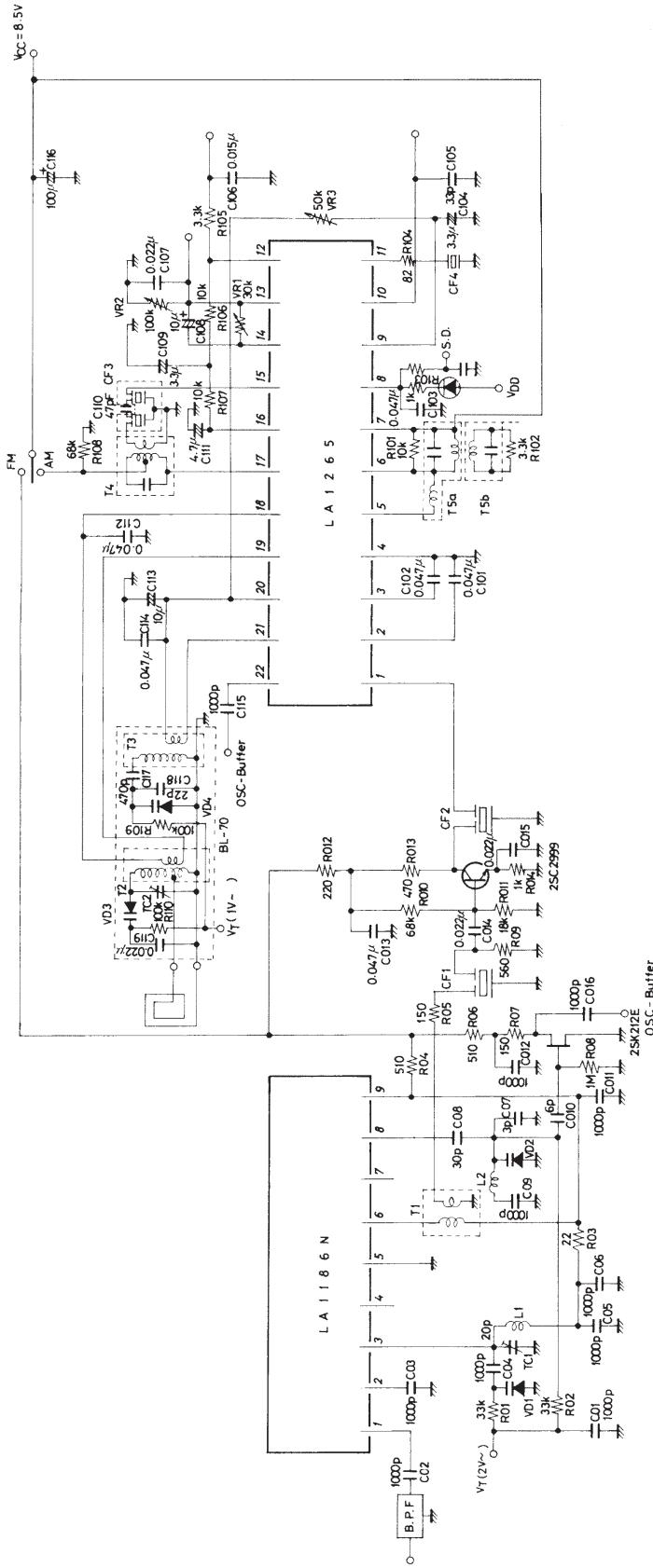
- 2231-096 (Sumida)
  - ③-④ 73.5T
  - ③-⑥ 23.5T
  - $Q_0 = 50 \pm 20\%$
  - Internal 62pF $\pm 10\%$

- 2231-097 (Sumida)
  - ④-⑥ 2T
  - ①-③ 21T
  - $Q_0 = 47 \pm 20\%$
  - Internal 82pF $\pm 10\%$

Unit (resistance :  $\Omega$ )

## LA1265

**Sample Application Circuit : LA1186N + LA1265 (US Band)**



B.P.F SNY-2101 (Sumida)

V<sub>D1</sub>, V<sub>D2</sub>=SVC201

V<sub>D3</sub>, V<sub>D4</sub>=SVC321

T<sub>C1</sub>=10pF

T<sub>C2</sub>=20pF

CF1, CF2=SFE10.7MA

CF3=SFZ450B (Murata)

CF4=BFU450CN (Murata)

L1 : YT-30196 (Mitsumi), 0708-700 (Sumida)

L2 : HW50433 (Mitsumi), 0267-034 (Sumida)

T1 : YT-30224 (Mitsumi)

T2 : KL412 (Korin) ] BL-70

T3 : KO387 (Korin)

T4 : HW-40174 (Mitsumi), 2150-2061-049 (Sumida)

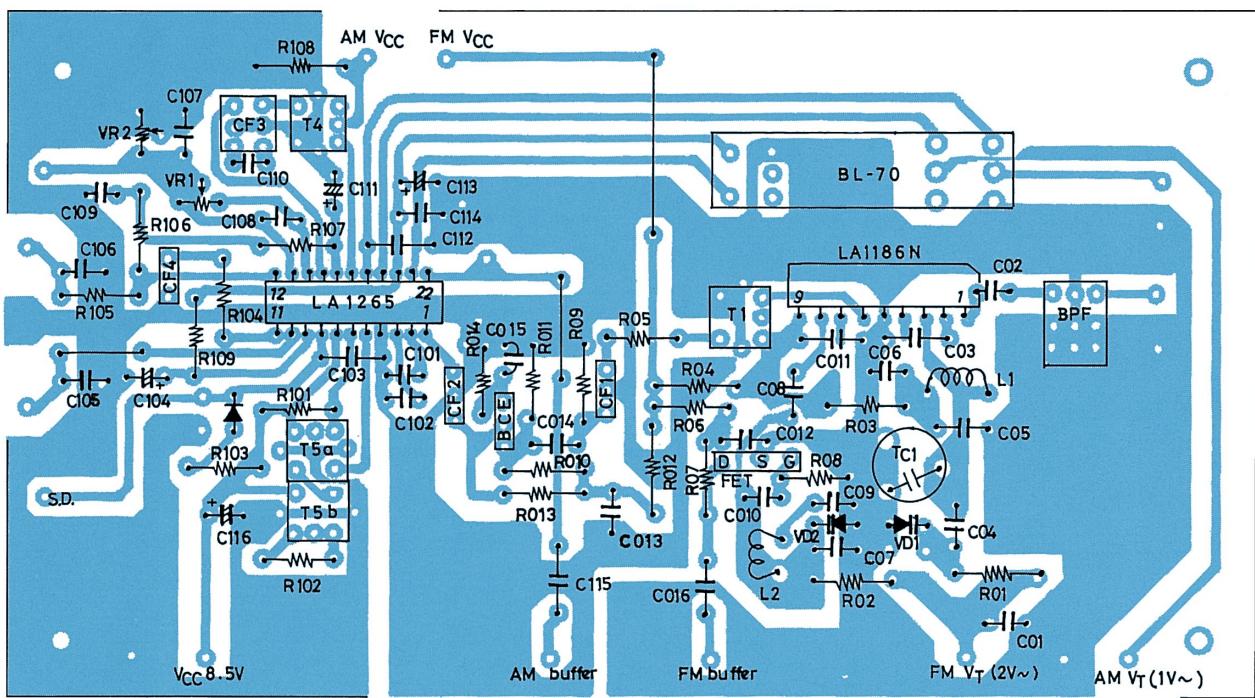
T5a : HW-40130 (Mitsumi), 2231-096 (Sumida)

T5b : HW-40130 (Mitsumi), 2231-096 (Sumida)

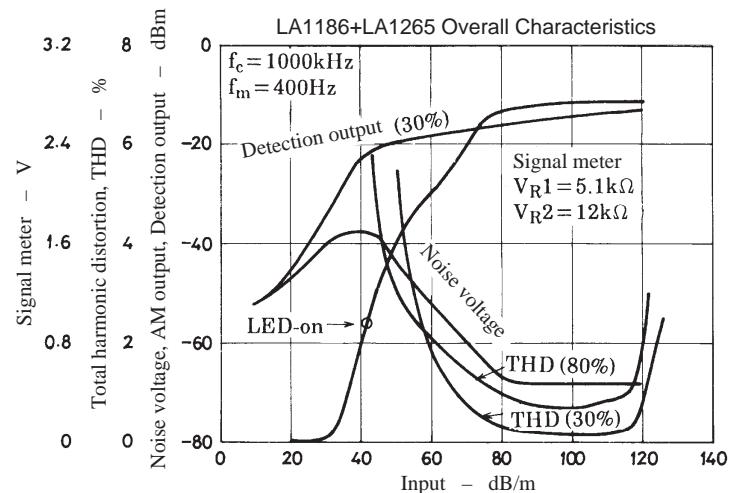
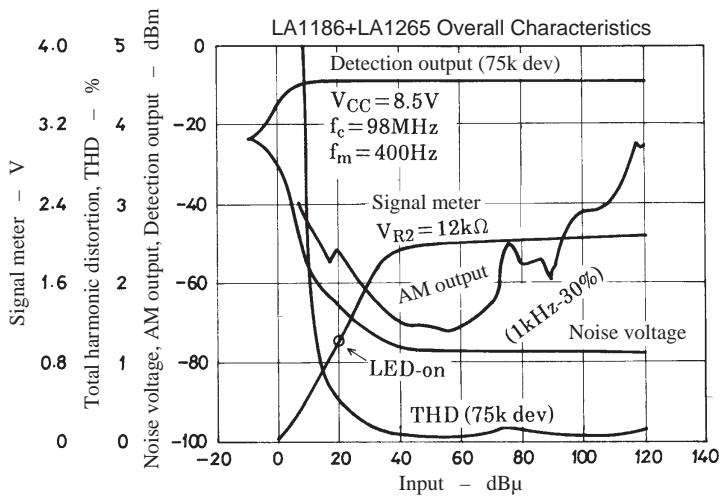
Unit (resistance : Ω, capacitance : F)

LA1265

## Sample Printed Circuit Pattern (Cu-foiled area)



$85 \times 155 \text{ mm}^2$



- No products described or contained herein are intended for use in surgical implants, life-support systems, aerospace equipment, nuclear power control systems, vehicles, disaster/crime-prevention equipment and the like, the failure of which may directly or indirectly cause injury, death or property loss.
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