



















# LT6233/LT6233-10/ LT6234/LT6235

## ELECTRICAL CHARACTERISTICS

**Note 1:** Absolute maximum ratings are those values beyond which the life of the device may be impaired.

**Note 2:** Inputs are protected by back-to-back diodes. If the differential input voltage exceeds 0.7V, the input current must be limited to less than 40mA.

**Note 3:** A heat sink may be required to keep the junction temperature below the absolute maximum rating when the output is shorted indefinitely.

**Note 4:** The LT6233C/LT6233I the LT6234C/LT6234I, and LT6235C/LT6235I are guaranteed functional over the temperature range of  $-40^{\circ}\text{C}$  and  $85^{\circ}\text{C}$ .

**Note 5:** The LT6233C/LT6234C/LT6235C are guaranteed to meet specified performance from  $0^{\circ}\text{C}$  to  $70^{\circ}\text{C}$ . The LT6233C/LT6234C/LT6235C are designed, characterized and expected to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ , but are not tested or QA sampled at these temperatures.

The LT6233I/LT6234I/LT6235I are guaranteed to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ .

**Note 6:** Matching parameters are the difference between the two amplifiers A and D and between B and C of the LT6235; between the two amplifiers of the LT6234. CMRR and PSRR match are defined as follows: CMRR and PSRR are measured in  $\mu\text{V/V}$  on the matched amplifiers. The difference is calculated between the matching sides in  $\mu\text{V/V}$ . The result is converted to dB.

**Note 7:** Minimum supply voltage is guaranteed by power supply rejection ratio test.

**Note 8:** Output voltage swings are measured between the output and power supply rails.

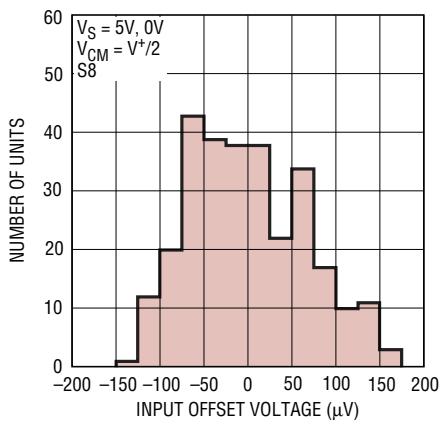
**Note 9:** Full-power bandwidth is calculated from the slew rate:  
 $\text{FPBW} = \text{SR}/2\pi V_p$

**Note 10:** This parameter is not 100% tested.

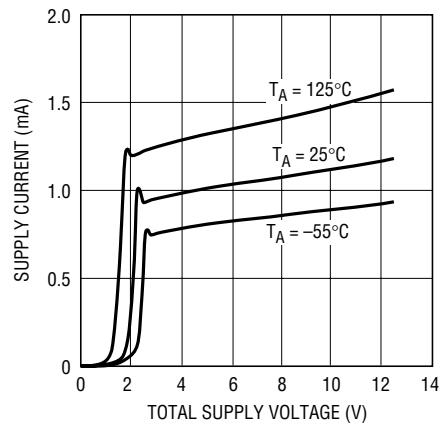
## TYPICAL PERFORMANCE CHARACTERISTICS

(LT6233/LT6234/LT6235)

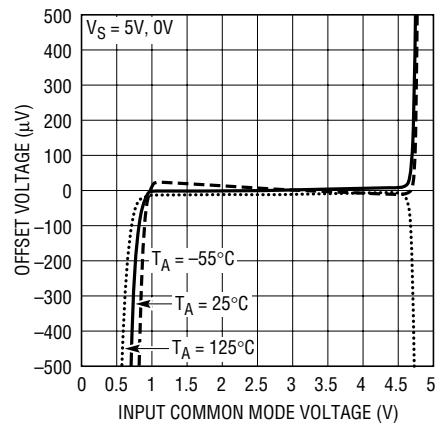
V<sub>OS</sub> Distribution



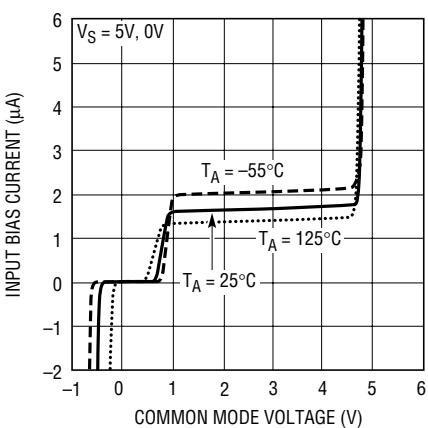
Supply Current vs Supply Voltage  
(Per Amplifier)



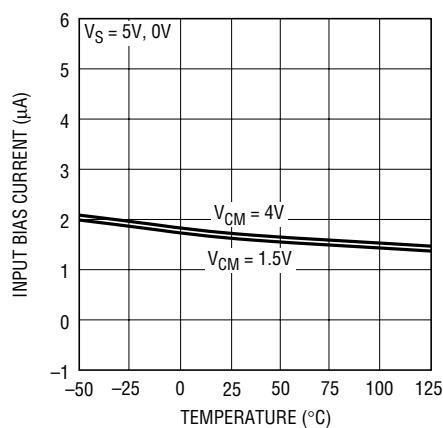
Offset Voltage vs Input Common Mode Voltage



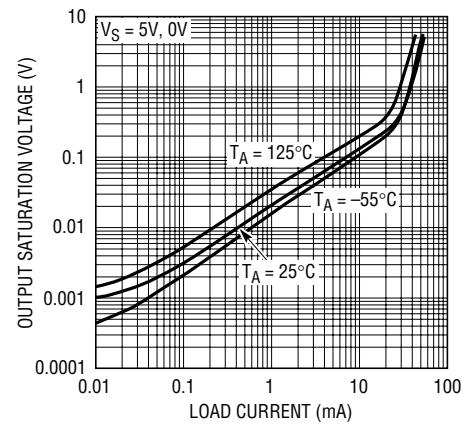
Input Bias Current vs  
Common Mode Voltage



Input Bias Current vs Temperature



Output Saturation Voltage vs  
Load Current (Output Low)



623345f





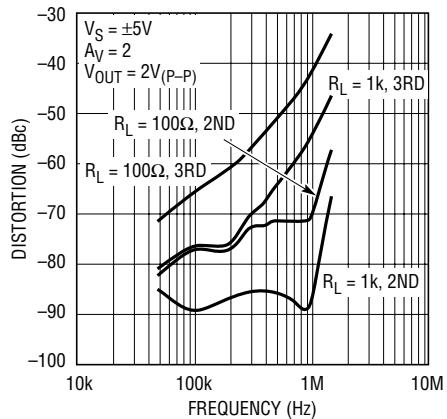


# LT6233/LT6233-10/ LT6234/LT6235

## TYPICAL PERFORMANCE CHARACTERISTICS

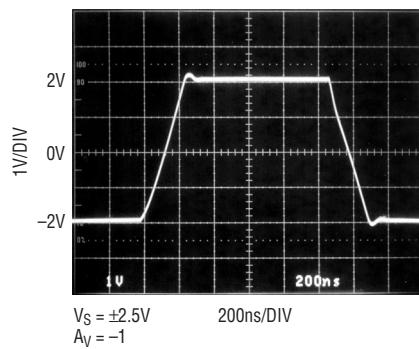
(LT6233/LT6234/LT6235)

### Distortion vs Frequency



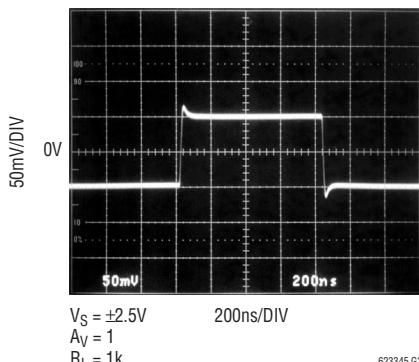
623345 G34

### Large Signal Response



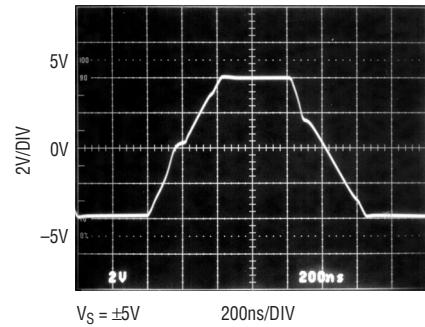
623345 G35

### Small Signal Response



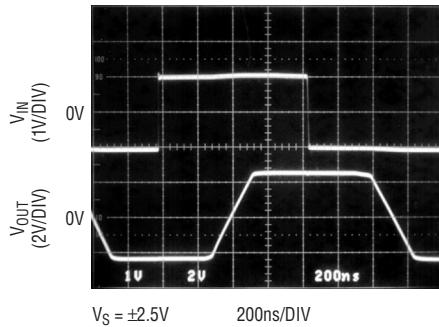
623345 G36

### Large Signal Response



623345 G37

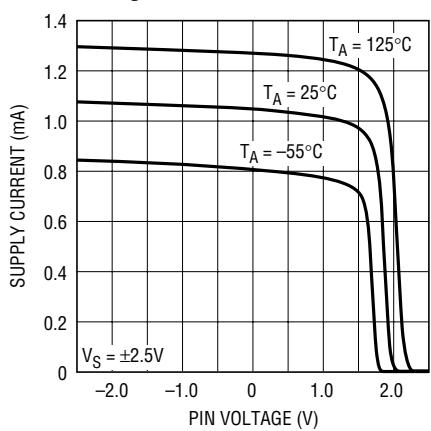
### Output Overdrive Recovery



623345 G38

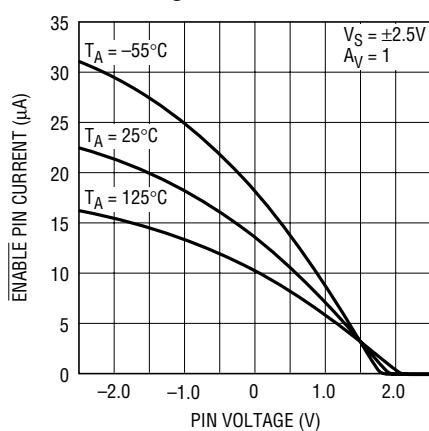
### (LT6233) ENABLE Characteristics

#### Supply Current vs ENABLE Pin Voltage



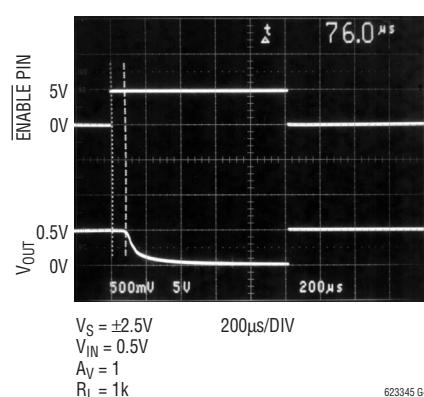
623345 G39

#### ENABLE Pin Current vs ENABLE Pin Voltage



623345 G40

#### ENABLE Pin Response Time



623345 G41

623345f

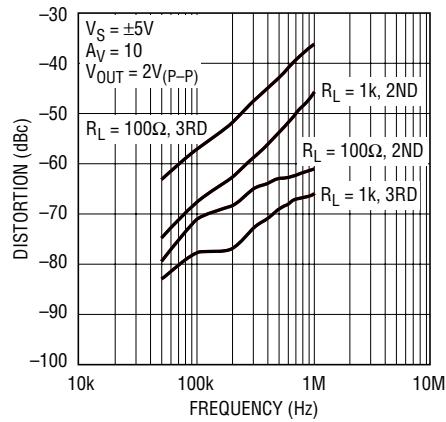


# LT6233/LT6233-10/ LT6234/LT6235

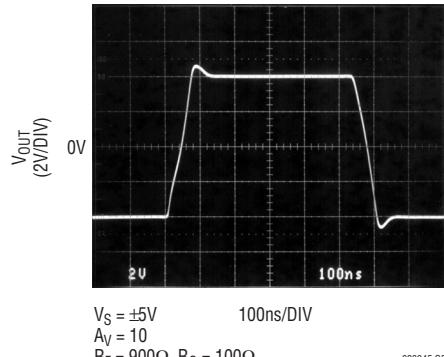
## TYPICAL PERFORMANCE CHARACTERISTICS

(LT6233-10)

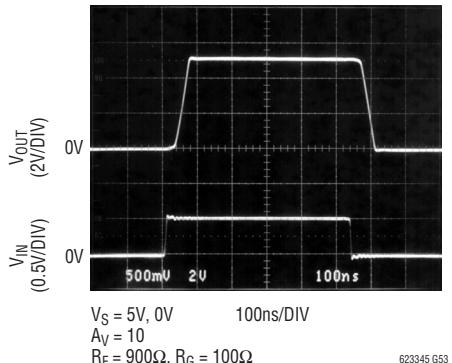
### 2<sup>nd</sup> and 3<sup>rd</sup> Harmonic Distortion vs Frequency



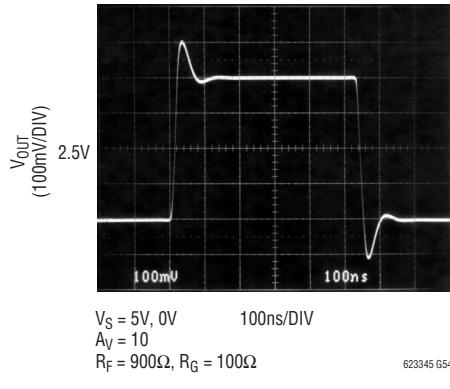
### Large Signal Response



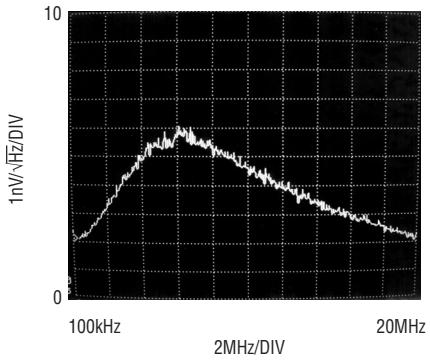
### Output-Overload Recovery



### Small Signal Response



### Input Referred High Frequency Noise Spectrum



623345 G53

623345 G55

623345f



# LT6233/LT6233-10/ LT6234/LT6235

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## APPLICATIONS INFORMATION

With  $R_S + R_G||R_{FB} = 225\Omega$  the total noise of the amplifier is:

$$e_N = \sqrt{(1.9\text{nV})^2 + (1.9\text{nV})^2} = 2.69\text{nV}/\sqrt{\text{Hz}}$$

Below this resistance value, the amplifier dominates the noise, but in the region between  $225\Omega$  and about  $30\text{k}$ , the noise is dominated by the resistor thermal noise. As the total resistance is further increased beyond  $30\text{k}$ , the amplifier noise current multiplied by the total resistance eventually dominates the noise.

The product of  $e_N \cdot \sqrt{I_{SUPPLY}}$  is an interesting way to gauge low noise amplifiers. Most low noise amplifiers with low  $e_N$  have high  $I_{SUPPLY}$  current. In applications that require low noise voltage with the lowest possible supply current, this product can prove to be enlightening. The LT6233/LT6234/LT6235 have an  $e_N \cdot \sqrt{I_{SUPPLY}}$  product of only 2.1 per amplifier, yet it is common to see amplifiers with similar noise specifications to have  $e_N \cdot \sqrt{I_{SUPPLY}}$  as high as 13.5.

For a complete discussion of amplifier noise, see the LT1028 data sheet.

### Enable Pin

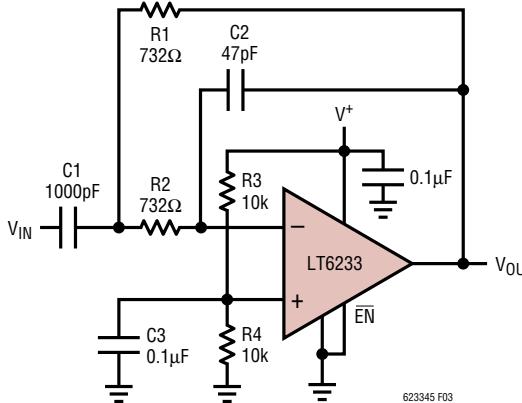
The LT6233 and LT6233-10 include an ENABLE pin that shuts down the amplifier to  $10\mu\text{A}$  maximum supply current. The ENABLE pin must be driven high to within  $0.35\text{V}$  of  $V^+$  to shut down the supply current. This can be accomplished with simple gate logic; however care must be taken if the logic and the LT6233 operate from different supplies. If this is the case, then open drain logic can be used with a pull-up resistor to ensure that the amplifier remains off. See Typical Characteristic Curves.

The output leakage current when disabled is very low; however, current can flow into the input protection diodes D1 and D2 if the output voltage exceeds the input voltage by a diode drop.

# LT6233/LT6233-10/ LT6234/LT6235

## APPLICATIONS INFORMATION

### Single Supply, Low Noise, Low Power, Bandpass Filter with Gain = 10



$$f_0 = \frac{1}{2\pi RC} = 1\text{MHz}$$

$$C = \sqrt{C_1 C_2}, R = R_1 = R_2$$

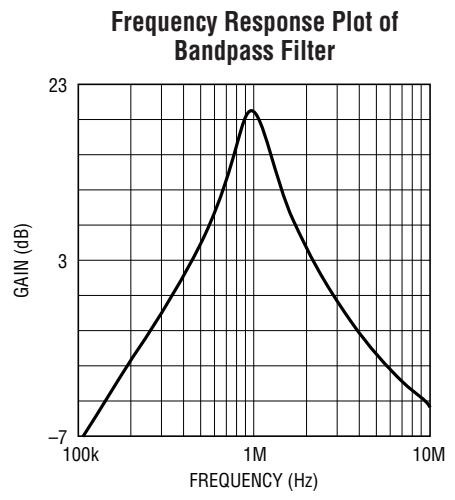
$$f_0 = \left(\frac{732\Omega}{R}\right) \text{MHz, MAXIMUM } f_0 = 1\text{MHz}$$

$$f_{-3\text{dB}} = \frac{f_0}{2.5}$$

$$A_V = 20\text{dB at } f_0$$

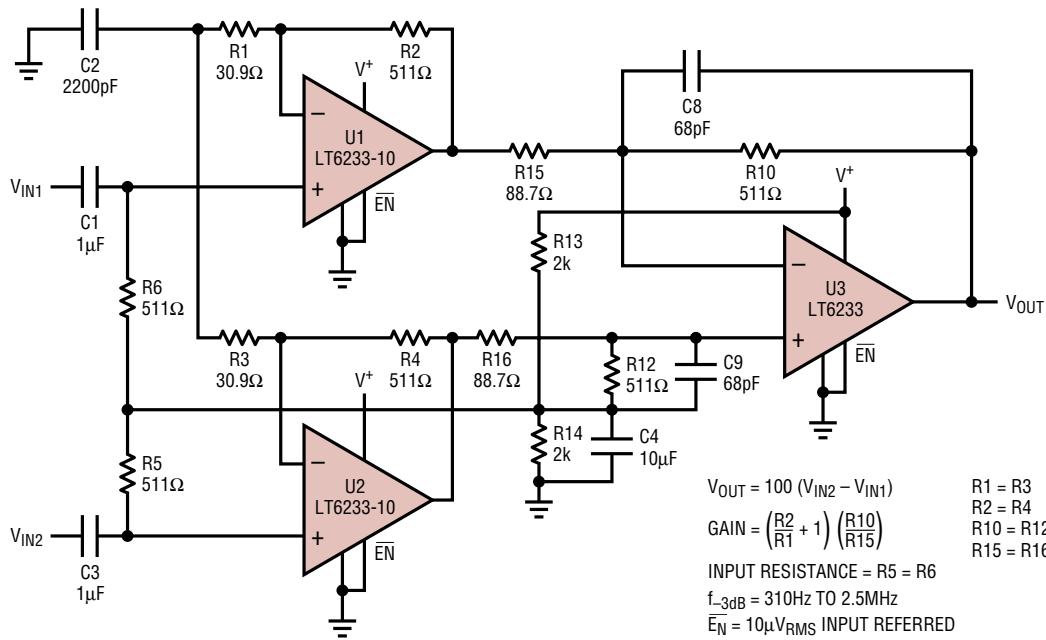
$$\bar{E}_N = 6\mu\text{V RMS INPUT REFERRED}$$

$$I_S = 1.5\text{mA FOR } V^+ = 5\text{V}$$



623345 F04

### Low Power, Low Noise, Single Supply, Instrumentation Amplifier with Gain = 100



$$V_{OUT} = 100(V_{IN2} - V_{IN1})$$

$$\text{GAIN} = \left(\frac{R_2}{R_1} + 1\right) \left(\frac{R_{10}}{R_{15}}\right)$$

$$\text{INPUT RESISTANCE} = R_5 = R_6$$

$$f_{-3\text{dB}} = 310\text{Hz TO } 2.5\text{MHz}$$

$$\bar{E}_N = 10\mu\text{V RMS INPUT REFERRED}$$

$$I_S = 4.7\text{mA FOR } V_S = 5\text{V, } 0\text{V}$$

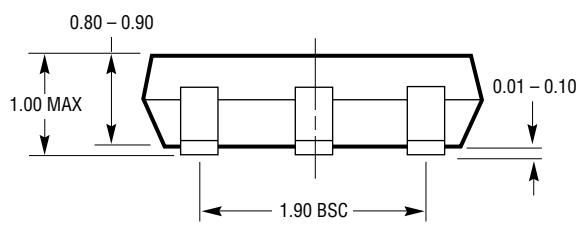
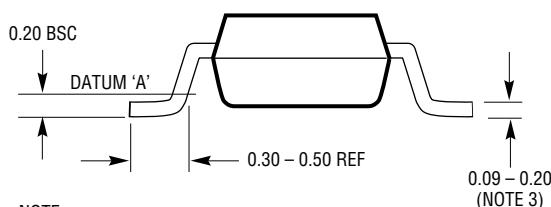
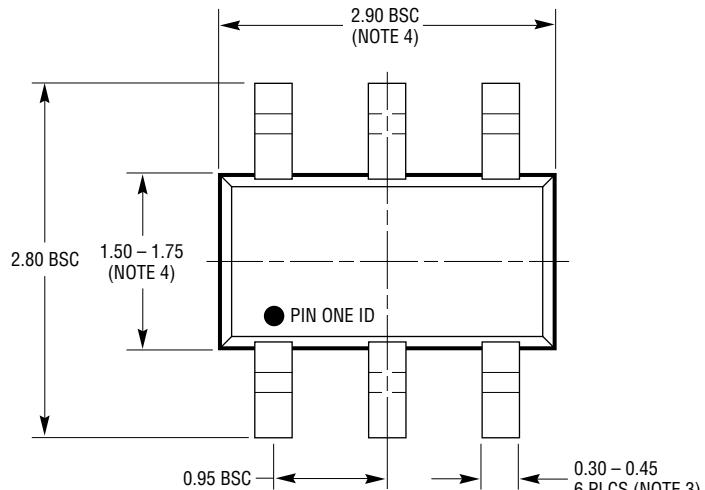
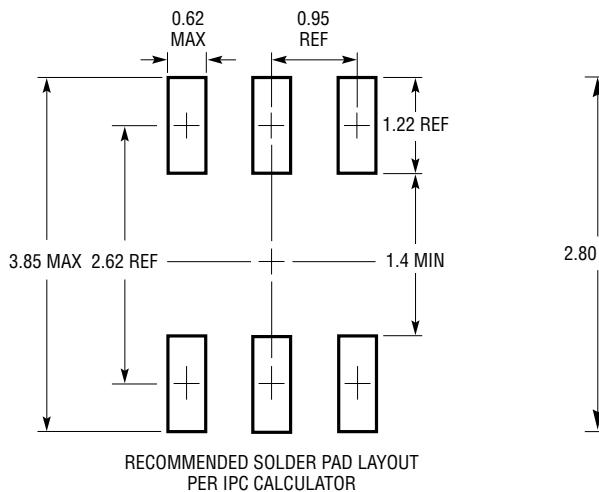
623345 F05

623345f

# LT6233/LT6233-10/ LT6234/LT6235

## PACKAGE DESCRIPTION

**S6 Package  
6-Lead Plastic TSOT-23**  
(Reference LTC DWG # 05-08-1636)



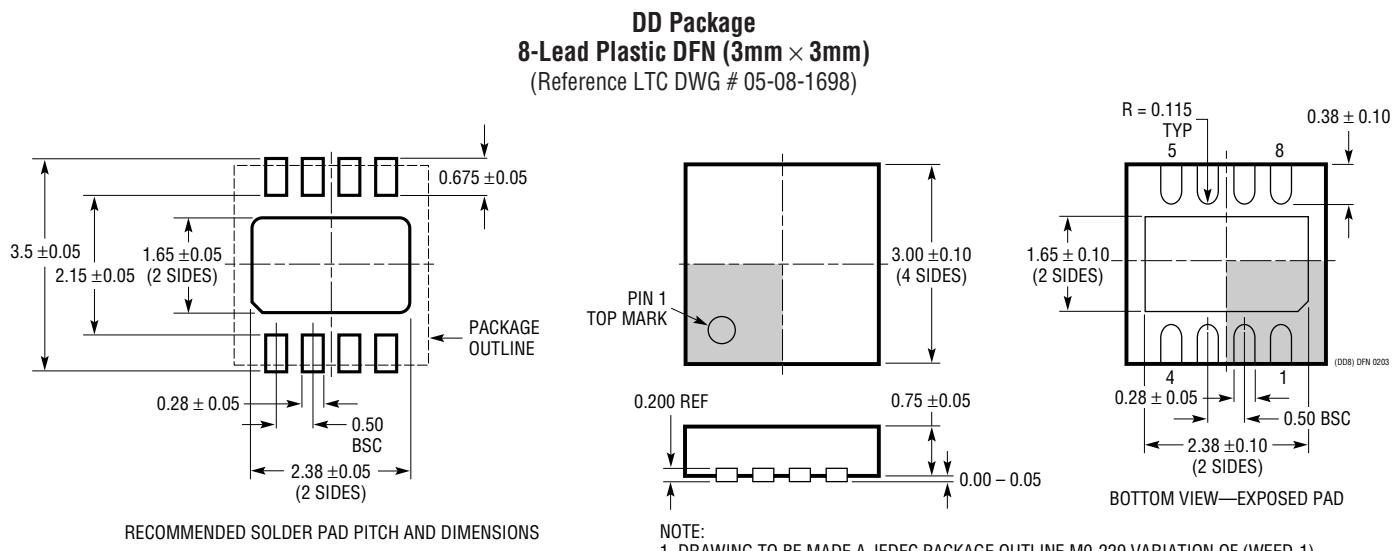
NOTE:

1. DIMENSIONS ARE IN MILLIMETERS
2. DRAWING NOT TO SCALE
3. DIMENSIONS ARE INCLUSIVE OF PLATING
4. DIMENSIONS ARE EXCLUSIVE OF MOLD FLASH AND METAL BURR
5. MOLD FLASH SHALL NOT EXCEED 0.254mm
6. JEDEC PACKAGE REFERENCE IS MO-193

S6 TSOT-23 0302

# LT6233/LT6233-10/ LT6234/LT6235

## PACKAGE DESCRIPTION



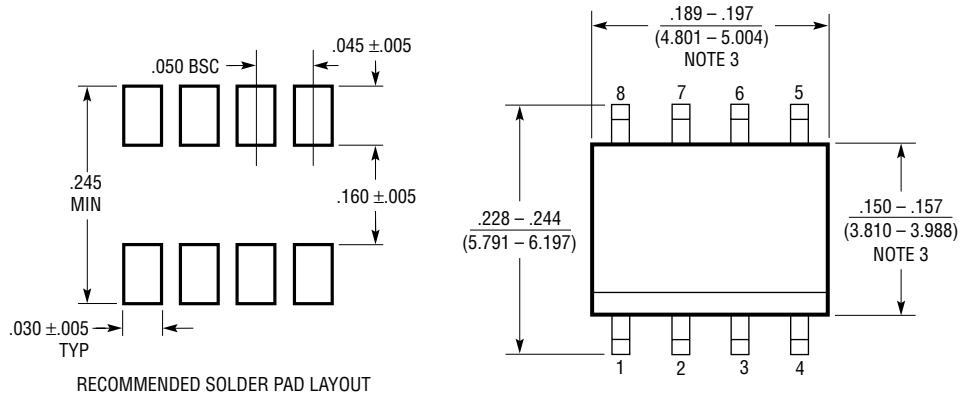
**NOTE:**

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-1)
2. ALL DIMENSIONS ARE IN MILLIMETERS
3. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
4. EXPOSED PAD SHALL BE SOLDER PLATED

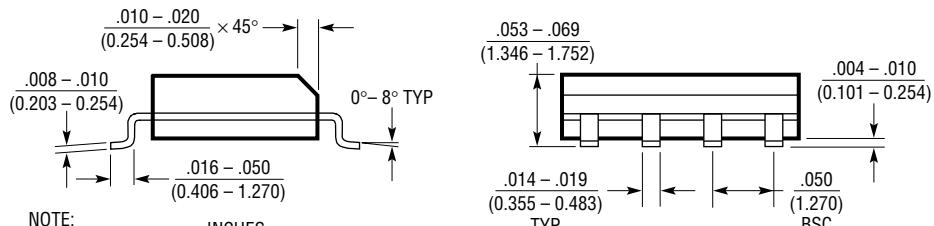
# LT6233/LT6233-10/ LT6234/LT6235

## PACKAGE DESCRIPTION

**S8 Package**  
**8-Lead Plastic Small Outline (Narrow .150 Inch)**  
 (Reference LTC DWG # 05-08-1610)



RECOMMENDED SOLDER PAD LAYOUT



NOTE:

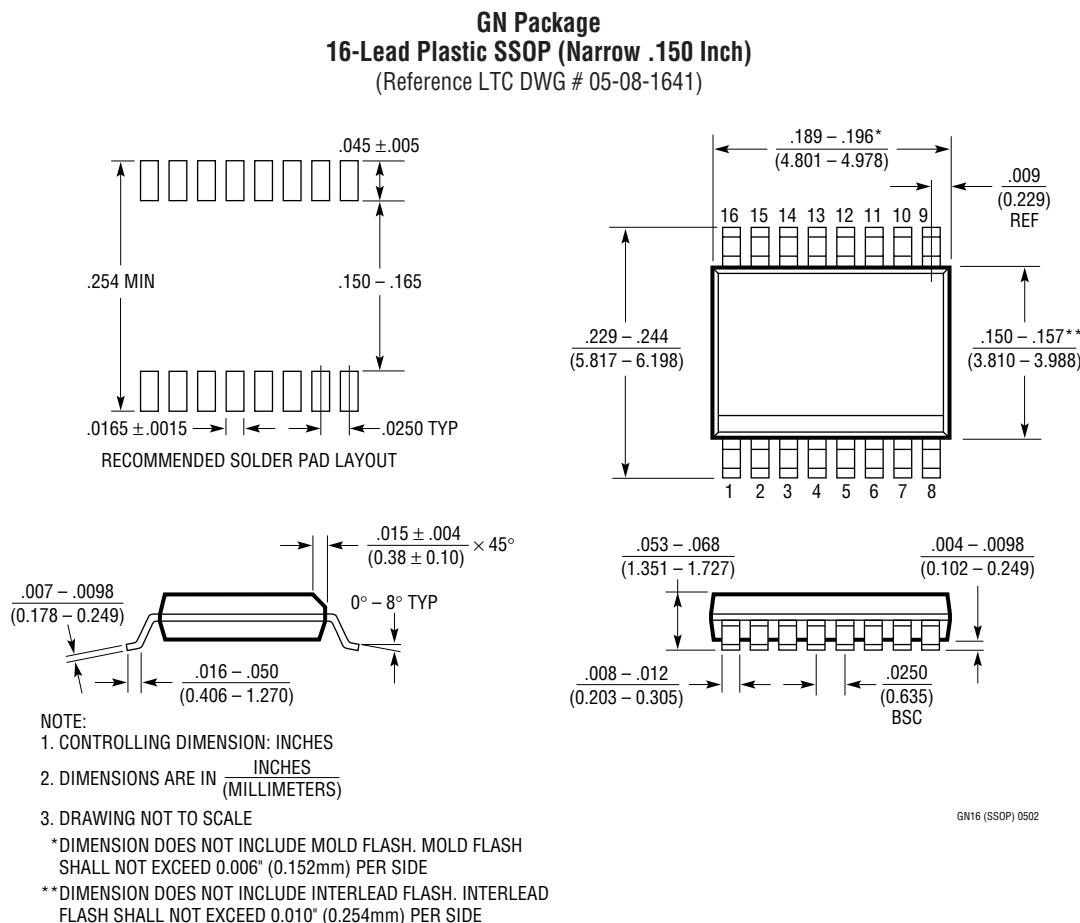
1. DIMENSIONS IN INCHES  
 (MILLIMETERS)

2. DRAWING NOT TO SCALE

3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.  
 MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

S08 0303

## PACKAGE DESCRIPTION



# LT6233/LT6233-10/ LT6234/LT6235

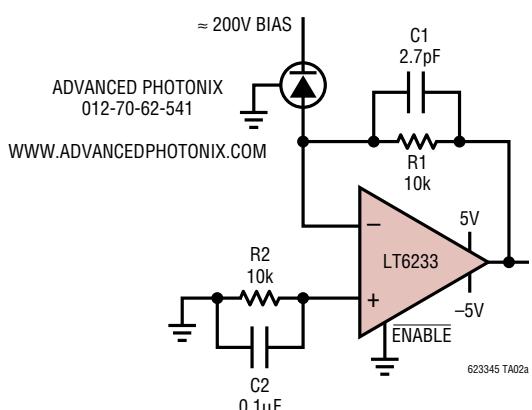
## TYPICAL APPLICATIONS

The LT6233 is applied as a transimpedance amplifier with an I-to-V conversion gain of  $10\text{k}\Omega$  set by R1. The LT6233 is ideally suited to this application because of its low input offset voltage and current, and its low noise. This is because the 10k resistor has an inherent thermal noise of  $13\text{nV}/\sqrt{\text{Hz}}$  or  $1.3\text{pA}/\sqrt{\text{Hz}}$  at room temperature, while the LT6233 contributes only  $2\text{nV}$  and  $0.8\text{pA}/\sqrt{\text{Hz}}$ . So, with respect to both voltage and current noises, the LT6233 is actually quieter than the gain resistor.

The circuit uses an avalanche photodiode with the cathode biased to approximately 200V. When light is incident on

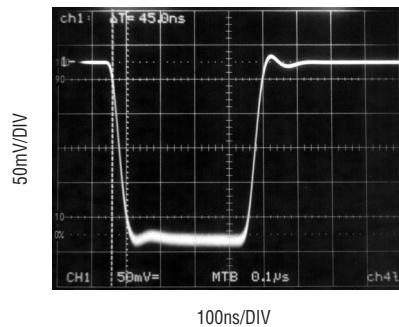
the photodiode, it induces a current  $I_{PD}$  which flows into the amplifier circuit. The amplifier output falls negative to maintain balance at its inputs. The transfer function is therefore  $V_{OUT} = -I_{PD} \cdot 10\text{k}$ . C1 ensures stability and good settling characteristics. Output offset was measured at better than  $500\mu\text{V}$ , so low in part because R2 serves to cancel the DC effects of bias current. Output noise was measured at below  $1\text{mV}_{P-P}$  on a 20MHz measurement bandwidth, with C2 shunting R2's thermal noise. As shown in the scope photo, the rise time is 45ns, indicating a signal bandwidth of 7.8MHz.

### Low Power Avalanche Photodiode Transimpedance Amplifier $I_S = 1.2\text{mA}$



OUTPUT OFFSET =  $500\mu\text{V}$  TYPICAL  
BANDWIDTH = 7.8MHz  
OUTPUT NOISE =  $1\text{mV}_{P-P}$  (20MHz MEASUREMENT BW)

### Photodiode Amplifier Time Domain Response



## RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1028	Single, Ultra Low Noise 50MHz Op Amp	$0.85\text{nV}/\sqrt{\text{Hz}}$
LT1677	Single, Low Noise Rail-to-Rail Amplifier	3V Operation, 2.5mA, $4.5\text{nV}/\sqrt{\text{Hz}}$ , $60\mu\text{V}$ Max $V_{OS}$
LT1806/LT1807	Single/Dual, Low Noise 325MHz Rail-to-Rail Amplifier	2.5V Operation, $550\mu\text{V}$ Max $V_{OS}$ , $3.5\text{nV}/\sqrt{\text{Hz}}$
LT6200/LT6201	Single/Dual, Low Noise 165MHz	$0.95\text{nV}/\sqrt{\text{Hz}}$ , Rail-to-Rail Input and Output
LT6202/LT6203/LT6204	Single/Dual/Quad, Low Noise, Rail-to-Rail Amplifier	$1.9\text{nV}/\sqrt{\text{Hz}}$ , 3mA Max, 100MHz Gain Bandwidth