查询VPS12供应商

Ordering number : EN5309A

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Wideband Output Module (Video Pack)

VPS12

CRT Display Video Output Amplifier: High-Voltage, Wideband Amplifier

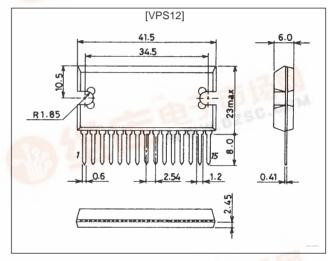
Features

- High output voltage and wide bandwidth: optimal for use in color monitors in the f_H (horizontal deflection frequency) = 90-kHz class
- $(f = 120 \text{ MHz} 3 \text{ dB at } V_{OUT} = 40 \text{ Vp-p})$
- Package: Molded 15-pin SIP package housing 3 channels in a single package

Package Dimensions

unit: mm

2127A



Specifications

Absolute Maximum Ratings at Ta = 25°C

Parameter Symbol		Conditions	Ratings	Unit	
	V _{CC} max		90	V	
Maximum supply voltage	V _{BB} max	990 VA 2 3 500	15	V	
Allowable power dissipation	Pd max	At Tc = 25°C with an ideal heat sink	25	W	
Maximum junction temperature	Tj max		150	°C	
Maximum case temperature	Tc max	COM	100	°C	
Storage temperature	Tstg		-20 to +110	°C	

Operating Conditions at Ta = 25°C

Parameter Symbol Co		Conditions	Ratings	Unit
Recommended cupply voltage	VCC		80	V
Recommended supply voltage	V _{BB}	E E	10	V

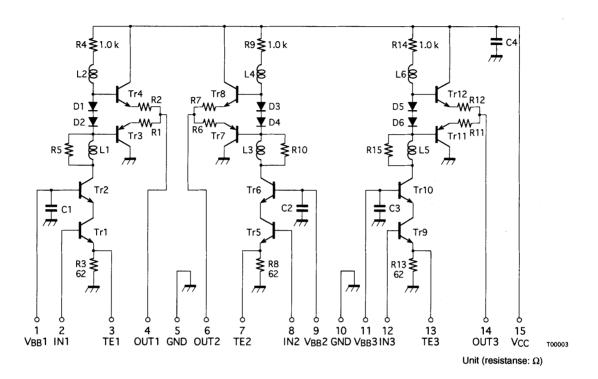
Electrical Characteristics at $Ta = 25^{\circ}C$ (for a single channel)

Parameter	Symbol	Conditions	Ratings			Unit
			min	typ	max	
Frequency band (-3 dB)	f _c	$V_{CC} = 80 \text{ V}, V_{BB} = 10 \text{ V}, C_L = 10 \text{ pF}$ $V_{IN} (DC) = 3.2 \text{ V}, V_{OUT} (p-p) = 40 \text{ V}$		120		MHz
	t _r	$V_{CC} = 80 \text{ V}, V_{BB} = 10 \text{ V}, C_{L} = 10 \text{ pF}$		4.2		ns
Pulse response	t _f	V _{IN} (DC) = 3.2 V, V _{OUT} (p-p) = 40 V		3.2		ns
Voltage gain	VG (DC)		13	15	17	Times
Current drain	I _{CC} (1)			45		mA
	I _{CC} (2)			70		mA

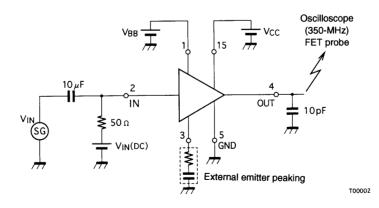
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VPS12

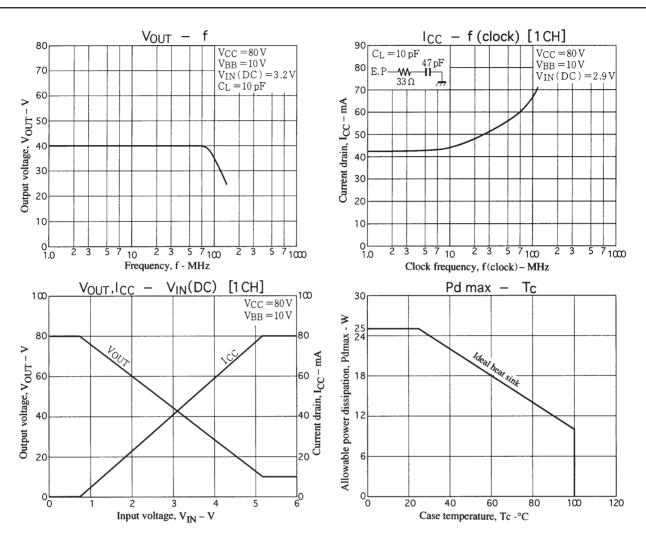
Internal Equivalent Circuit



Test Circuit (for testing a single channel)







Thermal Design

Since the VPS12 has the three-channel configuration shown in the circuit diagram on page 2, we first consider a single channel. The chip temperatures of the transistors during operation can be determined from the following formula:

 $Tj = (Tri) = \theta j-c (Tri) \times Pc (Tri) + \Delta Tc + Ta (^{\circ}C) \dots (1)$

 $\theta j\text{-}c$ (Tri): Thermal resistances of the transistor chips themselves

Pc (Tri): Collector loss of the transistors

 ΔTc : Increase in case temperature

Ta: Ambient temperature

The θj -c (Tri) for the individual transistors is:

 θj -c(Tr1) to (Tr4) = 35°C/W(2)

Although the loss in each transistor in the video pack changes with frequency and thus are not identical, assuming a maximum frequency of 120 MHz (clock), the transistor with the largest loss is Tr3 in the emitter-follower stage. From the Pd-f(clock) figure it can be seen that this loss is 22% of the total loss. Thus:

Pc (EF stage) $f = 120 \text{ MHz} = Pd (1ch) f = 120 \text{ MHz} \times 0.22 \text{ [W]} \dots (3)$

Select a θ h for the heat sink so that the junction temperature (Tj) of this transistor does not exceed 150°C. Equation (4) gives the relationship between θ h and Δ Tc.

 $\Delta Tc = Pd (TOTAL) \times \theta h \dots (4)$ The required θh can be calculated from this equation and equation (1).

VPS12 Thermal Design Example

Conditions: $f_V = 120 \text{ MHz} \text{ (clock)}$ in an $f_H = 85\text{-kHz}$ class monitor

 $V_{CC} = 80 \text{ V}, V_{BB} = 10 \text{ V}, V_{OUT} = 40 \text{ Vp-p} (C_L = 10 \text{ pF})$

Consider using this monitor at $Ta = 60^{\circ}C$ and operating it at a maximum frequency of f = 120 MHz (clock).

As was mentioned previously, the chip with the largest loss is Tr3 in the emitter-follower stage. Deriving that value from the figures below and equation (3) gives:

Pc (EF stage) = $5.8 \times 0.22 \approx 1.3$ [W].....(5)

Next, applying the value of θj -c to equation (5) shows $\Delta T j$ to be as follows:

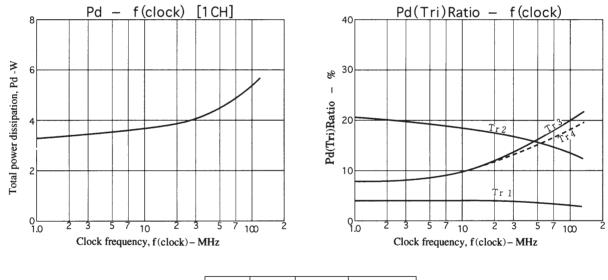
$$\Delta Tj = 1.3 \times 35 = 45.5 [^{\circ}C]$$

Here, ΔTj is less than 50°C, and in the thermal design we only have to assure that Tc is less than 100°C. That is, we must set θ h so that Tc is less than 100°C when Pd (TOTAL) = Pd (one channel) × 3.

Here, ΔTc will be $\Delta Tc = 100 - 60 = 40^{\circ}C$

Since $\theta h = \Delta Tc \div Pd$ (TOTAL) = 40 ÷ (5.8 × 3) = 2.3, then $\theta h = 2.3$ °C/W.

In an actual system, it may be possible to use a heat sink smaller than the one required for the value calculated above due to the actual ambient temperature and other operating conditions. Actual designs should be optimized to match those conditions using the data presented above.



$V_{CC}(V)$	$V_{BB}(V)$	V _{OUT} (V)	V _O (center)
80	10	40	45

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