

VOLTAGE OUTPUT, HIGH OR LOW SIDE MEASUREMENT, BIDIRECTIONAL, ZERO-DRIFT CURRENT SHUNT MONITOR

Check for Samples: [INA213-Q1](#), [INA214-Q1](#)

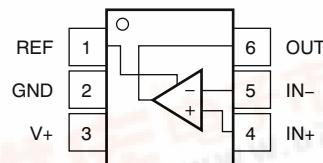
FEATURES

- Qualified for Automotive Applications
- Wide Common-Mode Range: -0.3 V to 26 V
- Offset Voltage: $\pm 100\text{ }\mu\text{V}$ (Max)
Enables Shunt Drops of 10 mV Full-Scale
- Accuracy
 - $\pm 1\%$ Gain Error (Max Over Temperature)
 - $0.5\text{ }\mu\text{V}/^\circ\text{C}$ Offset Drift (Max)
 - $10\text{ ppm}/^\circ\text{C}$ Gain Drift (Max)
- Choice of Gain
 - INA213: 50 V/V
 - INA214: 100 V/V
- Quiescent Current: $100\text{ }\mu\text{A}$ (Max)
- SC70 Package

APPLICATIONS

- Notebook Computers
- Cell Phones
- Telecom Equipment
- Power Management
- Battery Chargers
- Welding Equipment

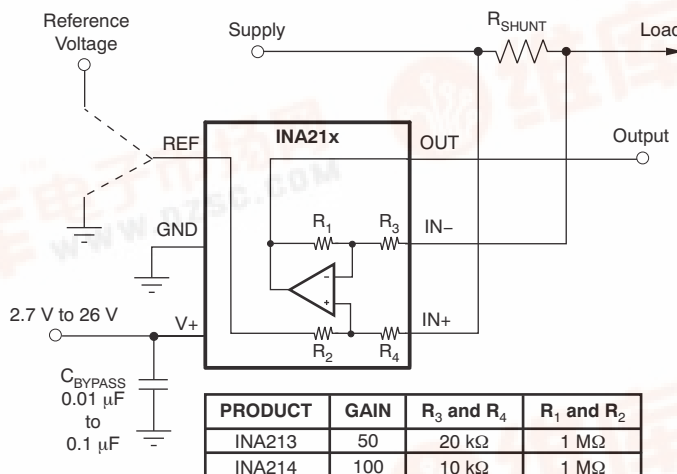
DCK PACKAGE
(TOP VIEW)



DESCRIPTION

The INA213 and INA214 are voltage-output current-shunt monitors that can sense drops across shunts at common-mode voltages from -0.3 V to 26 V , independent of the supply voltage. The INA213 offers a fixed gain of 50 V/V , and the INA214 offers a fixed gain of 100 V/V . The low offset of the zero-drift architecture enables current sensing with maximum drops across the shunt as low as 10-mV full-scale.

The devices operate from a single 2.7-V to 26-V power supply, drawing a maximum of $100\text{ }\mu\text{A}$ of supply current. They are specified over the operating temperature range of -40°C to 125°C and are offered in an SC70 package.



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

ORDERING INFORMATION⁽¹⁾

T _J	GAIN	PACKAGE ⁽²⁾		ORDERABLE PART NUMBER	TOP-SIDE MARKING
–40°C to 125°C	50 V/V	SC70 – DCK	Reel of 3000	INA213AQDCKRQ1	OBX
	100 V/V	SC70 – DCK	Reel of 3000	INA214AQDCKRQ1	OFT

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

(2) Package drawings, thermal data, and symbolization are available at www.ti.com/packaging.

ABSOLUTE MAXIMUM RATINGS⁽¹⁾

Over operating free-air temperature range, unless otherwise noted.

V _S	Supply voltage		26 V
V _{IN+} V _{IN–}	Analog inputs voltage ⁽²⁾	Differential (V _{IN+})–(V _{IN–})	–26 V to 26 V
		Common-Mode ⁽³⁾	GND – 0.3 V to 26 V
V _{REF}	REF input voltage		GND – 0.3 V to V ₊ + 0.3 V
V _{OUT}	Output voltage ⁽³⁾		GND – 0.3 V to V ₊ + 0.3 V
I _{IN}	Input current into any pin ⁽³⁾		5 mA
θ _{JA}	Thermal impedance, junction to free air		250°C/W
T _A	Operating temperature		–55°C to 150°C
T _{stg}	Storage temperature		–65°C to 150°C
T _J	Junction temperature		150°C
ESD	Electrostatic discharge rating	Human Body Model (HBM)	3000 V
		Charged-Device Model (CDM)	1000 V
		Machine Model (MM)	150 V

(1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.

(2) V_{IN+} and V_{IN–} are the voltages at the IN+ and IN– pins, respectively.

(3) Input voltage at any pin may exceed the voltage shown if the current at that pin is limited to 5 mA.

RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
V _S Supply voltage	2.7	26	V
T _J Junction temperature	–40	125	°C

ELECTRICAL CHARACTERISTICS

 $V_{SENSE} = V_{IN+} - V_{IN-}$, $V_S = +5\text{ V}$, $V_{IN+} = 12\text{ V}$, $V_{REF} = V_S/2$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS		T_A ⁽¹⁾	MIN	TYP	MAX	UNIT
V_{CM}	Common-mode input range			Full range	–0.3		26	V
CMRR	Common-mode rejection ratio	$V_{IN+} = 0\text{ V to } 26\text{ V}$, $V_{SENSE} = 0\text{ mV}$	INA213	Full range	100	120		dB
			INA214		100	140		
V_{OS}	Offset voltage	RTI ⁽²⁾ , $V_{SENSE} = 0\text{ mV}$	INA213	25°C		±5	±100	µV
			INA214			±1	±60	
dV_{OS}/dT	Offset voltage vs temperature ⁽³⁾			Full range		0.1	0.5	µV/°C
PSR	Offset voltage vs power supply	$V_S = 2.7\text{ V to } 18\text{ V}$, $V_{IN+} = 18\text{ V}$, $V_{SENSE} = 0\text{ mV}$		25°C		±0.1	±10	µV/V
I_B	Input bias current	$V_{SENSE} = 0\text{ mV}$		25°C	15	28	35	µA
I_{OS}	Input offset current	$V_{SENSE} = 0\text{ mV}$		25°C		±0.02		µA
	Gain	INA213				50		V/V
		INA214				100		
	Gain error	$V_{SENSE} = -5\text{ mV to } 5\text{ mV}$		Full range		±0.02	±1	%
	Gain error vs temperature ⁽³⁾			Full range		3	10	ppm/°C
	Nonlinearity error	$V_{SENSE} = -5\text{ mV to } 5\text{ mV}$		25°C		±0.01		%
	Maximum capacitive load	No sustained oscillation		25°C		1		nF
	Output voltage swing to V_+ power-supply rail ⁽⁴⁾	$R_L = 10\text{ k}\Omega$ to GND		Full range		$V_+ - 0.05$	$V_+ - 0.2$	V
	Output voltage swing to GND			Full range		$V_{GND} + 0.005$	$V_{GND} + 0.05$	V
BW	Bandwidth	$C_{LOAD} = 10\text{ pF}$		25°C		14		kHz
SR	Slew rate			25°C		0.4		V/µs
	Voltage noise density	RTI ⁽²⁾		25°C		25		nV/√Hz
I_Q	Quiescent current	$V_{SENSE} = 0\text{ mV}$		25°C		65	100	µA
				Full range			115	

(1) Full range $T_A = -40^\circ\text{C to } 125^\circ\text{C}$

(2) RTI = referred to input

(3) Not production tested

(4) See Typical Characteristic, *Output Voltage Swing vs Output Current* (Figure 10).

TYPICAL CHARACTERISTICS

$T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{REF} = V_S/2$ (unless otherwise noted)

**INPUT OFFSET VOLTAGE
PRODUCTION DISTRIBUTION**

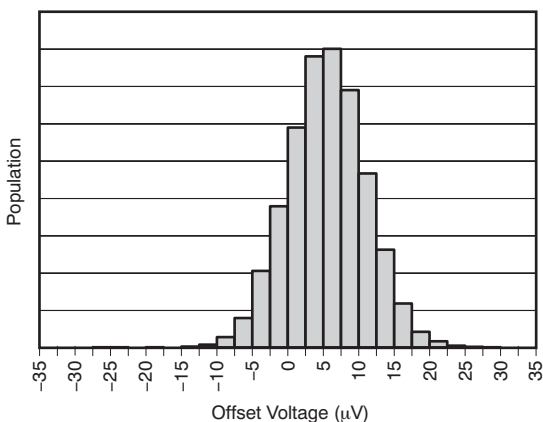


Figure 1.

**OFFSET VOLTAGE
vs TEMPERATURE**

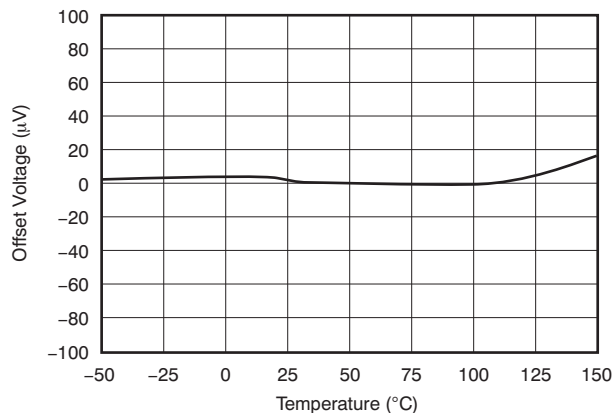


Figure 2.

**COMMON-MODE REJECTION
PRODUCTION DISTRIBUTION**

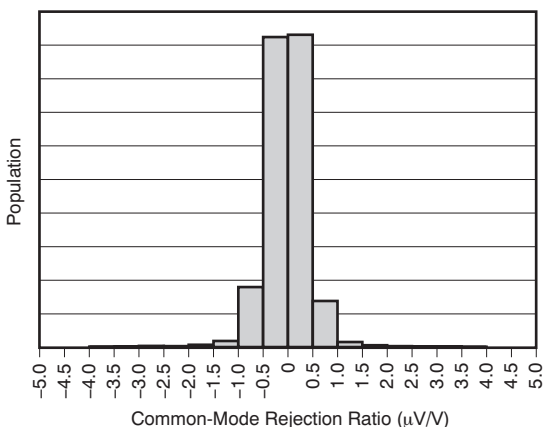


Figure 3.

**COMMON-MODE REJECTION RATIO
vs TEMPERATURE**

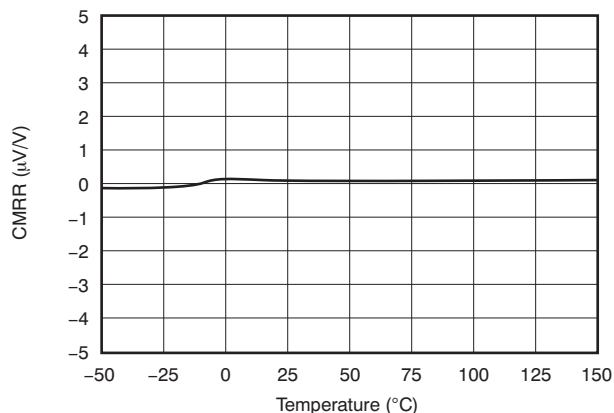


Figure 4.

TYPICAL CHARACTERISTICS (continued)

$T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{REF} = V_S/2$ (unless otherwise noted)

**GAIN ERROR
PRODUCTION DISTRIBUTION**

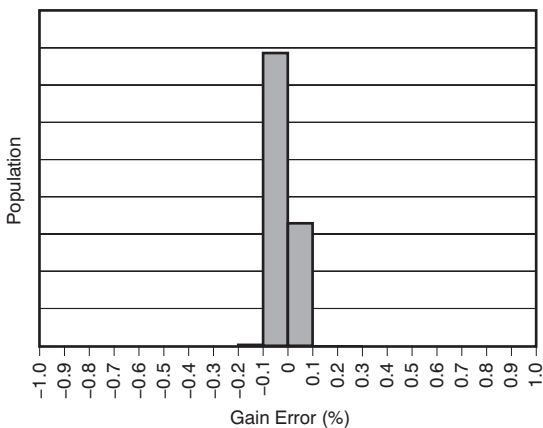


Figure 5.

**GAIN ERROR
vs TEMPERATURE**

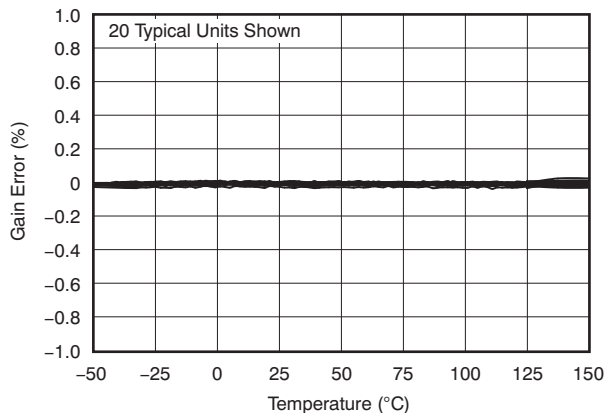


Figure 6.

**GAIN
vs FREQUENCY**

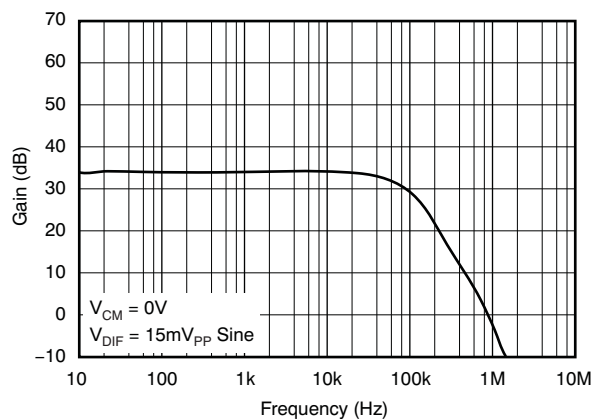


Figure 7.

**POWER-SUPPLY REJECTION RATIO
vs FREQUENCY**

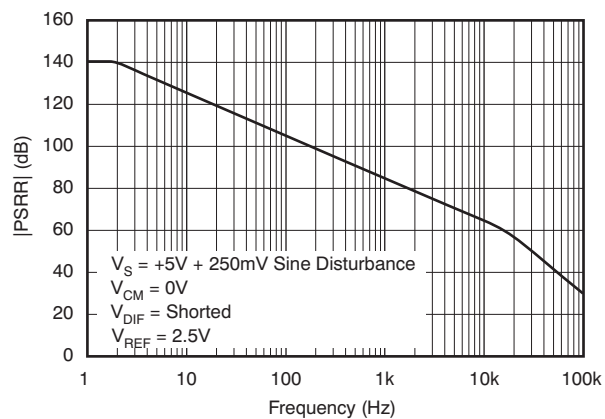


Figure 8.

TYPICAL CHARACTERISTICS (continued)

$T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{REF} = V_S/2$ (unless otherwise noted)

**COMMON-MODE REJECTION RATIO
vs FREQUENCY**

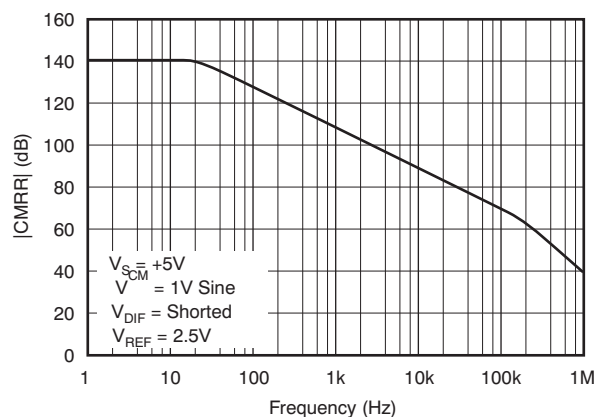


Figure 9.

**OUTPUT VOLTAGE SWING
vs OUTPUT CURRENT**

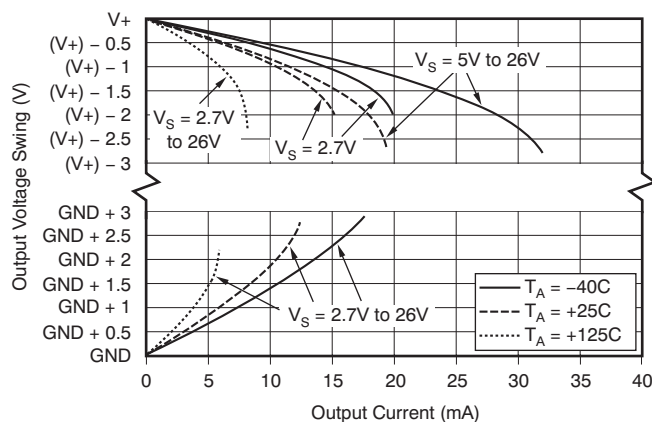


Figure 10.

**INPUT BIAS CURRENT vs COMMON-MODE VOLTAGE
with SUPPLY VOLTAGE = +5 V**

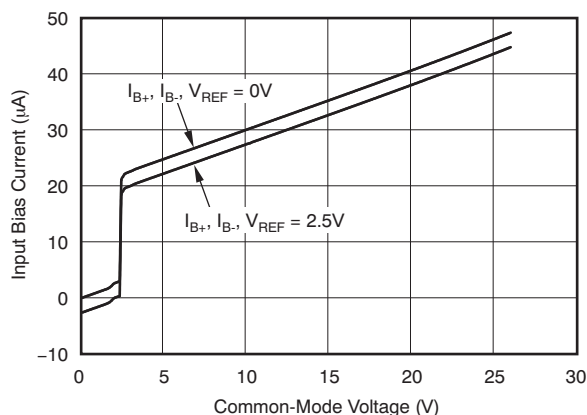


Figure 11.

**INPUT BIAS CURRENT vs COMMON-MODE VOLTAGE
with SUPPLY VOLTAGE = 0 V (Shutdown)**

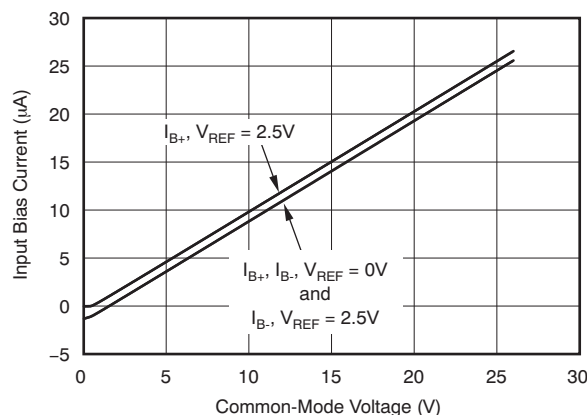


Figure 12.

**INPUT BIAS CURRENT
vs TEMPERATURE**

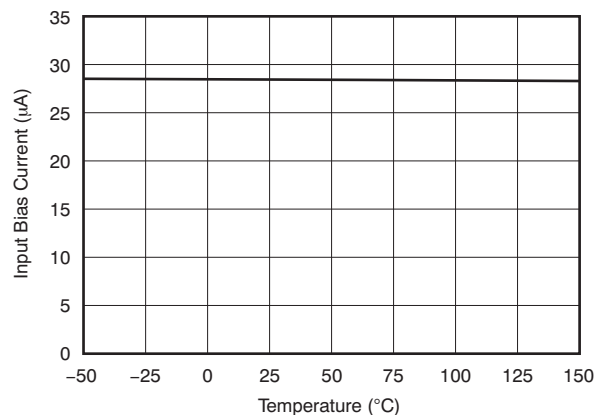


Figure 13.

**QUIESCENT CURRENT
vs TEMPERATURE**

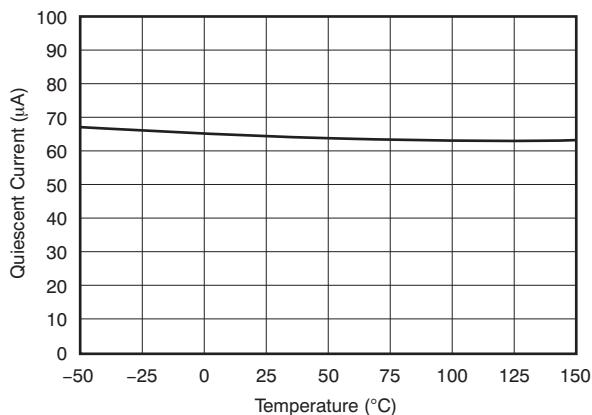


Figure 14.

TYPICAL CHARACTERISTICS (continued)

$T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{REF} = V_S/2$ (unless otherwise noted)

**INPUT-REFERRED VOLTAGE NOISE
vs FREQUENCY**

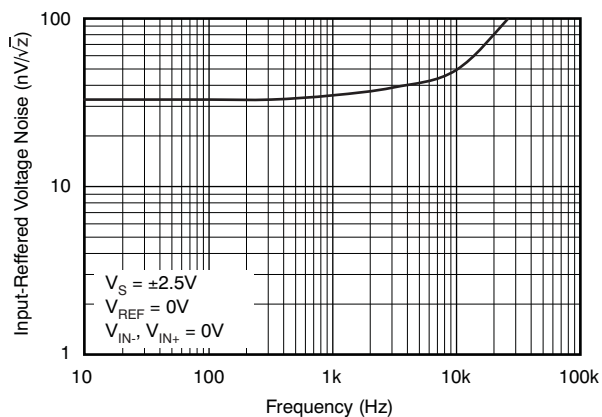


Figure 15.

**0.1 Hz to 10 Hz VOLTAGE NOISE
(Referred-to-Input)**

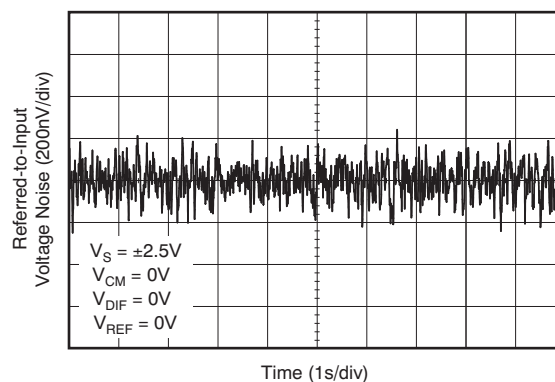


Figure 16.

**STEP RESPONSE
(10 mV_{PP} Input Step)**

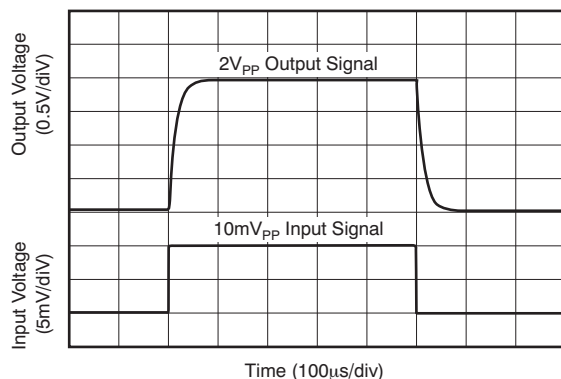


Figure 17.

**COMMON-MODE VOLTAGE
TRANSIENT RESPONSE**

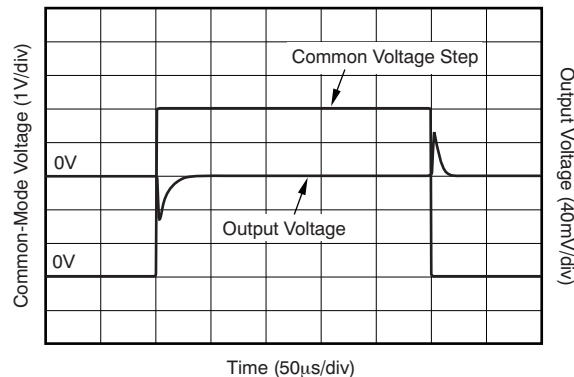


Figure 18.

INVERTING DIFFERENTIAL INPUT OVERLOAD

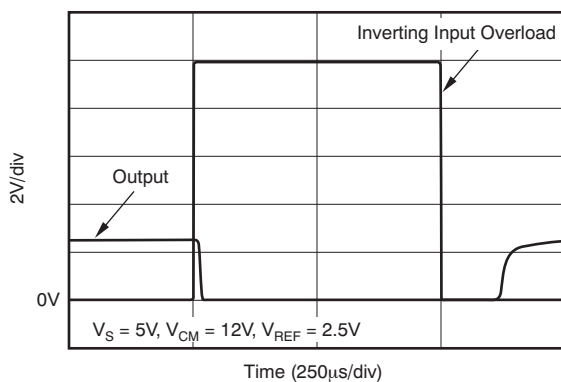


Figure 19.

NONINVERTING DIFFERENTIAL INPUT OVERLOAD

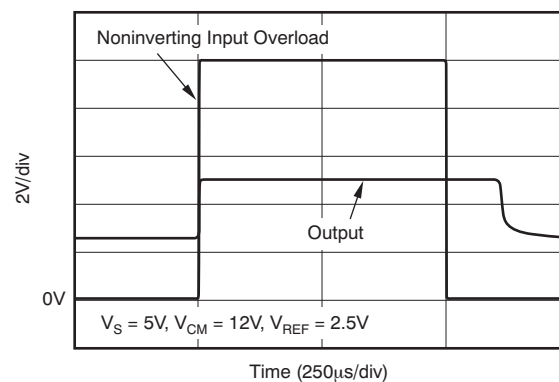


Figure 20.

TYPICAL CHARACTERISTICS (continued)

$T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{REF} = V_S/2$ (unless otherwise noted)

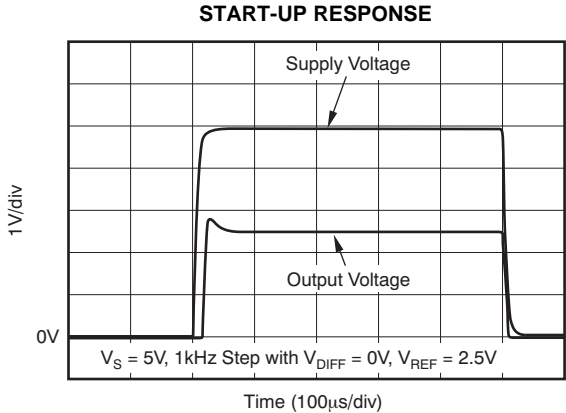


Figure 21.

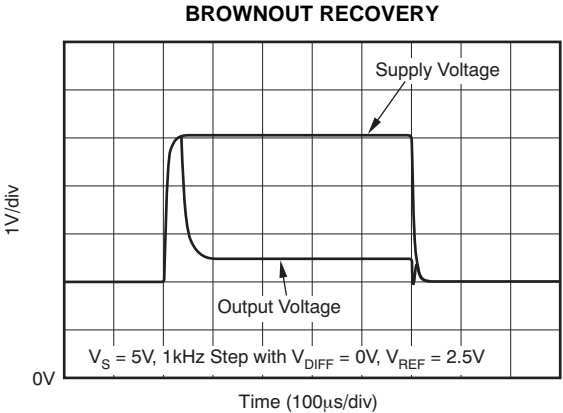


Figure 22.

APPLICATION INFORMATION

BASIC CONNECTIONS

Figure 23 shows the basic connections of the INA213 or INA214. The input pins, IN+ and IN–, should be connected as closely as possible to the shunt resistor to minimize any resistance in series with the shunt resistance.

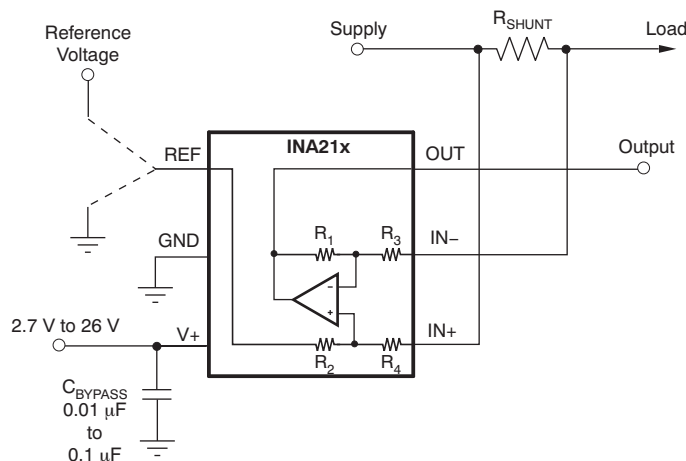


Figure 23. Typical Application

Power-supply bypass capacitors are required for stability. Applications with noisy or high impedance power supplies may require additional decoupling capacitors to reject power-supply noise. Connect bypass capacitors close to the device pins.

POWER SUPPLY

The input circuitry of the INA21x can accurately measure beyond its power-supply voltage, V+. For example, the V+ power supply can be 5 V, whereas the load power supply voltage can be as high as 26 V. However, the output voltage range of the OUT terminal is limited by the voltages on the power-supply pin. Note also that the INA21x can withstand the full –0.3 V to 26 V in the input pins, regardless of whether the device has power applied or not.

SELECTING R_S

The zero-drift offset performance of the INA21x offers several benefits. Most often, the primary advantage of the low offset characteristic enables lower full-scale drops across the shunt. For example, non-zero-drift current shunt monitors typically require a full-scale range of 100 mV.

The INA21x gives equivalent accuracy at a full-scale range on the order of 10 mV. This accuracy reduces shunt dissipation by an order of magnitude with many additional benefits.

Alternatively, there are applications that must measure current over a wide dynamic range that can take advantage of the low offset on the low end of the measurement. Most often, these applications can use the lower gain INA213 or INA214 to accommodate larger shunt drops on the upper end of the scale. For instance, an INA213 operating on a 3.3-V supply could easily handle a full-scale shunt drop of 60 mV, with only 60 μ V of offset.

UNIDIRECTIONAL OPERATION

Unidirectional operation allows the INA21x to measure currents through a resistive shunt in one direction. The most frequent case of unidirectional operation sets the output at ground by connecting the REF pin to ground. In unidirectional applications where the highest possible accuracy is desirable at very low inputs, bias the REF pin to a convenient value above 50 mV to get the device output swing into the linear range for zero inputs.

A less frequent case of unipolar output biasing is to bias the output by connecting the REF pin to the supply; in this case, the quiescent output for zero input is at quiescent supply. This configuration would only respond to negative currents (inverted voltage polarity at the device input).

BIDIRECTIONAL OPERATION

Bidirectional operation allows the INA21x to measure currents through a resistive shunt in two directions. In this case, the output can be set anywhere within the limits of what the reference inputs allow (that is, between 0 V and V+). Typically, it is set at half-scale for equal range in both directions. In some cases, however, it is set at a voltage other than half-scale when the bidirectional current is nonsymmetrical.

The quiescent output voltage is set by applying voltage to the reference input. Under zero differential input conditions the output assumes the same voltage as is applied to the reference input.

INPUT FILTERING

An obvious and straightforward location for filtering is at the output of the INA21x; however, this location negates the advantage of the low output impedance of the internal buffer. The only other option for filtering is at the input pins of the INA21x; this location requires consideration of the $\pm 30\%$ tolerance of the input impedance. [Figure 24](#) shows a filter placed at the input pins.

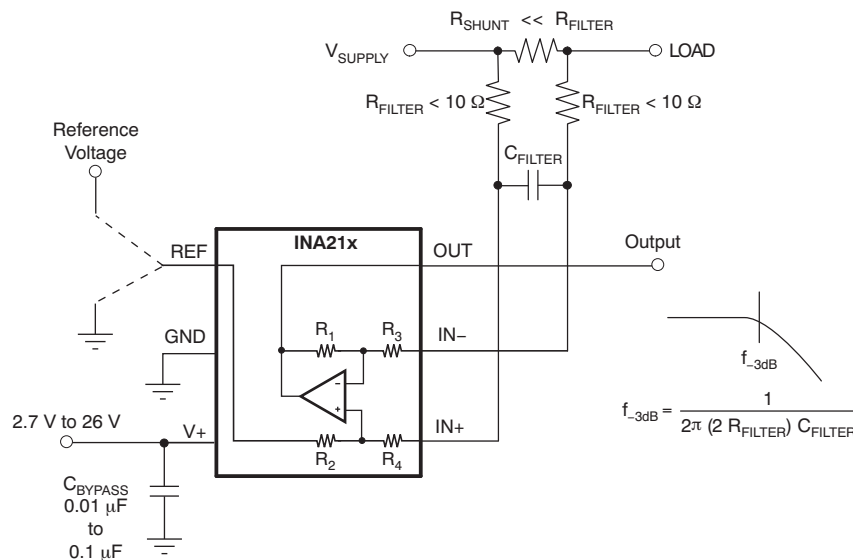


Figure 24. Input Filter

Using the lowest possible resistor values minimizes both the initial shift in gain and effects of tolerance. The effect on initial gain is given by [Equation 1](#):

$$\text{GainError\%} = 100 - [100 \times \{R/(R + R_{\text{FILT}})\}] \quad (1)$$

Where R is the value for R₃ or R₄ from [Table 1](#) for the model in question.

Table 1.

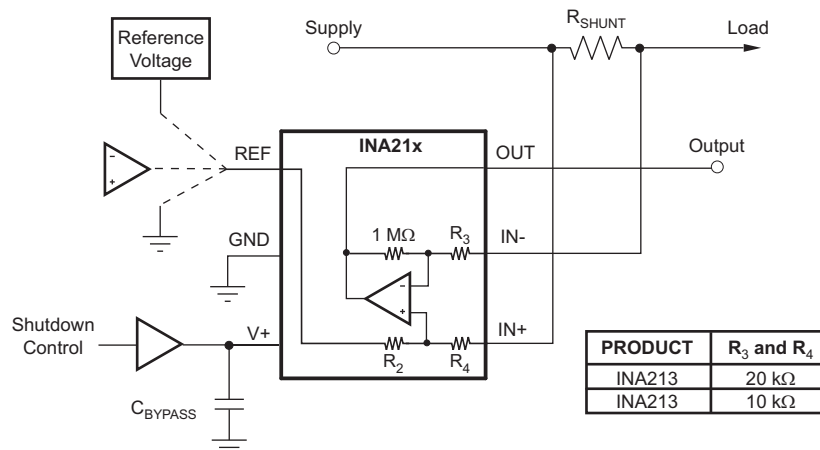
PRODUCT	GAIN (V/V)	R ₃ AND R ₄
INA213	50	20 kΩ
INA214	100	10 kΩ

Using an INA212, for example, the total effect on gain error can be calculated by replacing the R with 1 kΩ – 30%, (or 700 Ω) or 1 kΩ + 30% (or 1.3 kΩ). The tolerance extremes of R_{FILT} can also be inserted into the equation. If a pair of 100-Ω 1% resistors are used on the inputs, the initial gain error is approximately 2%.

SHUTTING DOWN

While the INA21x does not have a shutdown pin, its low power consumption allows powering from the output of a logic gate or transistor switch that can turn on and turn off the INA21x power-supply quiescent current.

However, in current shunt monitoring applications, there is also a concern for how much current is drained from the shunt circuit in shutdown conditions. Evaluating this current drain involves considering the simplified schematic of the INA21x in shutdown mode shown in Figure 25.



NOTE: 1-MΩ paths from shunt inputs to reference and INA21x outputs.

Figure 25. Basic Circuit for Shutting Down INA21x With Grounded Reference

Note that there is typically slightly more than 1-MΩ impedance (from the combination of 1-MΩ feedback and 5-kΩ input resistors) from each input of the INA21x to the OUT pin and to the REF pin. The amount of current flowing through these pins depends on the respective ultimate connection. For example, if the REF pin is grounded, the calculation of the effect of the 1-MΩ impedance from the shunt to ground is straightforward. However, if the reference or op amp is powered while the INA21x is shut down, the calculation is direct; instead of assuming 1 MΩ to ground, however, assume 1 MΩ to the reference voltage. If the reference or op amp is also shut down, some knowledge of the reference or op amp output impedance under shutdown conditions is required. For instance, if the reference source behaves as an open circuit when it is unpowered, little or no current flows through the 1-MΩ path.

Regarding the 1-MΩ path to the output pin, the output stage of a disabled INA21x does constitute a good path to ground; consequently, this current is directly proportional to a shunt common-mode voltage impressed across a 1-MΩ resistor.

As a final note, when the device is powered up, there is an additional, nearly constant, and well-matched 25 μA that flows in each of the inputs as long as the shunt common-mode voltage is 3 V or higher. Below 2-V common-mode, the only current effects are the result of the 1-MΩ resistors.

REF INPUT IMPEDANCE EFFECTS

As with any difference amplifier, the INA21x common-mode rejection ratio is affected by any impedance present at the REF input. This concern is not a problem when the REF pin is connected directly to most references or power supplies. When using resistive dividers from the power supply or a reference voltage, the REF pin should be buffered by an op amp.

In systems where the INA21x output can be sensed differentially, such as by a differential input analog-to-digital converter (ADC) or by using two separate ADC inputs, the effects of external impedance on the REF input can be cancelled. Figure 26 depicts a method of taking the output from the INA21x by using the REF pin as a reference.

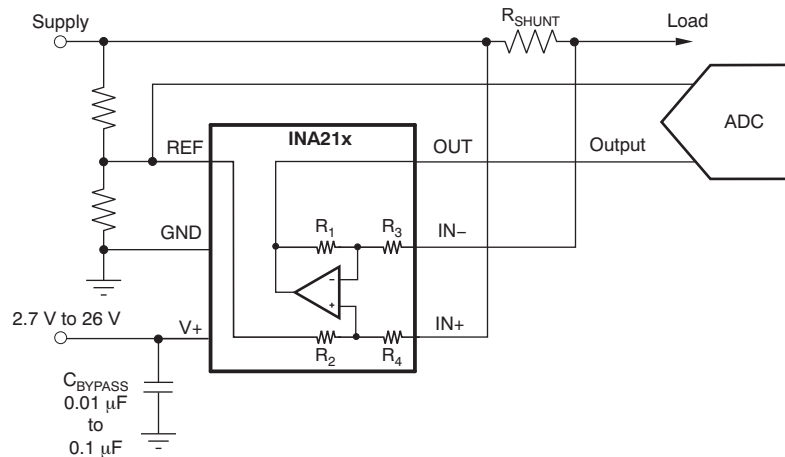


Figure 26. Sensing INA21x to Cancel Effects of Impedance on the REF Input

USING THE INA21x WITH COMMON-MODE TRANSIENTS ABOVE 26 V

With a small amount of additional circuitry, the INA21x can be used in circuits subject to transients higher than 26 V, such as automotive applications. Use only zener diode or zener-type transient absorbers (sometimes referred to as *Transzorbs*) — any other type of transient absorber has an unacceptable time delay. Start by adding a pair of resistors as shown in Figure 27 as a working impedance for the zener. It is desirable to keep these resistors as small as possible, most often around 10 Ω. Larger values can be used with an effect on gain that is discussed in the section on input filtering. Because this circuit is limiting only short-term transients, many applications are satisfied with a 10-Ω resistor along with conventional zener diodes of the lowest power rating that can be found. This combination uses the least amount of board space. These diodes can be found in packages as small as SOT-523 or SOD-523.

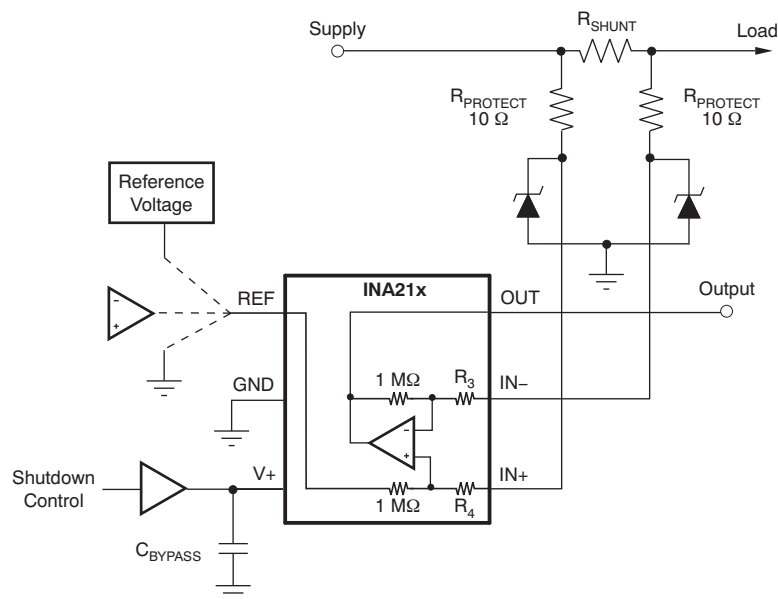


Figure 27. INA21x Transient Protection Using Dual Zener Diodes

If low-power zener diodes do not have sufficient transient absorption capability and a higher power transzorb must be used, the most package-efficient solution then involves using a single transzorb and back-to-back diodes between the device inputs. The most space-efficient solutions are dual series-connected diodes in a single SOT-523 or SOD-523 package. This method is shown in Figure 28. In either of these examples, the total board area required by the INA21x with all protective components is less than that of an SO-8 package, and only slightly greater than that of an MSOP-8 package.

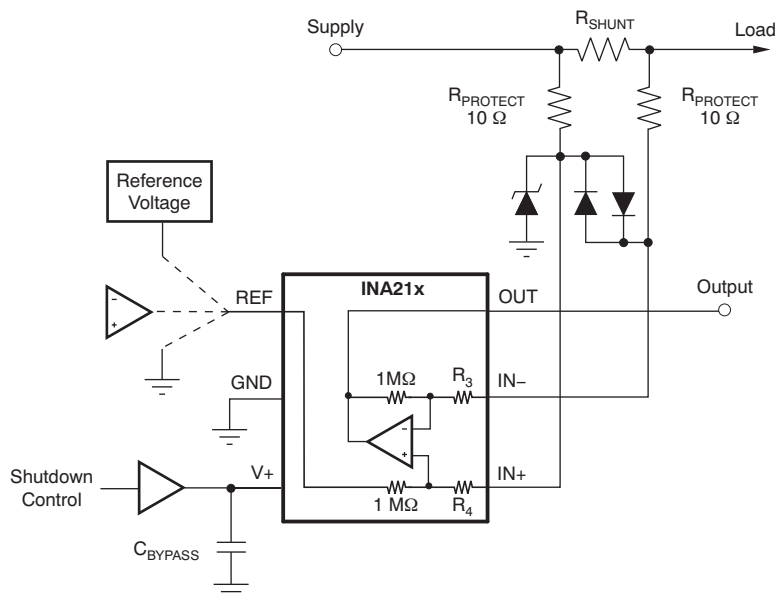


Figure 28. Transient Protection Using a Single Transzorb and Input Clamps



PACKAGING INFORMATION

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins	Package Qty	Eco Plan ⁽²⁾	Lead/ Ball Finish	MSL Peak
INA213AQDCKRQ1	ACTIVE	SC70	DCK	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-2600
INA214AQDCKRQ1	ACTIVE	SC70	DCK	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-2600

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBsolete: TI has discontinued the production of the device.

⁽²⁾ Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com> for more information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for high temperature applications.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die attach material used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (as required by UL recognition) in homogeneous material.

⁽³⁾ MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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OTHER QUALIFIED VERSIONS OF INA214-Q1 :

- Catalog: [INA214](#)

NOTE: Qualified Version Definitions:

[查询"INA213A-Q1"供应商](#)



PACKAG

-
- Catalog - TI's standard catalog product

TAPE AND REEL INFORMATION



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
INA214AQDCKRQ1	SC70	DCK	6	3000	180.0	8.4	2.25	2.4	1.22	4.0	8.0	Q3

TAPE AND REEL BOX DIMENSIONS

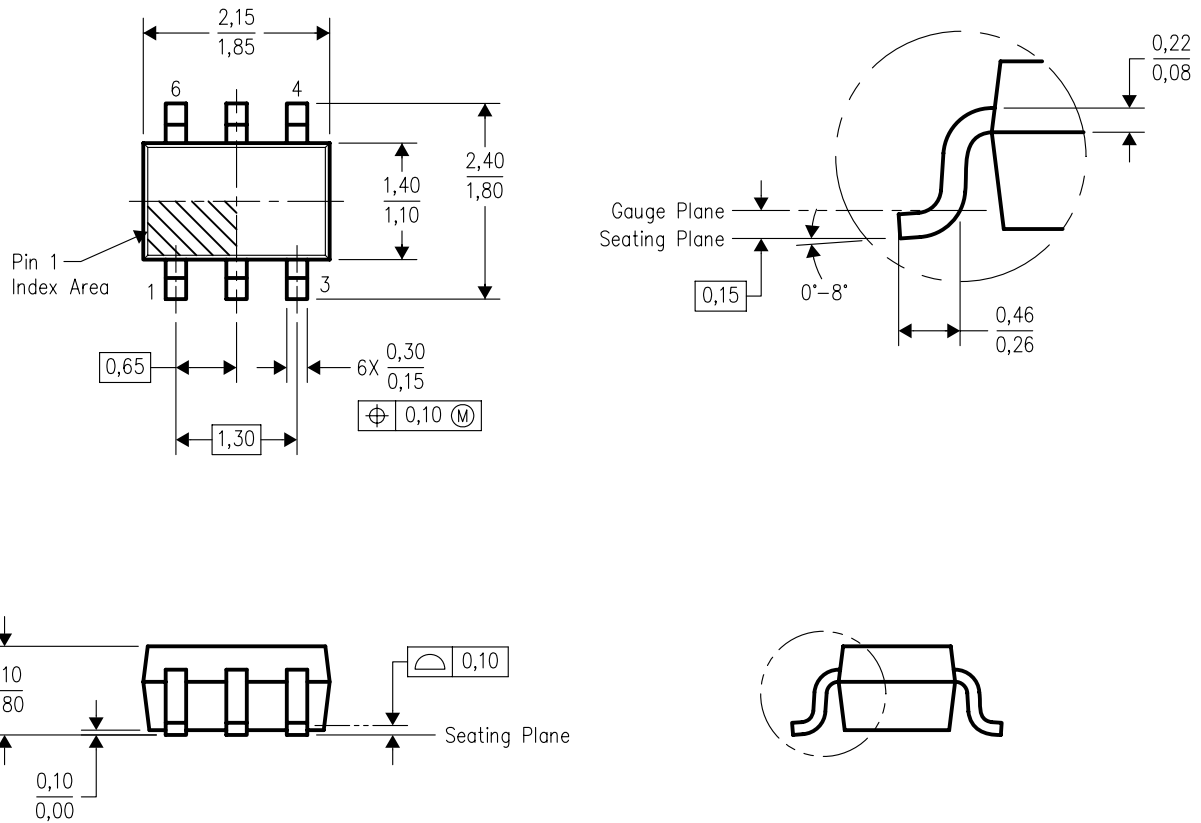


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
INA214AQDCKRQ1	SC70	DCK	6	3000	202.0	201.0	28.0

DCK (R-PDSO-G6)

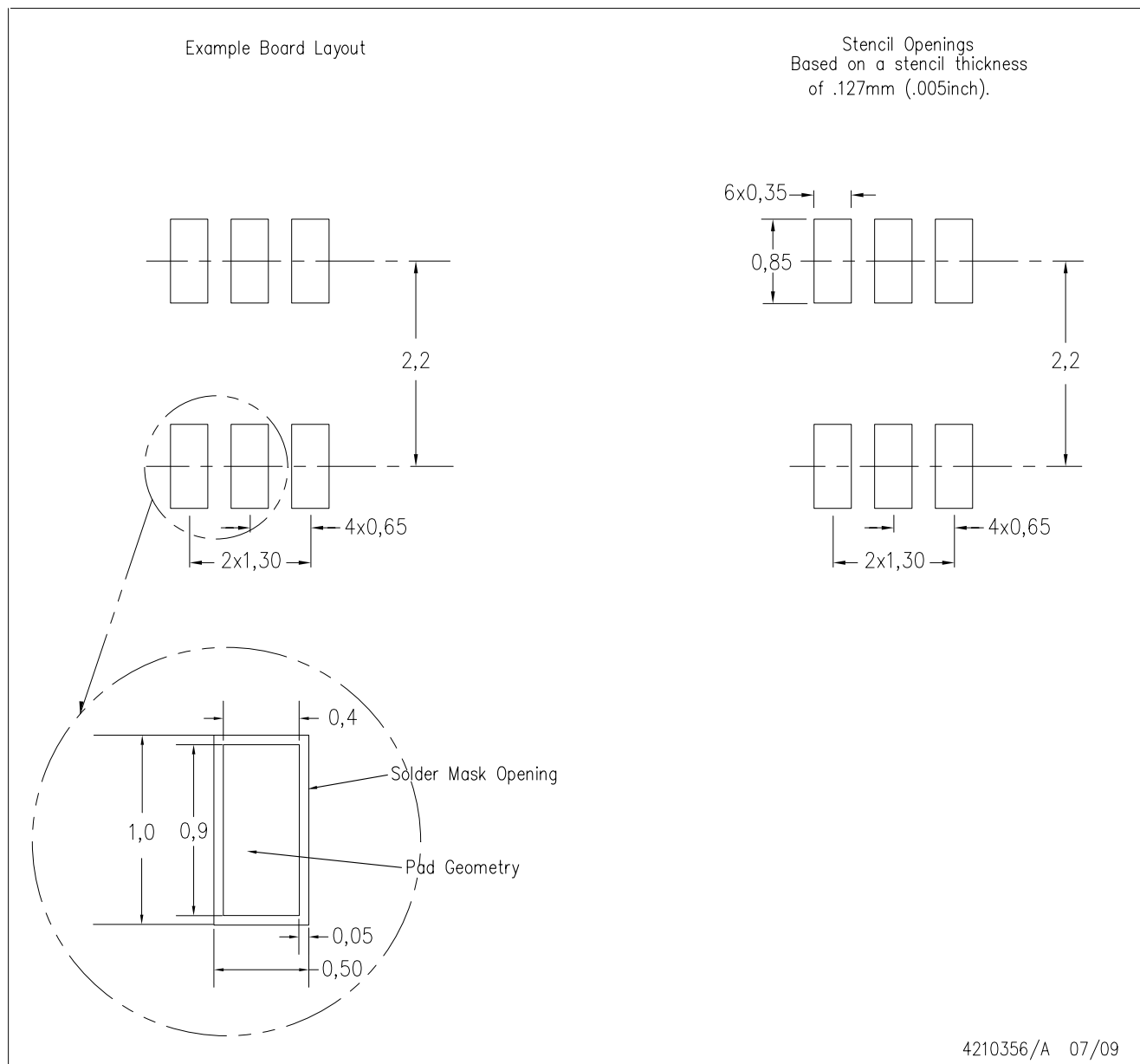
PLASTIC SMALL-OUTLINE PACKAGE



4093553-4/G 01/2007

- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
 - D. Falls within JEDEC MO-203 variation AB.

DCK (R-PDSO-G6)



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
 - Publication IPC-7351 is recommended for alternate designs.
 - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

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