

FEATURES

- Wide input range beyond supplies
- Rugged input overvoltage protection
- Low supply current: 200 μA maximum
- Low power dissipation: 0.5 mW at $V_S = 2.5\text{ V}$
- Bandwidth: 1 MHz ($G = \frac{1}{2}$)
- CMRR: 80 dB minimum, dc to 20 kHz ($G = \frac{1}{2}$)
- Low offset voltage drift: $\pm 2\ \mu\text{V}/^\circ\text{C}$ maximum (B Grade)
- Low gain drift: 1 ppm/ $^\circ\text{C}$ maximum (B Grade)
- Enhanced slew rate: 1.4 V/ μs
- Wide power supply range:
 - Single supply: 2 V to 36 V
 - Dual supplies: $\pm 2\text{ V}$ to $\pm 18\text{ V}$
- 8-lead SOIC and MSOP packages

APPLICATIONS

- Voltage measurement and monitoring
- Current measurement and monitoring
- Instrumentation amplifier building block
- Portable, battery-powered equipment
- Test and measurement

GENERAL DESCRIPTION

The AD8278 is a general-purpose difference amplifier intended for precision signal conditioning in power critical applications that require both high performance and low power. The AD8278 provides exceptional common-mode rejection ratio (80 dB) and high bandwidth while amplifying signals well beyond the supply rails. The on-chip resistors are laser-trimmed for excellent gain accuracy and high CMRR. They also have extremely low gain drift vs. temperature.

The common-mode range of the amplifier extends to almost triple the supply voltage (for $G = \frac{1}{2}$), making it ideal for single-supply applications that require a high common-mode voltage range. The internal resistors and ESD circuitry at the inputs also provide overvoltage protection to the op amp.

FUNCTIONAL BLOCK DIAGRAM

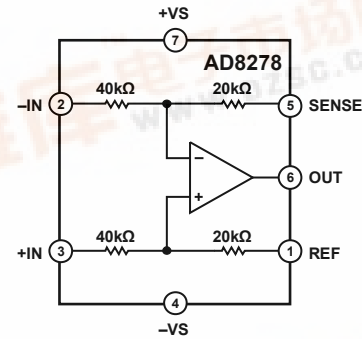


Figure 1.

Table 1. Difference Amplifiers by Category

Low Distortion	High Voltage	Current Sensing ¹	Low Power
AD8270	AD628	AD8202 (U)	AD8276
AD8271	AD629	AD8203 (U)	AD8277
AD8273		AD8205 (B)	
AD8274		AD8206 (B)	
AMP03		AD8216 (B)	

¹ U = unidirectional, B = bidirectional.

The AD8278 can be used as a difference amplifier with $G = \frac{1}{2}$ or $G = 2$. It can also be connected in a high precision, single-ended configuration for non-inverting and inverting gains of $-\frac{1}{2}$, -2 , $+3$, $+2$, $+1\frac{1}{2}$, $+1$, or $+\frac{1}{2}$. The AD8278 provides an integrated precision solution that has a smaller size, lower cost, and better performance than a discrete alternative.

The AD8278 operates on single supplies (2.0 V to 36 V) or dual supplies ($\pm 2\text{ V}$ to $\pm 18\text{ V}$). The maximum quiescent supply current is 200 μA , which makes it ideal for battery-operated and portable systems.

The AD8278 is available in the space-saving 8-lead MSOP and SOIC packages. It is specified for performance over the industrial temperature range of -40°C to $+85^\circ\text{C}$ and is fully RoHS compliant.

Rev. 0

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REVISION HISTORY

7/09—Revision 0: Initial Version

SPECIFICATIONS

$V_S = \pm 5\text{ V}$ to $\pm 15\text{ V}$, $V_{REF} = 0\text{ V}$, $T_A = 25^\circ\text{C}$, $R_L = 10\text{ k}\Omega$ connected to ground, $G = \frac{1}{2}$ difference amplifier configuration, unless otherwise noted.

Table 2.

Parameter	Conditions	G = 1/2						Unit
		Grade B			Grade A			
		Min	Typ	Max	Min	Typ	Max	
INPUT CHARACTERISTICS								
System Offset ¹	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		50	100		50	250	μV
vs. Temperature					100			250
Average Temperature Coefficient	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		0.3	1		2	5	$\mu\text{V}/^\circ\text{C}$
vs. Power Supply	$V_S = \pm 5\text{ V}$ to $\pm 18\text{ V}$			2.5			5	$\mu\text{V}/\text{V}$
Common-Mode Rejection Ratio (RTI)	$V_S = \pm 15\text{ V}$, $V_{CM} = \pm 27\text{ V}$, $R_S = 0\ \Omega$	80			74			dB
Input Voltage Range ²		$-3(V_S + 0.1)$		$+3(V_S - 1.5)$	$-3(V_S + 0.1)$		$+3(V_S - 1.5)$	V
Impedance ³								
Differential			120			120		k Ω
Common Mode			30			30		k Ω
DYNAMIC PERFORMANCE								
Bandwidth			1			1		MHz
Slew Rate		1.1	1.4		1.1	1.4		V/ μs
Settling Time to 0.01%	10 V step on output, $C_L = 100\text{ pF}$			9			9	μs
Settling Time to 0.001%				10			10	μs
GAIN								
Gain Error			0.005	0.02		0.01	0.05	%
Gain Drift	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			1			5	ppm/ $^\circ\text{C}$
Gain Nonlinearity	$V_{OUT} = 20\text{ V p-p}$			5			10	ppm
OUTPUT CHARACTERISTICS								
Output Voltage Swing ⁴	$V_S = \pm 15\text{ V}$, $R_L = 10\text{ k}\Omega$, $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$	$-V_S + 0.2$		$+V_S - 0.2$	$-V_S + 0.2$		$+V_S - 0.2$	V
Short-Circuit Current Limit			± 15			± 15		mA
Capacitive Load Drive			200			200		pF
NOISE ⁵								
Output Voltage Noise	$f = 0.1\text{ Hz}$ to 10 Hz		1.4			1.4		$\mu\text{V p-p}$
	$f = 1\text{ kHz}$		47	50		47	50	$\text{nV}/\sqrt{\text{Hz}}$
POWER SUPPLY								
Supply Current ⁶				200			200	μA
vs. Temperature	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			250			250	μA
Operating Voltage Range ⁷		± 2		± 18	± 2		± 18	V
TEMPERATURE RANGE								
Operating Range		-40		$+125$	-40		$+125$	$^\circ\text{C}$

¹ Includes input bias and offset current errors, RTO (referred to output)

² The input voltage range may also be limited by absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation for details.

³ Internal resistors are trimmed to be ratio matched and have $\pm 20\%$ absolute accuracy.

⁴ Output voltage swing varies with supply voltage and temperature. See Figure 20 through Figure 23 for details.

⁵ Includes amplifier voltage and current noise, as well as noise from internal resistors.

⁶ Supply current varies with supply voltage and temperature. See Figure 24 and Figure 26 for details.

⁷ Unbalanced dual supplies can be used, such as $-V_S = -0.5\text{ V}$ and $+V_S = +2\text{ V}$. The positive supply rail must be at least 2 V above the negative supply and reference voltage.

$V_S = \pm 5\text{ V}$ to $\pm 15\text{ V}$, $V_{REF} = 0\text{ V}$, $T_A = 25^\circ\text{C}$, $R_L = 10\text{ k}\Omega$ connected to ground, $G = 2$ difference amplifier configuration, unless otherwise noted.

Table 3.

Parameter	Conditions	G = 2						Unit
		Grade B			Grade A			
		Min	Typ	Max	Min	Typ	Max	
INPUT CHARACTERISTICS								
System Offset ¹	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		100	200		100	500	μV
vs. Temperature					200			500
Average Temperature Coefficient	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		0.6	2		2	5	$\mu\text{V}/^\circ\text{C}$
vs. Power Supply	$V_S = \pm 5\text{ V}$ to $\pm 18\text{ V}$			5			10	$\mu\text{V}/\text{V}$
Common-Mode Rejection Ratio (RTI)	$V_S = \pm 15\text{ V}$, $V_{CM} = \pm 27\text{ V}$, $R_S = 0\ \Omega$	86			80			dB
Input Voltage Range ²		$-1.5(V_S + 0.1)$		$+1.5(V_S - 1.5)$	$-1.5(V_S + 0.1)$		$+1.5(V_S - 1.5)$	V
Impedance ³								
Differential			120			120		k Ω
Common Mode			30			30		k Ω
DYNAMIC PERFORMANCE								
Bandwidth	10 V step on output, $C_L = 100\text{ pF}$		550			550		kHz
Slew Rate		1.1	1.4		1.1	1.4		V/ μs
Settling Time to 0.01%				10			10	μs
Settling Time to 0.001%				11			11	μs
GAIN								
Gain Error	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		0.005	0.02		0.01	0.05	%
Gain Drift					1			5
Gain Nonlinearity	$V_{OUT} = 20\text{ V p-p}$			5			10	ppm
OUTPUT CHARACTERISTICS								
Output Voltage Swing ⁴	$V_S = \pm 15\text{ V}$, $R_L = 10\text{ k}\Omega$, $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$	$-V_S + 0.2$		$+V_S - 0.2$	$-V_S + 0.2$		$+V_S - 0.2$	V
Short-Circuit Current Limit			± 15			± 15		mA
Capacitive Load Drive			350			350		pF
NOISE ⁵								
Output Voltage Noise	$f = 0.1\text{ Hz}$ to 10 Hz $f = 1\text{ kHz}$		2.8			2.8		$\mu\text{V p-p}$
			90	95		90	95	nV/ $\sqrt{\text{Hz}}$
POWER SUPPLY								
Supply Current ⁶	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			200			200	μA
vs. Temperature					250			250
Operating Voltage Range ⁷		± 2		± 18	± 2		± 18	V
TEMPERATURE RANGE								
Operating Range		-40		+125	-40		+125	$^\circ\text{C}$

¹ Includes input bias and offset current errors, RTO (referred to output).

² The input voltage range may also be limited by absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation for details.

³ Internal resistors are trimmed to be ratio matched and have $\pm 20\%$ absolute accuracy.

⁴ Output voltage swing varies with supply voltage and temperature. See Figure 20 through Figure 23 for details.

⁵ Includes amplifier voltage and current noise, as well as noise from internal resistors.

⁶ Supply current varies with supply voltage and temperature. See Figure 24 and Figure 26 for details.

⁷ Unbalanced dual supplies can be used, such as $-V_S = -0.5\text{ V}$ and $+V_S = +2\text{ V}$. The positive supply rail must be at least 2 V above the negative supply and reference voltage.

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$V_S = +2.7\text{ V}$ to $<\pm 5\text{ V}$, $V_{REF} = \text{midsupply}$, $T_A = 25^\circ\text{C}$, $R_L = 10\text{ k}\Omega$ connected to midsupply, $G = \frac{1}{2}$ difference amplifier configuration, unless otherwise noted.

Table 4.

Parameter	Conditions	G = 1/2						Unit
		Grade B			Grade A			
		Min	Typ	Max	Min	Typ	Max	
INPUT CHARACTERISTICS								
System Offset ¹	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		75	150		75	250	μV
vs. Temperature					150			250
Average Temperature Coefficient	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		0.3	1		2	5	$\mu\text{V}/^\circ\text{C}$
vs. Power Supply	$V_S = \pm 5\text{ V}$ to $\pm 18\text{ V}$			2.5			5	$\mu\text{V}/\text{V}$
Common-Mode Rejection Ratio (RTI)	$V_S = 2.7\text{ V}$, $V_{CM} = 0\text{ V}$ to 2.4 V , $R_S = 0\ \Omega$	80			74			dB
	$V_S = \pm 5\text{ V}$, $V_{CM} = -10\text{ V}$ to $+7\text{ V}$, $R_S = 0\ \Omega$	80			74			dB
Input Voltage Range ²		$-3(V_S + 0.1)$		$+3(V_S - 1.5)$	$-3(V_S + 0.1)$		$+3(V_S - 1.5)$	V
Impedance ³								
Differential			120			120		k Ω
Common Mode			30			30		k Ω
DYNAMIC PERFORMANCE								
Bandwidth			870			870		kHz
Slew Rate			1.3			1.3		V/ μs
Settling Time to 0.01%	2 V step on output, $C_L = 100\text{ pF}$, $V_S = 2.7\text{ V}$		7			7		μs
GAIN								
Gain Error			0.005	0.02		0.01	0.05	%
Gain Drift	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			1			5	ppm/ $^\circ\text{C}$
OUTPUT CHARACTERISTICS								
Output Swing ⁴	$R_L = 10\text{ k}\Omega$, $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$	$-V_S + 0.1$		$+V_S - 0.15$	$-V_S + 0.1$		$+V_S - 0.15$	V
Short-Circuit Current Limit			± 10			± 10		mA
Capacitive Load Drive			200			200		pF
NOISE ⁵								
Output Voltage Noise	$f = 0.1\text{ Hz}$ to 10 Hz		1.4			1.4		$\mu\text{V p-p}$
	$f = 1\text{ kHz}$		47	50		47	50	nV/ $\sqrt{\text{Hz}}$
POWER SUPPLY								
Supply Current ⁶	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			200			200	μA
Operating Voltage Range		2.0		36	2.0		36	V
TEMPERATURE RANGE								
Operating Range		-40		$+125$	-40		$+125$	$^\circ\text{C}$

¹ Includes input bias and offset current errors, RTO (referred to output).

² The input voltage range may also be limited by absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation section for details.

³ Internal resistors are trimmed to be ratio matched and have $\pm 20\%$ absolute accuracy.

⁴ Output voltage swing varies with supply voltage and temperature. See Figure 20 through Figure 23 for details.

⁵ Includes amplifier voltage and current noise, as well as noise from internal resistors.

⁶ Supply current varies with supply voltage and temperature. See Figure 25 and Figure 26 for details.

$V_S = +2.7\text{ V}$ to $\pm 5\text{ V}$, $V_{REF} = \text{midsupply}$, $T_A = 25^\circ\text{C}$, $R_L = 10\text{ k}\Omega$ connected to midsupply, $G = 2$ difference amplifier configuration, unless otherwise noted.

Table 5.

Parameter	Conditions	G = 2						Unit
		Grade B			Grade A			
		Min	Typ	Max	Min	Typ	Max	
INPUT CHARACTERISTICS								
System Offset ¹	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		150	300		150	500	μV
vs. Temperature					300			500
Average Temperature Coefficient	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$		0.6	2		3	5	$\mu\text{V}/^\circ\text{C}$
vs. Power Supply	$V_S = \pm 5\text{ V}$ to $\pm 18\text{ V}$			5			10	$\mu\text{V}/\text{V}$
Common-Mode Rejection Ratio (RTI)	$V_S = 2.7\text{ V}$, $V_{CM} = 0\text{ V}$ to 2.4 V , $R_S = 0\ \Omega$	86			80			dB
	$V_S = \pm 5\text{ V}$, $V_{CM} = -10\text{ V}$ to $+7\text{ V}$, $R_S = 0\ \Omega$	86			80			dB
Input Voltage Range ²		$-1.5(V_S + 0.1)$		$+1.5(V_S - 1.5)$	$-1.5(V_S + 0.1)$		$+1.5(V_S - 1.5)$	V
Impedance ³								
Differential			120			120		k Ω
Common Mode			30			30		k Ω
DYNAMIC PERFORMANCE								
Bandwidth			450			450		kHz
Slew Rate			1.3			1.3		V/ μs
Settling Time to 0.01%	2 V step on output, $C_L = 100\text{ pF}$, $V_S = 2.7\text{ V}$		9			9		μs
GAIN								
Gain Error			0.005	0.02		0.01	0.05	%
Gain Drift	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			1			5	ppm/ $^\circ\text{C}$
OUTPUT CHARACTERISTICS								
Output Swing ⁴	$R_L = 10\text{ k}\Omega$, $T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$	$-V_S + 0.1$		$+V_S - 0.15$	$-V_S + 0.1$		$+V_S - 0.15$	V
Short-Circuit Current Limit			± 10			± 10		mA
Capacitive Load Drive			200			200		pF
NOISE ⁵								
Output Voltage Noise	$f = 0.1\text{ Hz}$ to 10 Hz		2.8			2.8		$\mu\text{V p-p}$
	$f = 1\text{ kHz}$		94	100		94	100	nV/ $\sqrt{\text{Hz}}$
POWER SUPPLY								
Supply Current ⁶	$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			200			220	μA
Operating Voltage Range		2.0		36	2.0		36	V
TEMPERATURE RANGE								
Operating Range		-40		$+125$	-40		$+125$	$^\circ\text{C}$

¹ Includes input bias and offset current errors, RTO (referred to output).

² The input voltage range may also be limited by absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation section for details.

³ Internal resistors are trimmed to be ratio matched and have $\pm 20\%$ absolute accuracy.

⁴ Output voltage swing varies with supply voltage and temperature. See Figure 20 through Figure 23 for details.

⁵ Includes amplifier voltage and current noise, as well as noise from internal resistors.

⁶ Supply current varies with supply voltage and temperature. See Figure 25 and Figure 26 for details.

ABSOLUTE MAXIMUM RATINGS

Table 6.

Parameter	Rating
Supply Voltage	± 18 V
Maximum Voltage at Any Input Pin	$-V_S + 40$ V
Minimum Voltage at Any Input Pin	$+V_S - 40$ V
Storage Temperature Range	-65°C to $+150^\circ\text{C}$
Specified Temperature Range	-40°C to $+85^\circ\text{C}$
Package Glass Transition Temperature (T_G)	150°C

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

THERMAL RESISTANCE

The θ_{JA} values in Table 7 assume a 4-layer JEDEC standard board with zero airflow.

Table 7. Thermal Resistance

Package Type	θ_{JA}	Unit
8-Lead MSOP	135	$^\circ\text{C}/\text{W}$
8-Lead SOIC	121	$^\circ\text{C}/\text{W}$

MAXIMUM POWER DISSIPATION

The maximum safe power dissipation for the AD8278 is limited by the associated rise in junction temperature (T_J) on the die. At approximately 150°C , which is the glass transition temperature, the properties of the plastic change. Even temporarily exceeding this temperature limit may change the stresses that the package exerts on the die, permanently shifting the parametric performance of the amplifiers. Exceeding a temperature of 150°C for an extended period may result in a loss of functionality.

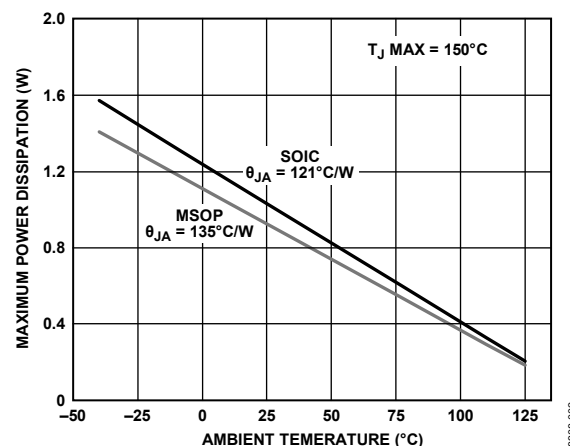


Figure 2. Maximum Power Dissipation vs. Ambient Temperature

SHORT-CIRCUIT CURRENT

The AD8278 has built-in, short-circuit protection that limits the output current (see Figure 27 for more information). While the short-circuit condition itself does not damage the part, the heat generated by the condition can cause the part to exceed its maximum junction temperature, with corresponding negative effects on reliability. Figure 2 and Figure 27, combined with knowledge of the supply voltages and ambient temperature of the part can be used to determine whether a short circuit will cause the part to exceed its maximum junction temperature.

ESD CAUTION



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

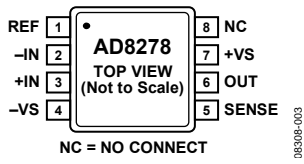


Figure 3. MSOP Pin Configuration

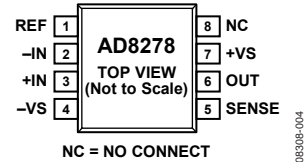


Figure 4. SOIC Pin Configuration

Table 8. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	REF	Reference Voltage Input.
2	-IN	Inverting Input.
3	+IN	Noninverting Input.
4	-VS	Negative Supply.
5	SENSE	Sense Terminal.
6	OUT	Output.
7	+VS	Positive Supply.
8	NC	No Connect.

TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15\text{ V}$, $T_A = 25^\circ\text{C}$, $R_L = 10\text{ k}\Omega$ connected to ground, $G = \frac{1}{2}$ difference amplifier configuration, unless otherwise noted.

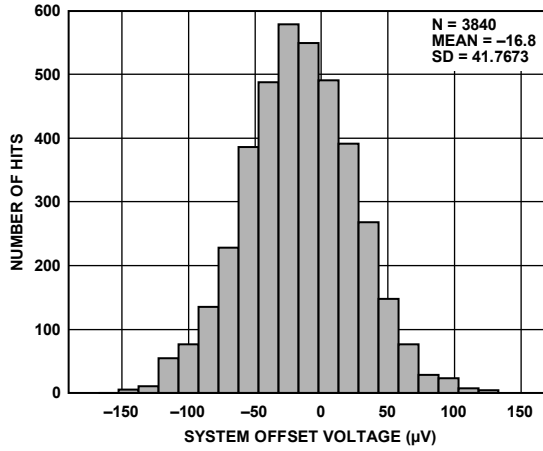


Figure 5. Distribution of Typical System Offset Voltage, $G = 2$

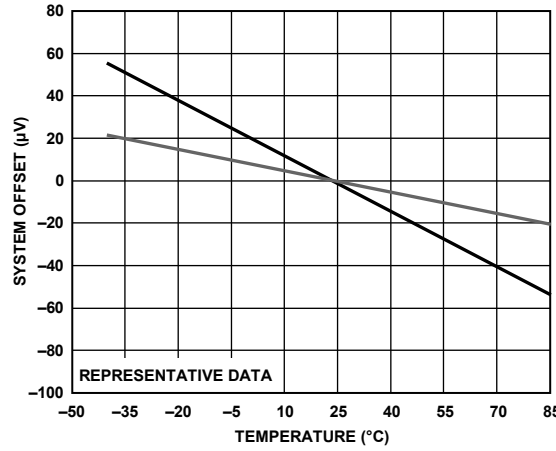


Figure 8. System Offset vs. Temperature, Normalized at 25°C , $G = \frac{1}{2}$

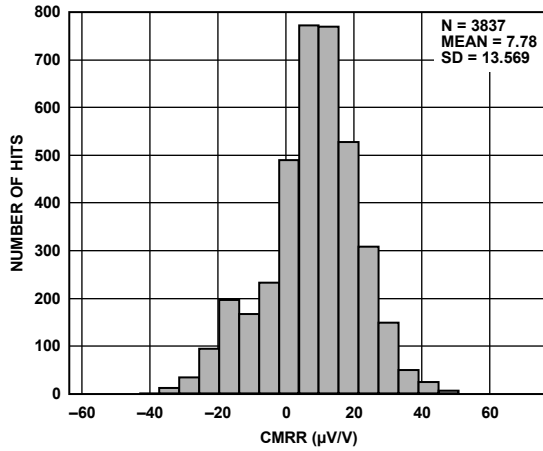


Figure 6. Distribution of Typical Common-Mode Rejection, $G = 2$

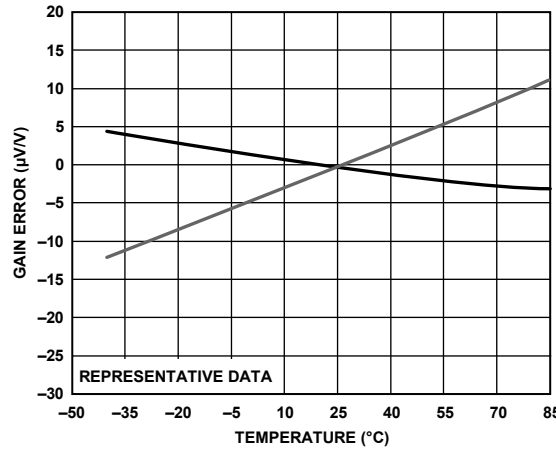


Figure 9. Gain Error vs. Temperature, Normalized at 25°C , $G = \frac{1}{2}$

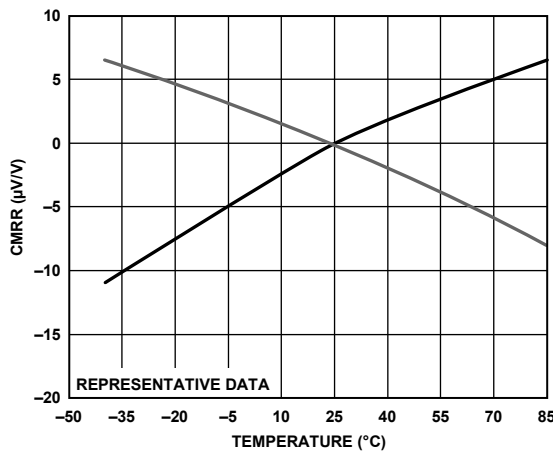


Figure 7. CMRR vs. Temperature, Normalized at 25°C , $G = \frac{1}{2}$

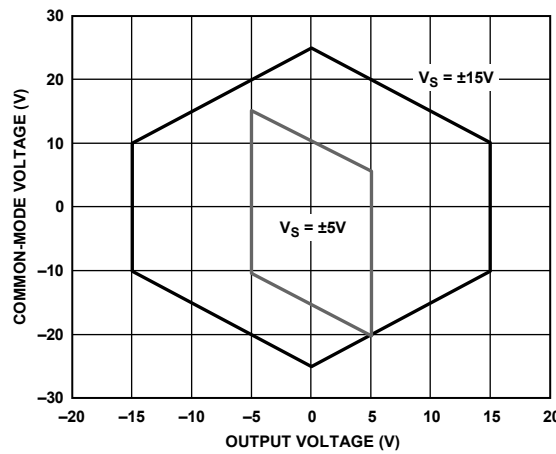


Figure 10. Input Common-Mode Voltage vs. Output Voltage, $\pm 15\text{ V}$ and $\pm 5\text{ V}$ Supplies, $G = \frac{1}{2}$

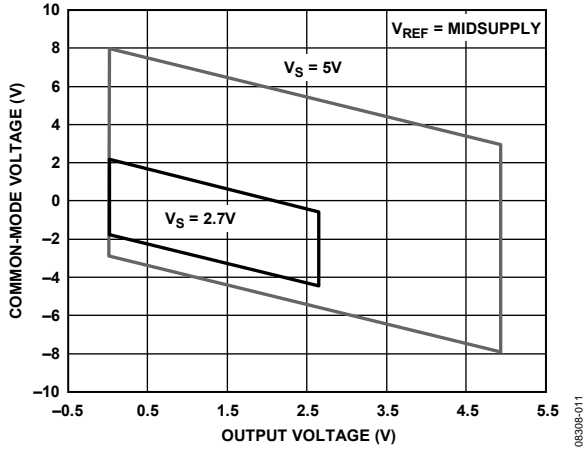


Figure 11. Input Common-Mode Voltage vs. Output Voltage, 5 V and 2.7 V Supplies, $V_{REF} = \text{Midsupply}$, $G = \frac{1}{2}$

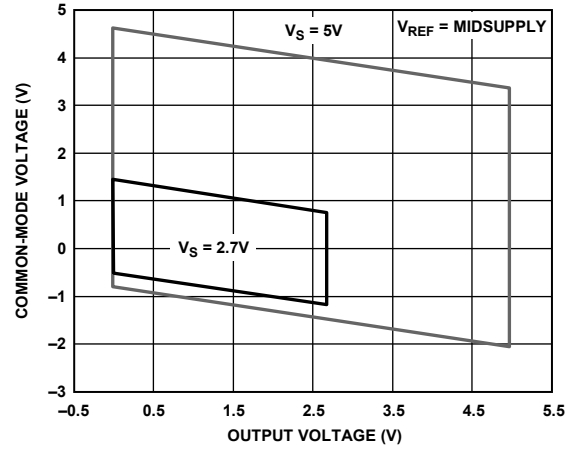


Figure 14. Input Common-Mode Voltage vs. Output Voltage, 5 V and 2.7 V Supplies, $V_{REF} = \text{Midsupply}$, $G = 2$

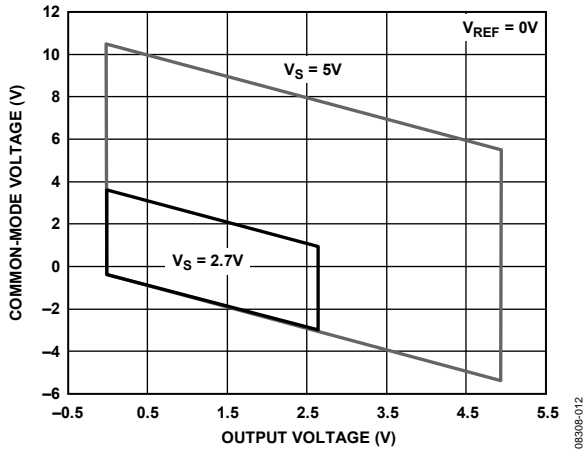


Figure 12. Input Common-Mode Voltage vs. Output Voltage, 5 V and 2.7 V Supplies, $V_{REF} = 0V$, $G = \frac{1}{2}$

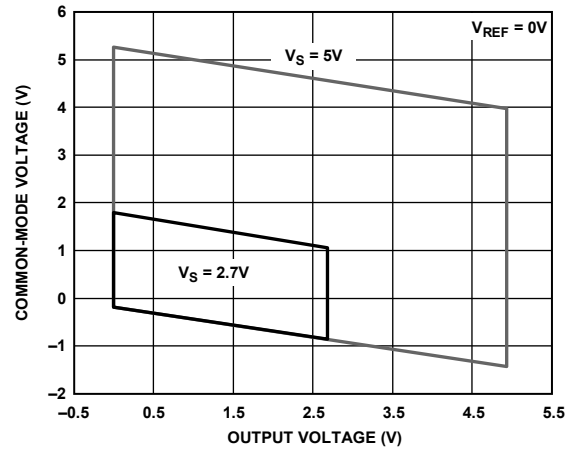


Figure 15. Input Common-Mode Voltage vs. Output Voltage, 5 V and 2.7 V Supplies, $V_{REF} = 0V$, $G = 2$

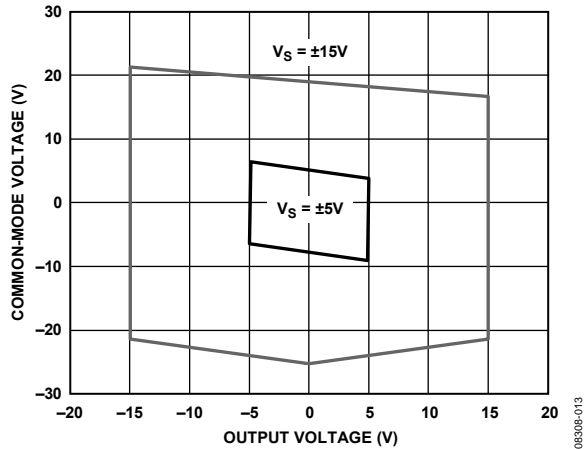


Figure 13. Input Common-Mode Voltage vs. Output Voltage, $\pm 15V$ and $\pm 5V$ Supplies, $G = 2$

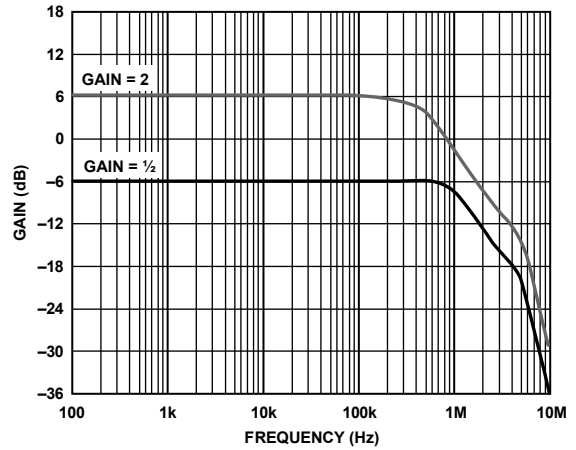


Figure 16. Gain vs. Frequency, $\pm 15V$ Supplies

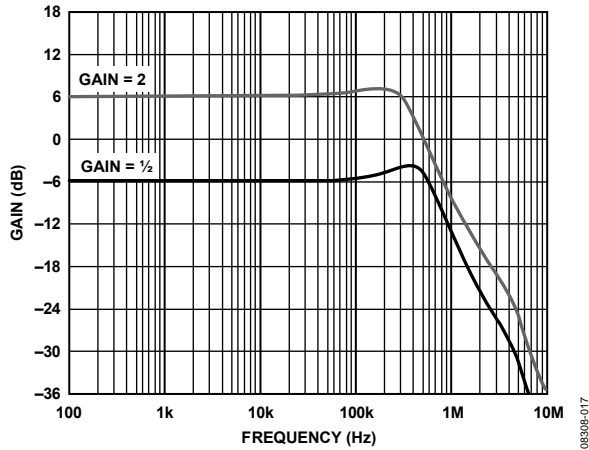


Figure 17. Gain vs. Frequency, +2.7 V Single Supply

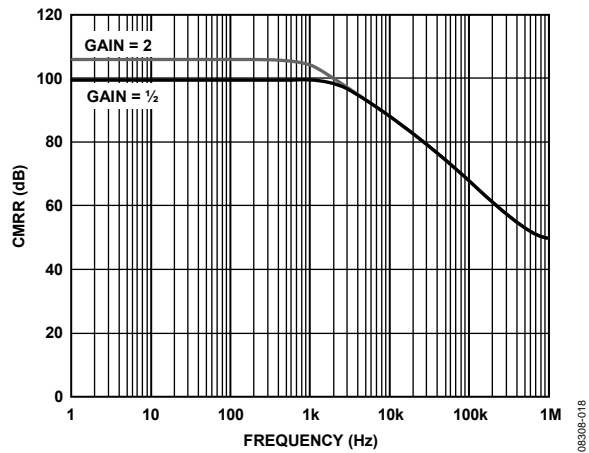


Figure 18. CMRR vs. Frequency

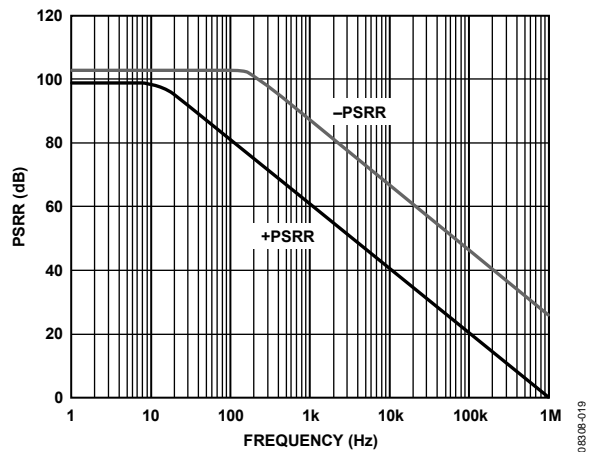


Figure 19. PSRR vs. Frequency

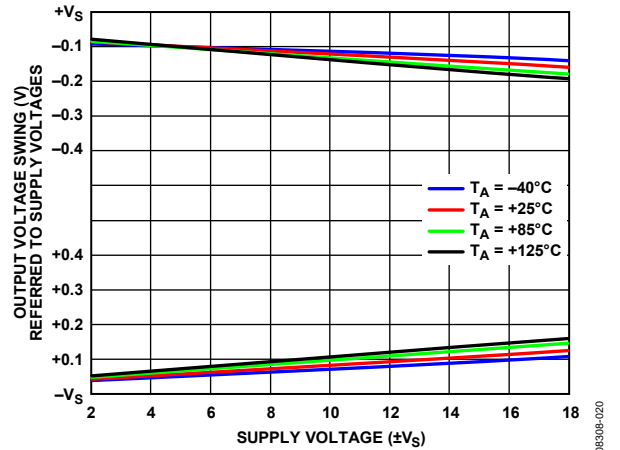


Figure 20. Output Voltage Swing vs. Supply Voltage and Temperature, $R_L = 10\text{ k}\Omega$

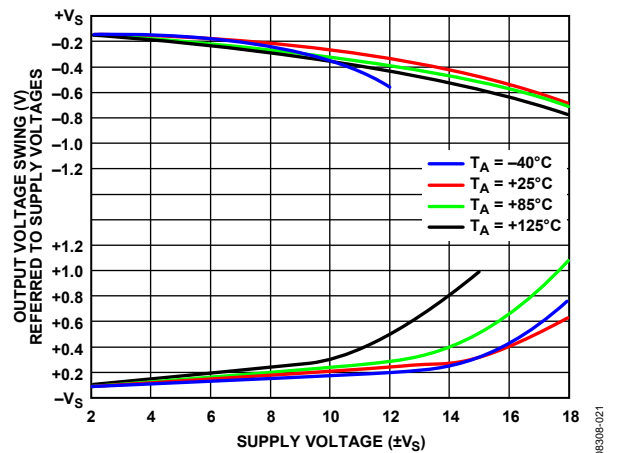


Figure 21. Output Voltage Swing vs. Supply Voltage and Temperature, $R_L = 2\text{ k}\Omega$

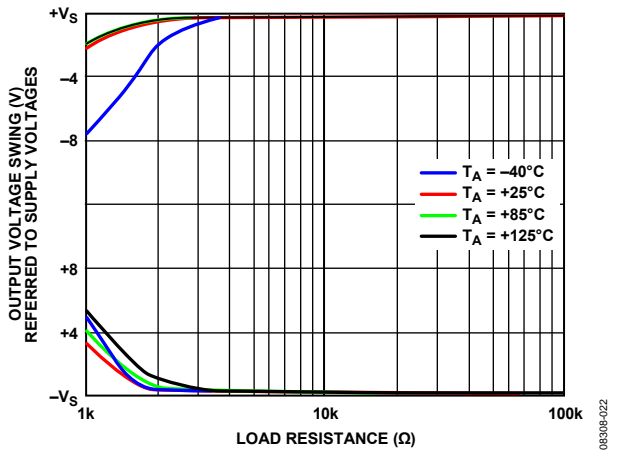


Figure 22. Output Voltage Swing vs. R_L and Temperature, $V_S = \pm 15\text{ V}$

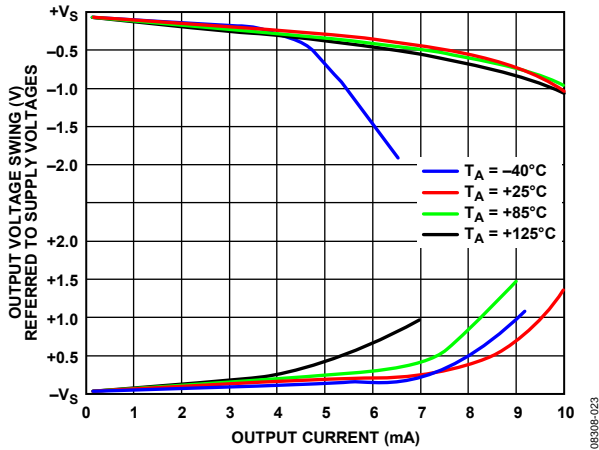


Figure 23. Output Voltage Swing vs. I_{OUT} and Temperature, $V_S = \pm 15\text{ V}$

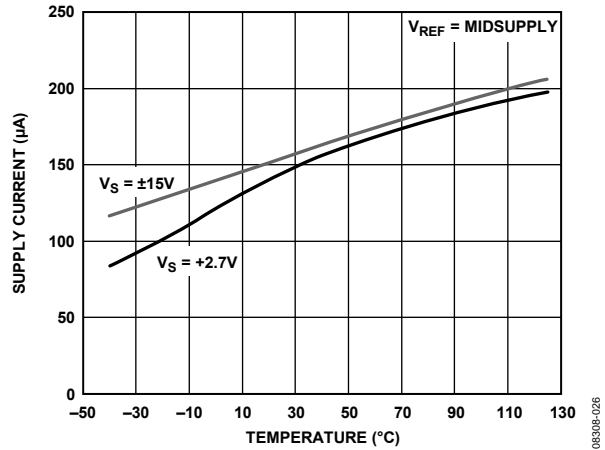


Figure 26. Supply Current vs. Temperature

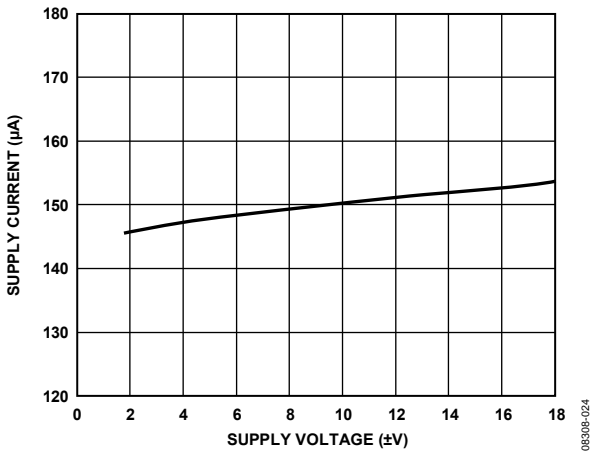


Figure 24. Supply Current vs. Dual-Supply Voltage, $V_{IN} = 0\text{ V}$

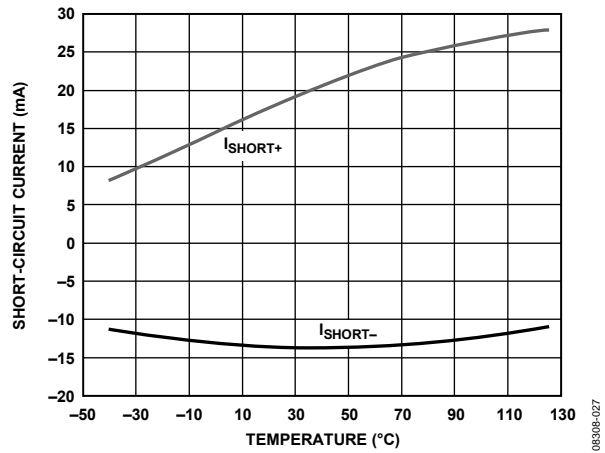


Figure 27. Short-Circuit Current vs. Temperature

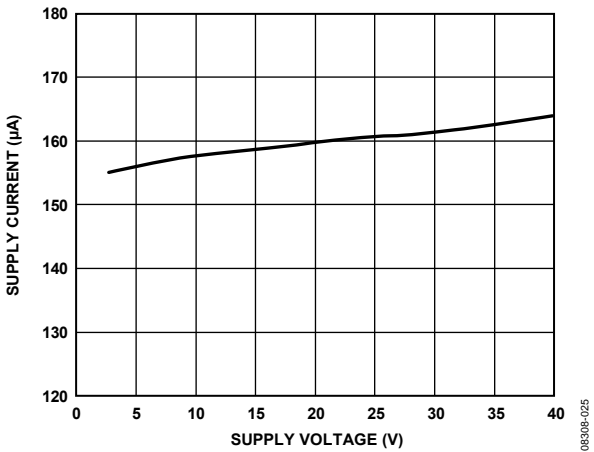


Figure 25. Supply Current vs. Single-Supply Voltage, $V_{IN} = 0\text{ V}$, $V_{REF} = 0\text{ V}$

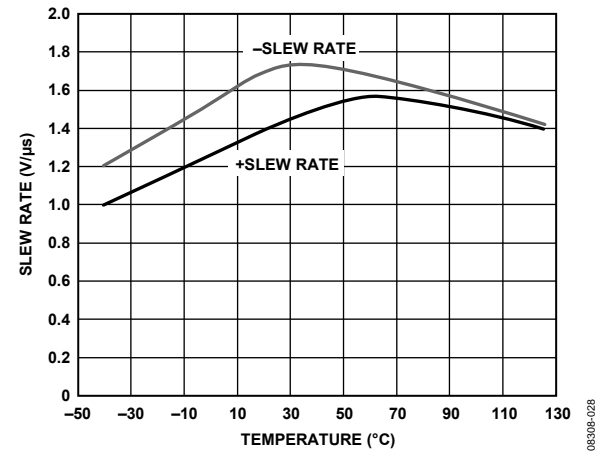


Figure 28. Slew Rate vs. Temperature, $V_{IN} = 20\text{ V p-p}$, 1 kHz

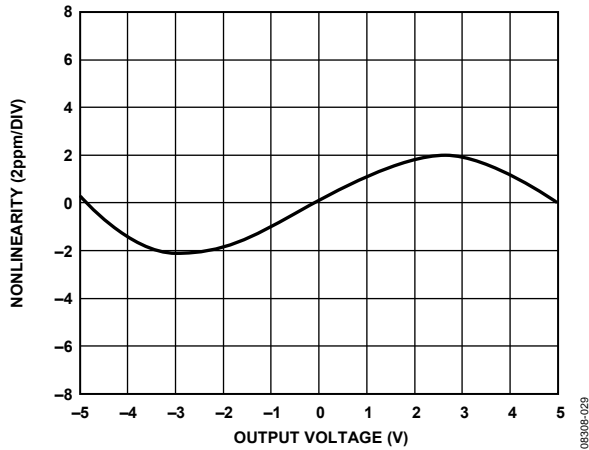


Figure 29. Gain Nonlinearity, $V_S = \pm 15\text{ V}$, $R_L \geq 2\text{ k}\Omega$, $G = \frac{1}{2}$

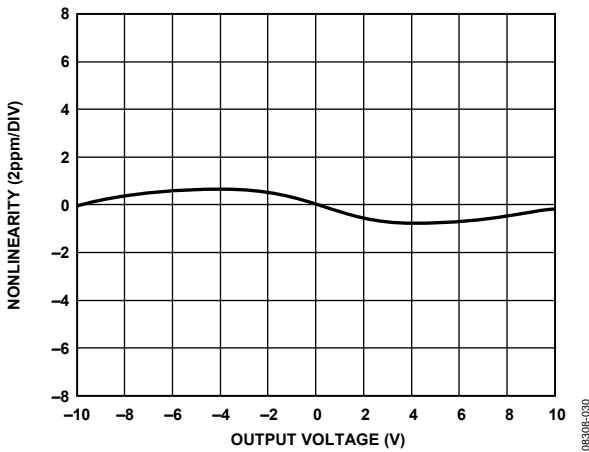


Figure 30. Gain Nonlinearity, $V_S = \pm 15\text{ V}$, $R_L \geq 2\text{ k}\Omega$, $G = 2$

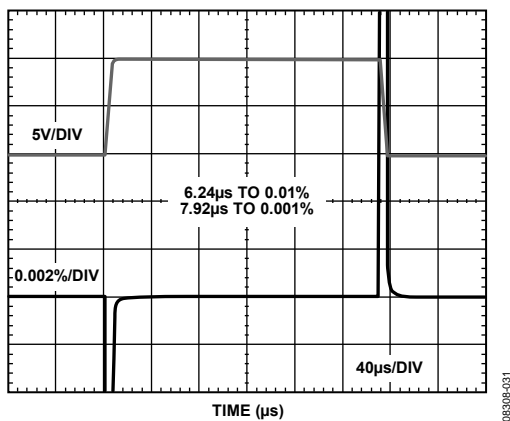


Figure 31. Large-Signal Pulse Response and Settling Time, 10 V Step, $V_S = \pm 15\text{ V}$, $G = \frac{1}{2}$

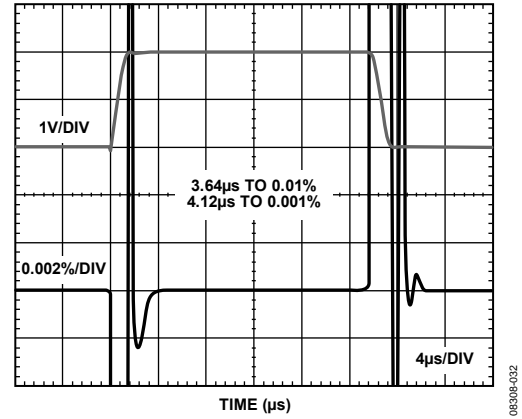


Figure 32. Large-Signal Pulse Response and Settling Time, 2 V Step, $V_S = 2.7\text{ V}$, $G = \frac{1}{2}$

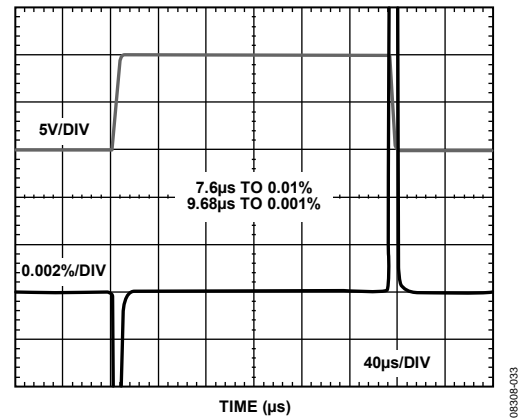


Figure 33. Large-Signal Pulse Response and Settling Time, 10 V Step, $V_S = \pm 15\text{ V}$, $G = 2$

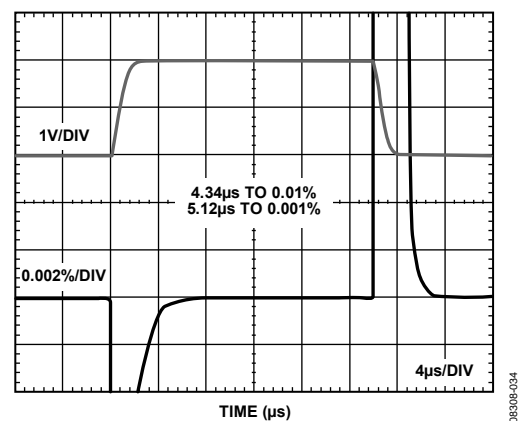


Figure 34. Large-Signal Pulse Response and Settling Time, 2 V Step, $V_S = 2.7\text{ V}$

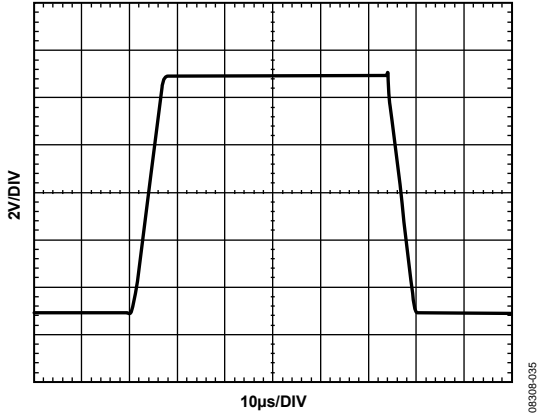


Figure 35. Large-Signal Step Response, $G = \frac{1}{2}$

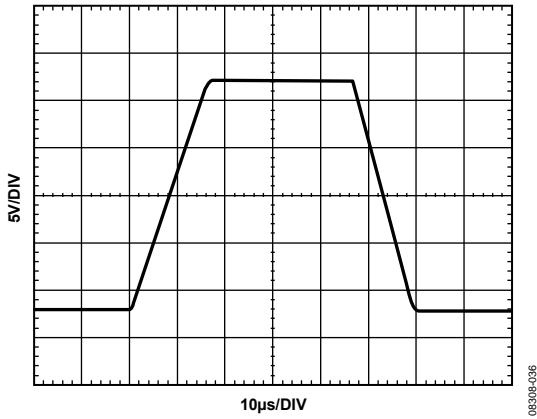


Figure 36. Large-Signal Step Response, $G = 2$

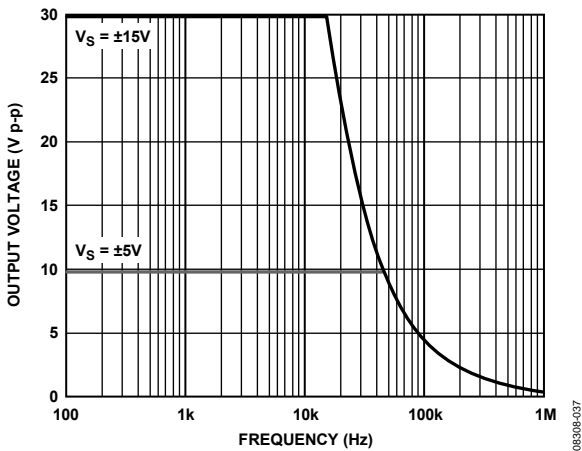


Figure 37. Maximum Output Voltage vs. Frequency, $V_S = \pm 15V, \pm 5V$

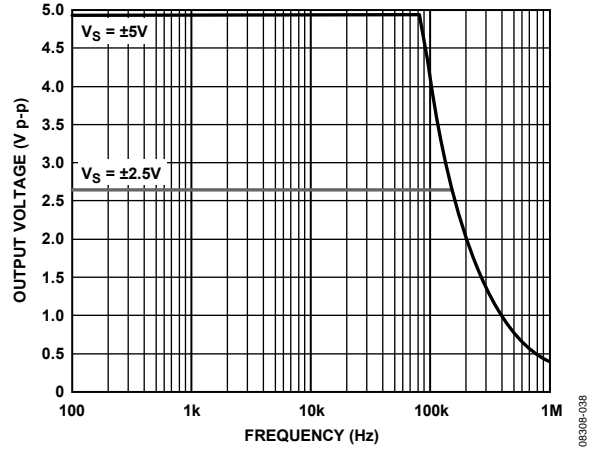


Figure 38. Maximum Output Voltage vs. Frequency, $V_S = 5V, 2.7V$

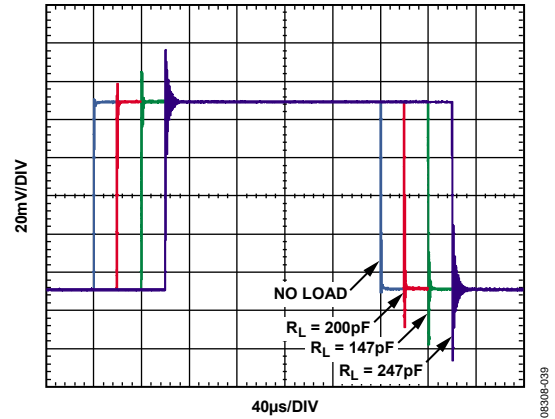


Figure 39. Small-Signal Step Response for Various Capacitive Loads, $G = \frac{1}{2}$

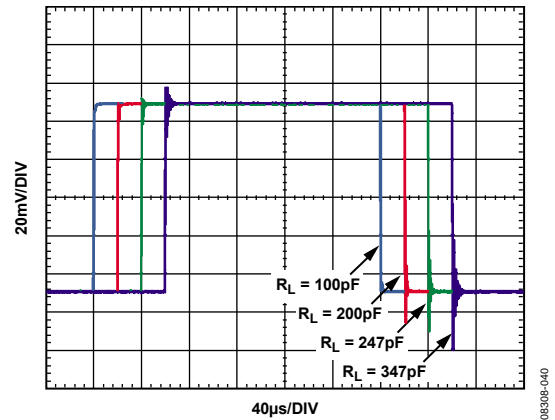


Figure 40. Small-Signal Step Response for Various Capacitive Loads, $G = 2$

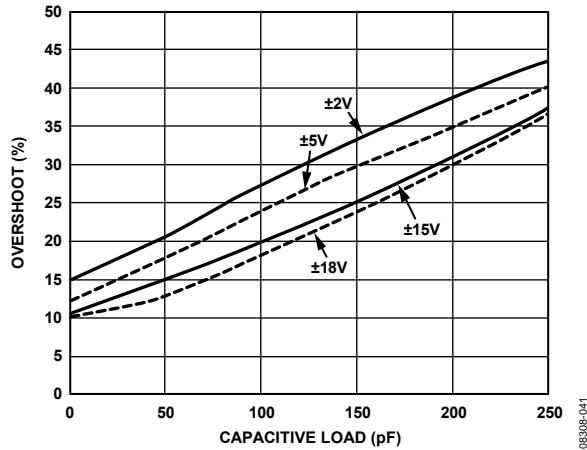


Figure 41. Small-Signal Overshoot vs. Capacitive Load, $R_L \geq 2 \text{ k}\Omega$, $G = \frac{1}{2}$

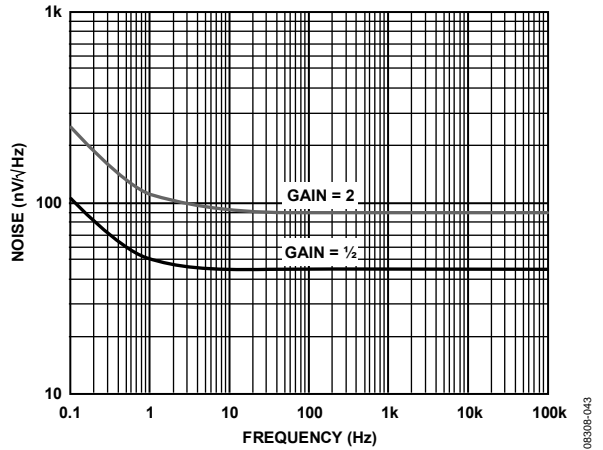


Figure 43. Voltage Noise Density vs. Frequency

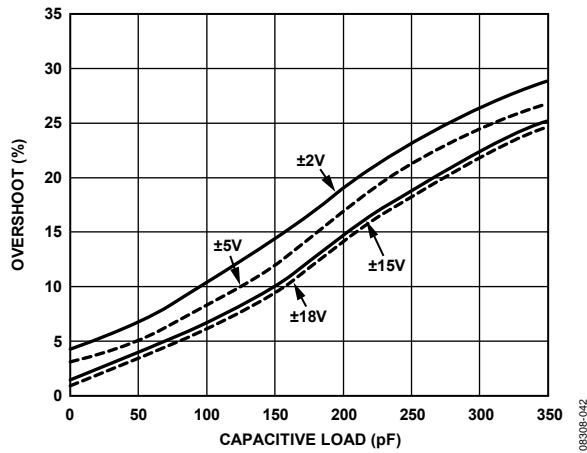


Figure 42. Small-Signal Overshoot vs. Capacitive Load, $R_L \geq 2 \text{ k}\Omega$, $G = 2$

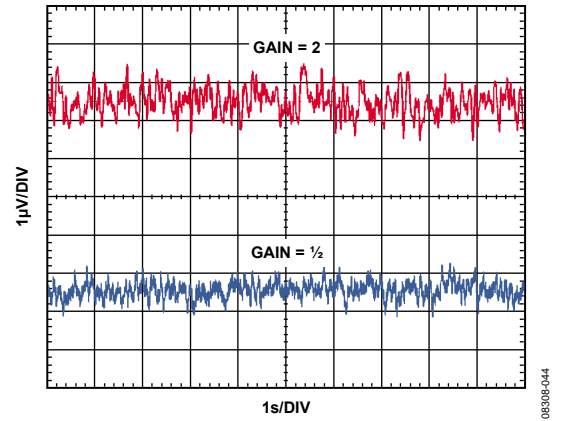


Figure 44. 0.1 Hz to 10 Hz Voltage Noise

THEORY OF OPERATION

CIRCUIT INFORMATION

The AD8278 consists of a low power, low noise op amp and four laser-trimmed on-chip resistors. These resistors can be externally connected to make a variety of amplifier configurations, including difference, noninverting, and inverting configurations. Taking advantage of the integrated resistors of the AD8278 provides the designer with several benefits over a discrete design, including smaller size, lower cost, and better ac and dc performance.

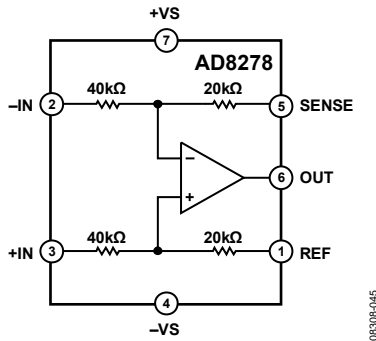


Figure 45. Functional Block Diagram

DC Performance

Much of the dc performance of op amp circuits depends on the accuracy of the surrounding resistors. Using superposition to analyze a typical difference amplifier circuit, as is shown in Figure 46, the output voltage is found to be

$$V_{OUT} = V_{IN+} \left(\frac{R2}{R1 + R2} \right) \left(1 + \frac{R4}{R3} \right) - V_{IN-} \left(\frac{R4}{R3} \right)$$

This equation demonstrates that the gain accuracy and common-mode rejection ratio of the AD8278 is determined primarily by the matching of resistor ratios. Even a 0.1% mismatch in one resistor degrades the CMRR to 69 dB for a $G = 2$ difference amplifier.

The difference amplifier output voltage equation can be reduced to

$$V_{OUT} = \frac{R4}{R3} (V_{IN+} - V_{IN-})$$

as long as the following ratio of the resistors is tightly matched:

$$\frac{R2}{R1} = \frac{R4}{R3}$$

The resistors on the AD8278 are laser trimmed to match accurately. As a result, the AD8278 provides superior performance over a discrete solution, enabling better CMRR, gain accuracy, and gain drift, even over a wide temperature range.

AC Performance

Component sizes and trace lengths are much smaller in an IC than on a PCB, so the corresponding parasitic elements are also smaller. This results in better ac performance of the AD8278. For example, the positive and negative input terminals of the AD8278 op amp are intentionally not pinned out. By not connecting these nodes to the traces on the PCB, their capacitance remains low and balanced, resulting in improved loop stability and excellent common-mode rejection over frequency.

DRIVING THE AD8278

Care should be taken to drive the AD8278 with a low impedance source: for example, another amplifier. Source resistance of even a few kilohms (kΩ) can unbalance the resistor ratios and, therefore, significantly degrade the gain accuracy and common-mode rejection of the AD8278. Because all configurations present several kilohms (kΩ) of input resistance, the AD8278 does not require a high current drive from the source and so is easy to drive.

INPUT VOLTAGE RANGE

The AD8278 is able to measure input voltages beyond the supply rails. The internal resistors divide down the voltage before it reaches the internal op amp, and provide protection to the op amp inputs. Figure 46 shows an example of how the voltage division works in a difference amplifier configuration. For the AD8278 to measure correctly, the input voltages at the input nodes of the internal op amp must stay below 1.5 V of the positive supply rail and can exceed the negative supply rail by 0.1 V. Refer to the Power Supplies section for more details.

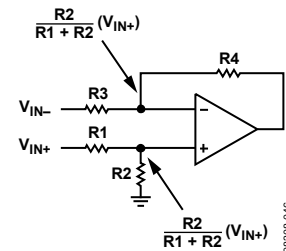


Figure 46. Voltage Division in the Difference Amplifier Configuration

The AD8278 has integrated ESD diodes at the inputs that provide overvoltage protection. This feature simplifies system design by eliminating the need for additional external protection circuitry, and enables a more robust system.

The voltages at any of the inputs of the parts can safely range from $+V_S - 40$ V up to $-V_S + 40$ V. For example, on ± 10 V supplies, input voltages can go as high as ± 30 V. Care should be taken to not exceed the $+V_S - 40$ V to $-V_S + 40$ V input limits to avoid risking damage to the parts.

POWER SUPPLIES

The AD8278 operates extremely well over a very wide range of supply voltages. It can operate on a single supply as low as 2 V and as high as 36 V, under appropriate setup conditions.

For best performance, the user must exercise care that the setup conditions ensure that the internal op amp is biased correctly. The internal input terminals of the op amp must have sufficient voltage headroom to operate properly. Proper operation of the part requires at least 1.5 V between the positive supply rail and the op amp input terminals. This relationship is expressed in the following equation:

$$\frac{R1}{R1 + R2} V_{REF} < +V_S - 1.5 V$$

For example, when operating on a $+V_S = 2 V$ single supply and $V_{REF} = 0 V$, it can be seen from Figure 47 that the op amp's input terminals are biased at 0 V, allowing more than the required 1.5 V headroom. However, if $V_{REF} = 1 V$ under the same conditions, the input terminals of the op amp are biased at 0.66 V ($G = \frac{1}{2}$). Now the op amp does not have the required 1.5 V headroom and can not function. Therefore, the user needs to increase the supply voltage or decrease V_{REF} to restore proper operation.

The AD8278 is typically specified at single- and dual-supplies, but it can be used with unbalanced supplies as well; for example, $-V_S = -5 V$, $+V_S = 20 V$. The difference between the two supplies must be kept below 36 V. The positive supply rail must be at least 2 V above the negative supply and reference voltage.

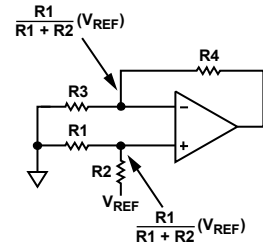
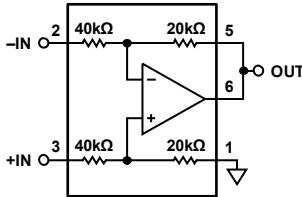


Figure 47. Ensure Sufficient Voltage Headroom on the Internal Op Amp Inputs

Use a stable dc voltage to power the AD8278. Noise on the supply pins can adversely affect performance. Place a bypass capacitor of 0.1 μF between each supply pin and ground, as close as possible to each supply pin. Use a tantalum capacitor of 10 μF between each supply and ground. It can be farther away from the supply pins and, typically, it can be shared by other precision integrated circuits.

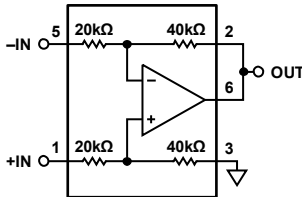
APPLICATIONS INFORMATION CONFIGURATIONS

The AD8278 can be configured in several ways, as a difference amplifier or a single-ended amplifier (see Figure 48 to Figure 54). All of these configurations have excellent gain accuracy and gain drift because they rely on the internal matched resistors. Note that Figure 50 shows the AD8278 as a difference amplifier with a midsupply reference voltage at the noninverting input. This allows the AD8278 to be used as a level shifter, which is appropriate in single-supply applications that are referenced to midsupply. Table 9 lists several single-ended amplifier configurations that are not illustrated.



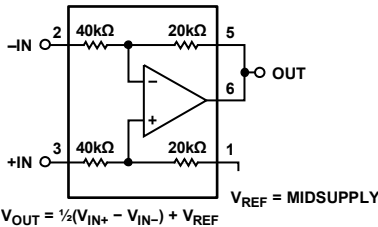
$$V_{OUT} = \frac{1}{2}(V_{IN+} - V_{IN-})$$

Figure 48. Difference Amplifier, Gain = 1/2



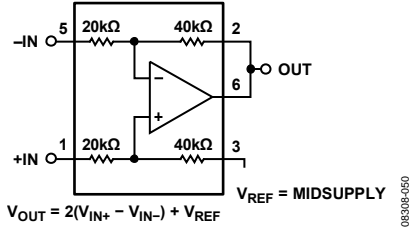
$$V_{OUT} = 2(V_{IN+} - V_{IN-})$$

Figure 49. Difference Amplifier, Gain = 2



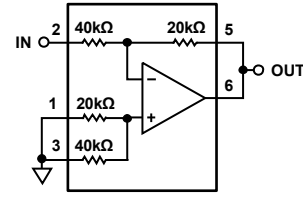
$$V_{OUT} = \frac{1}{2}(V_{IN+} - V_{IN-}) + V_{REF}$$

Figure 50. Difference Amplifier, Gain = 1/2, Referenced to Midsupply



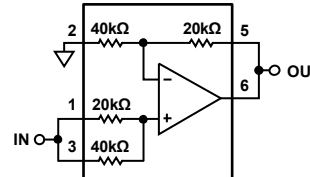
$$V_{OUT} = 2(V_{IN+} - V_{IN-}) + V_{REF}$$

Figure 51. Difference Amplifier, Gain = 2, Referenced to Midsupply



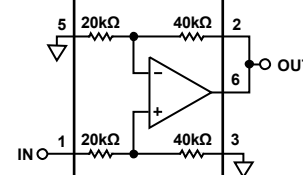
$$V_{OUT} = -\frac{1}{2}V_{IN}$$

Figure 52. Inverting Amplifier, Gain = -1/2



$$V_{OUT} = 1.5V_{IN}$$

Figure 53. Noninverting Amplifier, Gain = 1.5



$$V_{OUT} = 2V_{IN}$$

Figure 54. Noninverting Amplifier, Gain = 2

Table 9. Difference and Single-Ended Amplifier Configurations

Amplifier Configuration	Signal Gain	Pin 1 (REF)	Pin 2 (VIN-)	Pin 3 (VIN+)	Pin 5 (SENSE)
Difference Amplifier	+1/2	GND	IN-	IN+	OUT
Difference Amplifier	+2	IN+	OUT	GND	IN-
Single-Ended Inverting Amplifier	-1/2	GND	IN	GND	OUT
Single-Ended Inverting Amplifier	-2	GND	OUT	GND	IN
Single-Ended Non Inverting Amplifier	+3/2	IN	GND	IN	OUT
Single-Ended Non Inverting Amplifier	+3	IN	OUT	IN	GND
Single-Ended Non Inverting Amplifier	+1/2	GND	GND	IN	OUT
Single-Ended Non Inverting Amplifier	+1	IN	GND	GND	OUT
Single-Ended Non Inverting Amplifier	+1	GND	OUT	IN	GND
Single-Ended Non Inverting Amplifier	+2	IN	OUT	GND	GND

As with the other inputs, the reference must be driven with a low impedance source to maintain the internal resistor ratio. An example using the low power, low noise OP1177 as a reference is shown in Figure 55.

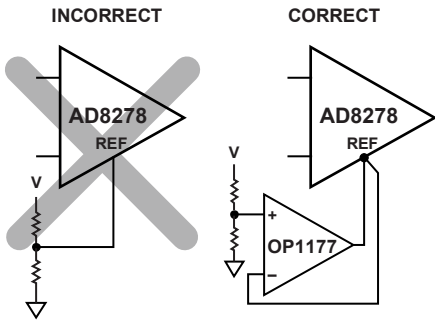


Figure 55. Driving the Reference Pin

INSTRUMENTATION AMPLIFIER

The AD8278 can be used as a building block for a low power, low cost instrumentation amplifier. An instrumentation amplifier provides high impedance inputs and delivers high common-mode rejection. Combining the AD8278 with an Analog Devices, Inc., low power amplifier (see Table 10) creates a precise, power efficient voltage measurement solution suitable for power critical systems.

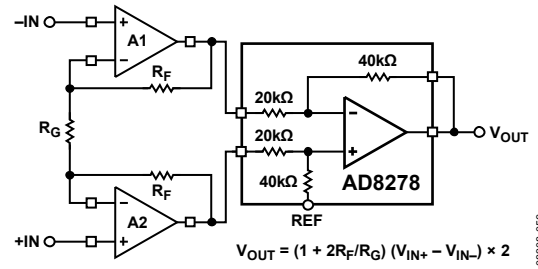


Figure 56. Low Power Precision Instrumentation Amplifier

$$V_{OUT} = (1 + 2R_F/R_G) (V_{IN+} - V_{IN-}) \times 2$$

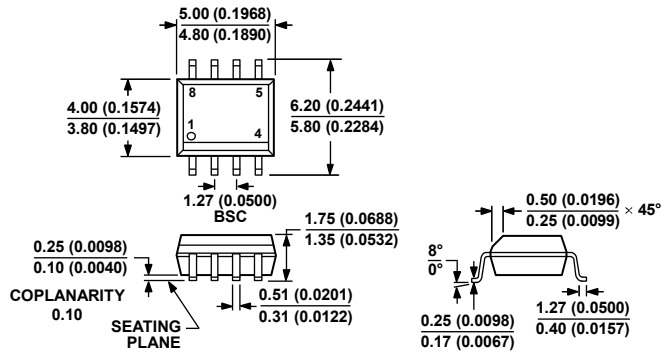
Table 10. Low Power Op Amps

Op Amp (A1, A2)	Features
AD8506	Dual micropower op amp
AD8607	Precision dual micropower op amp
AD8617	Low cost CMOS micropower op amp
AD8667	Dual precision CMOS micropower op amp

It is preferable to use dual op amps for the high impedance inputs, because they have better matched performance and track each other over temperature. The AD8278 difference amplifier cancels out common-mode errors from the input op amps, if they track each other. The differential gain accuracy of the in-amp is proportional to how well the input feedback resistors (R_F) match each other. The CMRR of the in-amp increases as the differential gain is increased ($1 + 2R_F/R_G$), but a higher gain also reduces the common-mode voltage range. Note that dual supplies must be used for proper operation of this configuration.

Refer to *A Designer's Guide to Instrumentation Amplifiers* for more design ideas and considerations.

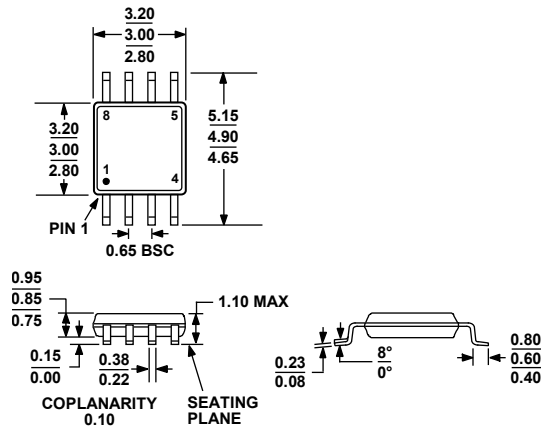
OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-012-AA
 CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS
 (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 57. 8-Lead Standard Small Outline Package [SOIC_N]
 Narrow Body (R-8)
 Dimensions shown in millimeters and (inches)

012407-A



COMPLIANT TO JEDEC STANDARDS MO-187-AA
 Figure 58. 8-Lead Mini Small Outline Package [MSOP]
 (RM-8)
 Dimensions shown in millimeters

ORDERING GUIDE

Model	Temperature Range	Package Description	Package Option	Branding
AD8278ARZ ¹	-40°C to +85°C	8-Lead SOIC_N	R-8	
AD8278ARZ-R7 ¹	-40°C to +85°C	8-Lead SOIC_N, 7" Tape and Reel	R-8	
AD8278ARZ-RL ¹	-40°C to +85°C	8-Lead SOIC_N, 13" Tape and Reel	R-8	
AD8278BRZ ¹	-40°C to +85°C	8-Lead SOIC_N	R-8	
AD8278BRZ-R7 ¹	-40°C to +85°C	8-Lead SOIC_N, 7" Tape and Reel	R-8	
AD8278BRZ-RL ¹	-40°C to +85°C	8-Lead SOIC_N, 13" Tape and Reel	R-8	
AD8278ARMZ ¹	-40°C to +85°C	8-Lead MSOP	RM-8	Y21
AD8278ARMZ-R7 ¹	-40°C to +85°C	8-Lead MSOP, 7" Tape and Reel	RM-8	Y21
AD8278ARMZ-RL ¹	-40°C to +85°C	8-Lead MSOP, 13" Tape and Reel	RM-8	Y21
AD8278BRMZ ¹	-40°C to +85°C	8-Lead MSOP	RM-8	Y22
AD8278BRMZ-R7 ¹	-40°C to +85°C	8-Lead MSOP, 7" Tape and Reel	RM-8	Y22
AD8278BRMZ-RL ¹	-40°C to +85°C	8-Lead MSOP, 13" Tape and Reel	RM-8	Y22

¹ Z = RoHS Compliant Part.

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