# LM5008A Evaluation Board

National Semiconductor Application Note 1925 Dennis Morgan March 25, 2010



#### Introduction

The LM5008AEVAL evaluation board provides the design engineer with a fully functional buck regulator, employing the constant on-time (COT) operating principle. This evaluation board provides a 5V output over an input range of 8V to 75V. The circuit delivers load currents to 300 mA, with current limit set at a nominal 440 mA.

The board's specification are:

Input Voltage: 8V to 75V

Output Voltage: 5V

Maximum load current: 300 mA

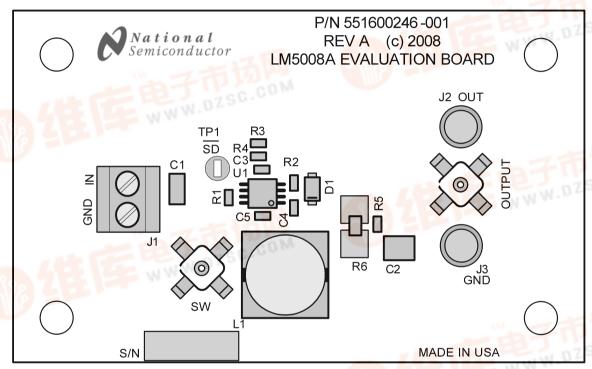
Minimum load current: 0A

• Current Limit: 440 mA (nominal)

Measured Efficiency: 92.4% (V<sub>IN</sub> = 8V, I<sub>OUT</sub> = 100 mA)

Nominal Switching Frequency: 130 kHz

Size: 2.6 in. x 1.6 in.



30086301

FIGURE 1. Evaluation Board - Top Side

# **Theory of Operation**

Refer to the evaluation board schematic in *Figure 5*. When the circuit is in regulation, the buck switch is on each cycle for a time determined by R1 and VIN according to the equation:

$$t_{ON} = \frac{1.385 \times 10^{-10} \times R1}{V_{IN}}$$

The on-time of this evaluation board ranges from ≊4.85 µs at VIN = 8V, to ≊517 ns at VIN = 75V. The on-time varies inversely with VIN to maintain a nearly constant switching fre-

quency. At the end of each on-time the Minimum Off-Timer ensures the buck switch is off for at least 300 ns. In normal operation, the off-time is much longer. During the off-time, the load current is supplied by the output capacitor (C2). When the output voltage falls sufficiently that the voltage at FB is below 2.5V, the regulation comparator initiates a new on-time period. For stable, fixed frequency operation, a minimum of 25 mV of ripple is required at FB to switch the regulation comparator. The current limit threshold is ≊470 mA at Vin = 8V, and ≊415 mA at Vin = 75V. Refer to the LM5008A data sheet for a more detailed block diagram, and a complete description of the various functional blocks.

- Board Layout and Probing

  in M5008A House shows the placement of the circuit components. The following should be kept in mind when the board is powered:
- 1) When operating at high input voltage and high load current, forced air flow may be necessary.
- 2) The LM5008A, and diode D1 may be hot to the touch when operating at high input voltage and high load current.
- 3) Use CAUTION when probing the circuit at high input voltages to prevent injury, as well as possible damage to the
- 4) At maximum load current, the wire size and length used to connect the load becomes important. Ensure there is not a significant drop in the wires between this evaluation board and the load.

### **Board Connection/Start-up**

The input connections are made to the J1 connector. The load is connected to the J2 (OUT) and J3 (GND) terminals. Ensure the wires are adequately sized for the intended load current. Before start-up a voltmeter should be connected to the input terminals, and to the output terminals. The load current should be monitored with an ammeter or a current probe. It is recommended that the input voltage be increased gradually to 8V, at which time the output voltage should be 5V. If the output voltage is correct with 8V at VIN, then increase the input voltage as desired and proceed with evaluating the circuit. DO NOT EXCEED 75V AT VIN.

## **Output Ripple Control**

The LM5008A requires a minimum of 25 mVp-p ripple at the FB pin, in phase with the switching waveform at the SW pin, for proper operation. The required ripple can be supplied from ripple at V<sub>OUT</sub>, through the feedback resistors as described in Option A below. Options B and C provide lower output ripple with one or two additional components.

Option A) Lowest Cost Configuration: In this configuration R5 is installed in series with the output capacitance (C2). Since ≥25 mVp-p are required at the FB pin, R5 must be chosen to generate ≥50 mVp-p at V<sub>OUT</sub>, knowing that the minimum ripple current in this circuit is 266 mAp-p at minimum  $V_{IN}$ . Using  $0.82\Omega$  for R5, the ripple at  $V_{OUT}$  ranges from ≊54 mVp-p to ≊135 mVp-p over the input voltage range. If the application can accept this ripple level, this is the most economical solution. The circuit is shown in Figure 2. See Figure

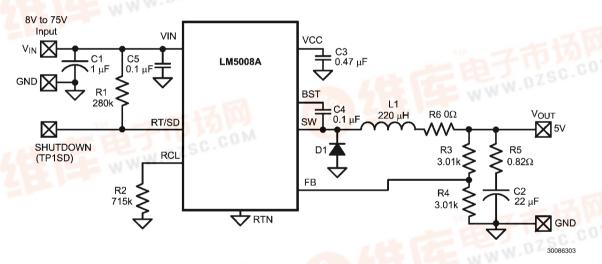


FIGURE 2. Lowest Cost Configuration



Option B) Intermediate Ripple Configuration: This configuration are noticed by the plant of the policy of the poli

the addition of one capacitor (Cff) across R3, as shown in *Figure 3*.

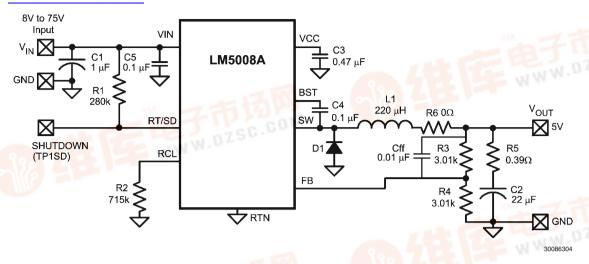


FIGURE 3. Intermediate Ripple Configuration

Since the output ripple is passed by Cff to the FB pin with little or no attenuation, R5 can be reduced so the minimum ripple at V<sub>OUT</sub> is ≊25 mVp-p. The minimum value for Cff is calculated from:

$$Cff \ge \frac{3 \times t_{ON \text{ (max)}}}{(R3//R4)}$$

where  $t_{ON(max)}$  is the maximum on-time (at minimum  $V_{IN}$ ), and R3//R4 is the parallel equivalent of the feedback resistors. The ripple at  $V_{OUT}$  ranges from 26 mVp-p to 64 mVp-p over the input voltage range. See *Figure 8*.

**Option C) Minimum Ripple Configuration:** To obtain minimum ripple at  $V_{OUT}$ , R5 is set to  $0\Omega$ , and RA, CA, and CB are added to generate the required ripple for the FB pin. In this configuration, the output ripple is determined primarily by the characteristics of the output capacitance and the inductor's ripple current. See *Figure 4*.

The ripple voltage required by the FB pin is generated by RA, and CA since the SW pin switches from -1V to  $V_{\rm IN}$ , and the right end of CA is a virtual ground. The values for RA and CA are chosen to generate a 50-100 mVp-p triangle waveform at their junction. That triangle wave is then coupled to the FB pin through CB. The following procedure is used to calculate values for RA, CA and CB:

1) Calculate the voltage V<sub>A</sub>:

$$V_A = V_{OUT} - (V_{SW} x (1 - (V_{OUT}/V_{IN})))$$

where  $V_{SW}$  is the absolute value of the voltage at the SW pin during the off-time (typically 0.6V), and  $V_{IN}$  is the minimum input voltage. For this circuit,  $V_A$  calculates to 4.78V. This is the approximate DC voltage at the RA/CA junction, and is used in the next equation.

2) Calculate the RA x CA product:

$$RA \times CA = \frac{(V_{IN} - V_A) \times t_{ON}}{\Delta V}$$

where  $t_{ON}$  is the maximum on-time ( $\approxeq 4.85~\mu s$ ),  $V_{IN}$  is the minimum input voltage, and  $\Delta V$  is the desired ripple amplitude at the RA/CA junction, 50 mVp-p for this example.

RA x CA = 
$$\frac{(8V - 4.78V) \times 4.85 \ \mu s}{0.05V} = 3.12 \times 10^{-4}$$

RA and CA are then chosen from standard value components to satisfy the above product. Typically CA is 3000 to 10000 pF, and RA is 10 k $\Omega$  to 300 k $\Omega$ . CB is chosen large compared to CA, typically 0.1 µF. The ripple at V<sub>OUT</sub> is typically less than 10 mVp-p. See *Figure 4* and *Figure 8*.





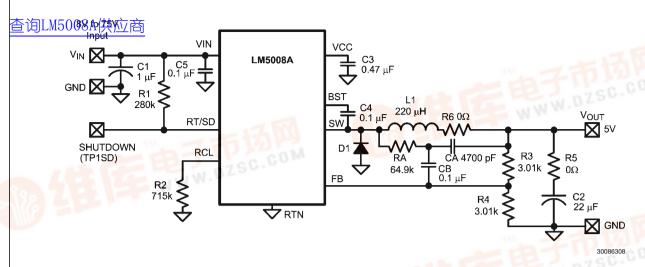


FIGURE 4. Minimum Output Ripple Configuration

### **Current Limit Off-Time**

When current limit is detected the on-time period is immediately terminated, and the off-time forced by the LM5008A must be greater than the maximum normal off-time, which occurs at maximum input voltage. The longer-than-normal off-time is necessary to allow the inductor current to decrease at least as much, if not more, than the current increase which occurred during the on-time leading to the current limit detection. The forced off-time is determined by the resistor at the RCL pin (R2), and is calculated from the following:

$$T_{OFF} = 10^{-5}/(0.285 + (V_{FB}/6.35 \times 10^{-6} \times R2))$$

where  $V_{FB}$  is the voltage at the FB pin at the time of the current limit detection. In this evaluation board, the maximum normal off-time is approximately 7.2  $\mu$ s (at 75V). Due to the 25% tolerance of the on-time, the off-time tolerance is also 25%, yielding a maximum possible off-time of 9  $\mu$ s. Allowing for the response time of the current limit detection circuit (350 ns) the maximum off-time, for the purpose of this calculation, is increased to 9.35  $\mu$ s. This is increased an additional 25% to

11.7  $\mu$ s to allow for the tolerances of the above equation. Using the above equation, R2 calculates to 691 k $\Omega$  at V<sub>FB</sub> = 2.5V. A standard value 715 k $\Omega$  resistor is used.

#### **Monitor The Inductor Current**

The inductor's current can be monitored or viewed on a scope with a current probe. Remove R6, and install an appropriate current loop across the two large pads where R6 was located. In this way the inductor's ripple current and peak current can be accurately determined.

### **Scope Probe Adapters**

Scope probe adapters are provided on this evaluation board for monitoring the waveform at the SW pin, and at the circuit's output  $(V_{OUT})$ , without using the probe's ground lead which can pick up noise from the switching waveforms. The probe adapters are suitable for Tektronix P6137 or similar probes, with a 0.135" diameter.

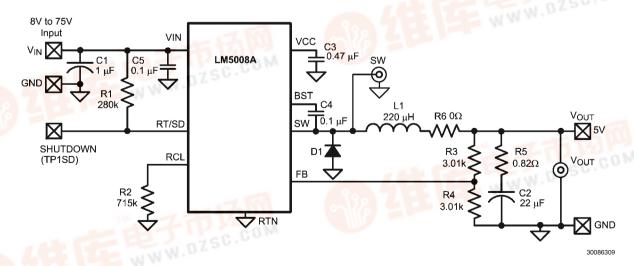


FIGURE 5. Complete Evaluation Board Schematic (As Supplied)

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| Item   | Description         | Mfg., Part Number                                 | Package     | Value                       |  |  |  |
|--------|---------------------|---|-------------|-----------------------------|--|--|--|
| C1     | Ceramic Capacitor   | TDK C3216X7R2A105M or Murata GRM31CR72A105KA01L   | 1206        | 1 μF, 100V                  |  |  |  |
| C2     | Ceramic Capacitor   | TDK C3225X7R1C226M or Murata GRM32ER71C226KE18L   | 1210        | 22 μF, 16V                  |  |  |  |
| C3     | Ceramic Capacitor   | TDK C1608X7R1C474M or TDK C1608X7R1C474K          | 0603        | 0. <mark>4</mark> 7 μF, 16V |  |  |  |
| C4     | Ceramic Capacitor   | TDK C1608X7R1H103M                                | 0603        | 0.01 μF, 50V                |  |  |  |
| C5     | Ceramic Capacitor   | TDK C2012X7R2A104M or Murata GRM188R72A104KA35D   | 0805        | 0.1 μF, 100V                |  |  |  |
| D1     | Schottky Diode      | Diodes Inc. DFLS1100 or Central Semi CMMSH1-100   | Power DI123 | 100V, 1A                    |  |  |  |
| L1     | Power Inductor      | Coiltronics DR1050-221-R or TDK SLF10145T-221MR65 | 10mm x 10mm | 220 μH                      |  |  |  |
| R1     | Resistor            | Vishay CRCW06032803F                              | 0603        | 280k                        |  |  |  |
| R2     | Resistor            | Vishay CRCW06037153F                              | 0603        | 715k                        |  |  |  |
| R3, R4 | Resistor            | Vishay CRCW06033011F                              | 0603        | 3.01k                       |  |  |  |
| R5     | Resistor            | Panasonic ERJ-3RQFR82V                            | 0603        | 0.82 ohms                   |  |  |  |
| R6     | Resistor            | Vishay CRCW08050000Z                              | 0805        | 0Ω Jumper                   |  |  |  |
| U1     | Switching Regulator | National Semiconductor LM5008AMM                  | MSOP-8      | DZSU.                       |  |  |  |



# Circuit Performance 查询LM5008A供应商

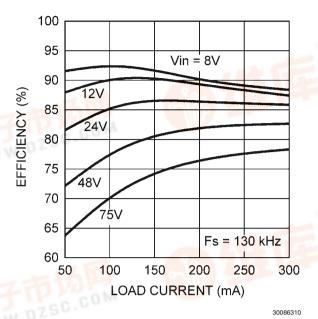


FIGURE 6. Efficiency vs Load Current

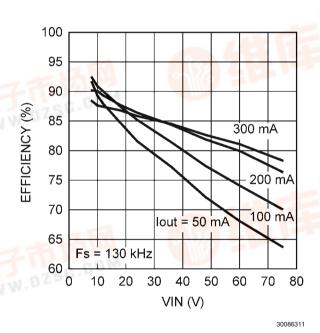


FIGURE 7. Efficiency vs Input Voltage

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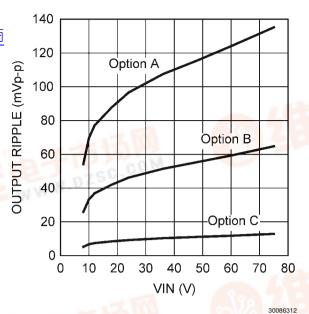


FIGURE 8. Output Voltage Ripple

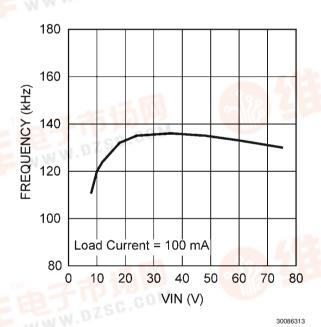


FIGURE 9. Switching Frequency vs. Input Voltage

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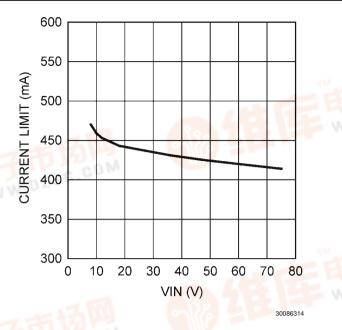


FIGURE 10. Current Limit vs Input Voltage

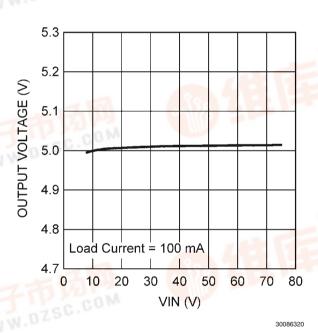
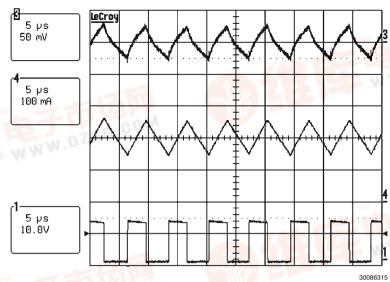


FIGURE 11. Line Regulation

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# Typical Waveforms 查询LM5008A供应商



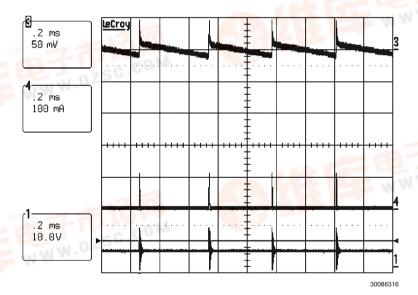
Trace 1 = SW Pin

Trace 3 = V<sub>OUT</sub>

Trace 4 = Inductor Current

Vin = 12V, lout = 200 mA

#### **FIGURE 13. Continuous Conduction Mode**



Trace 1 = SW Pin

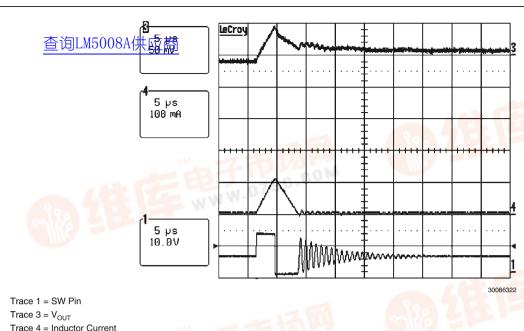
Trace 3 = V<sub>OUT</sub>

Trace 4 = Inductor Current

Vin = 12V, lout = 0 mA

FIGURE 14. Discontinuous Conduction Mode





Trace 4 = Inductor Current Vin = 12V, lout = 0 mA

FIGURE 15. Discontinuous Conduction Mode





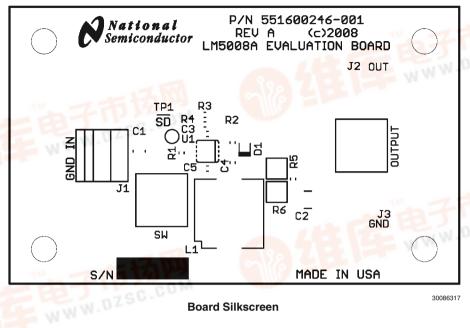






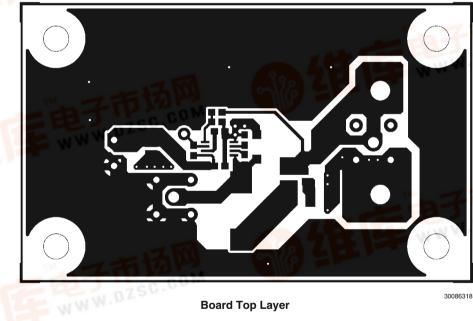


# PC Board Layout 查询LM5008A供应商



**Board Silkscreen** 

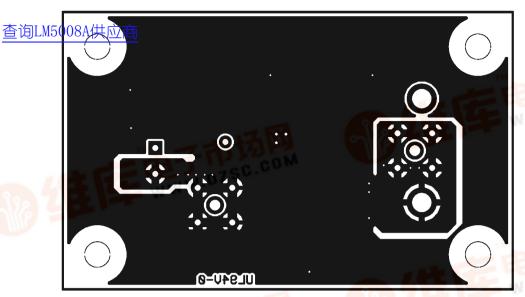
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**Board Top Layer** 

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Board Bottom Layer (Viewed from Top)

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| LDOs                           | www.national.com/ldo         | Quality and Reliability         | www.national.com/quality       |  |
| LED Lighting                   | www.national.com/led         | Feedback/Support                | www.national.com/feedback      |  |
| Voltage References             | www.national.com/vref        | Design Made Easy                | www.national.com/easy          |  |
| PowerWise® Solutions           | www.national.com/powerwise   | Applications & Markets          | www.national.com/solutions     |  |
| Serial Digital Interface (SDI) | www.national.com/sdi         | Mil/Aero                        | www.national.com/milaero       |  |
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