

| Pin | Symbol | | Function |
|-----|-----------------|---|--|
| 1 | OUT | O | Output to the load. The pins 1 and 5 must be shorted with each other especially in high current applications! ³⁾ |
| 2 | IN | I | Input, activates the power switch in case of short to ground |
| 3 | V _{bb} | + | Positive power supply voltage, the tab is electrically connected to this pin. In high current applications the tab should be used for the V _{bb} connection instead of this pin ⁴⁾ . |
| 4 | IS | S | Diagnostic feedback providing a sense current proportional to the load current; zero current on failure (see Truth Table on page 6) |
| 5 | OUT | O | Output to the load. The pins 1 and 5 must be shorted with each other especially in high current applications! ³⁾ |

Maximum Ratings at $T_j = 25\text{ °C}$ unless otherwise specified

| Parameter | Symbol | Values | Unit |
|--|-----------------------|--------------|------|
| Supply voltage (overvoltage protection see page 4) | V_{bb} | 60 | V |
| Supply voltage for full short circuit protection, resistive load or $L < t_{bd} \mu\text{H}$ $T_{j,start} = -40 \dots +150\text{ °C}$: | V_{bb} | 55 | V |
| Load current (short circuit current, see page 4) | I_L | self-limited | A |
| Load dump protection $V_{LoadDump} = U_A + V_S$, $U_A = 13.5\text{ V}$ $R_1^{5)} = 2\ \Omega$, $R_L = 0.1\ \Omega$, $t_d = 200\text{ ms}$, IN, IS = open or grounded | $V_{Load\ dump}^{6)}$ | 80 | V |
| Operating temperature range | T_j | -40 ... +150 | °C |
| Storage temperature range | T_{stg} | -55 ... +150 | |
| Power dissipation (DC), $T_C \leq 25\text{ °C}$ | P_{tot} | 310 | W |
| Inductive load switch-off energy dissipation, single pulse $V_{bb} = 12\text{ V}$, $T_{j,start} = 150\text{ °C}$, $T_C = 150\text{ °C}$ const., $I_L = t_{bd} (>=20)\text{ A}$, $Z_L = t_{bd}\text{ mH}$, $0\ \Omega$, see diagrams on page 9 | E_{AS} | tbd | J |
| Electrostatic discharge capability (ESD) Human Body Model acc. MIL-STD883D, method 3015.7 and ESD asn. std. S5.1-1993, $C = 100\text{ pF}$, $R = 1.5\text{ k}\Omega$ | V_{ESD} | 2.0 | kV |
| Current through input pin (DC) | I_{IN} | +15, -250 | mA |
| Current through current sense status pin (DC) see internal circuit diagrams on page 7 | I_{IS} | +15, -250 | |

3) Not shorting all outputs will considerably increase the on-state resistance, reduce the peak current capability and decrease the current sense accuracy

4) Otherwise add up to 0.5 mΩ (depending on used length of the pin) to the R_{ON} if the pin is used instead of the tab.

5) R_1 = internal resistance of the load dump test pulse generator.

6) $V_{Load\ dump}$ is setup without the DUT connected to the generator per ISO 7637-1 and DIN 40839.

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Thermal Characteristics

| Parameter and Conditions | Symbol | Values | | | Unit |
|--|------------------|--------|-----|------|------|
| | | min | typ | max | |
| Thermal resistance chip - case: junction - ambient (free air): | $R_{thJC}^{(7)}$ | -- | -- | 0.40 | K/W |
| | R_{thJA} | -- | 30 | -- | |

Electrical Characteristics

| Parameter and Conditions | Symbol | Values | | | Unit |
|---|--------|--------|-----|-----|------|
| | | min | typ | max | |
| at $T_j = -40 \dots +150 \text{ }^\circ\text{C}$, $V_{bb} = 12 \text{ V}$ unless otherwise specified | | | | | |

Load Switching Capabilities and Characteristics

| | | | | | |
|---|----------------|------------|------------|-------------------|------------------------|
| On-state resistance (Tab to pins 1,5, see measurement circuit page 7) $I_L = tbd (>=20) \text{ A}$, $T_j = 25 \text{ }^\circ\text{C}$: $V_{IN} = 0$, $I_L = tbd (>=20) \text{ A}$, $T_j = 150 \text{ }^\circ\text{C}$: $I_L = 150 \text{ A}$, $T_j = 150 \text{ }^\circ\text{C}$: | R_{ON} | -- | 3.3 6.5 | 4.0 7.8 7.9 | $\text{m}\Omega$ |
| Nominal load current ⁸⁾ (Tab to pins 1,5) ISO 10483-1/6.7: $V_{ON} = 0.5 \text{ V}$, $T_C = 85 \text{ }^\circ\text{C}$ ⁹⁾ | $I_{L(ISO)}$ | 80 | 96 | -- | A |
| Maximum load current in resistive range (Tab to pins 1,5) $V_{ON} = 1.8 \text{ V}$, $T_C = 25 \text{ }^\circ\text{C}$: see diagram on page 12 $V_{ON} = 1.8 \text{ V}$, $T_C = 150 \text{ }^\circ\text{C}$: | $I_{L(Max)}$ | tbd tbd | -- -- | -- -- | A |
| Turn-on time ¹⁰⁾ $I_{IN} \begin{matrix} \text{---} \\ \text{┘} \end{matrix}$ to 90% V_{OUT} : | t_{on} | 130 | -- | 550 | μs |
| Turn-off time $I_{IN} \begin{matrix} \text{---} \\ \text{└} \end{matrix}$ to 10% V_{OUT} : $R_L = 1 \Omega$, $T_j = -40 \dots +150 \text{ }^\circ\text{C}$ | t_{off} | 60 | -- | 240 | |
| Slew rate on ¹⁰⁾ (10 to 30% V_{OUT}) $R_L = 1 \Omega$ | dV/dt_{on} | -- | 0.8 | -- | $\text{V}/\mu\text{s}$ |
| Slew rate off ¹⁰⁾ (70 to 40% V_{OUT}) $R_L = 1 \Omega$ | $-dV/dt_{off}$ | -- | 0.8 | -- | $\text{V}/\mu\text{s}$ |

Inverse Load Current Operation

| | | | | | |
|--|---------------|----|------------|------------|------------------|
| On-state resistance (Pins 1,5 to pin 3) $V_{bIN} = 12 \text{ V}$, $I_L = - tbd (>=20) \text{ A}$ see diagram on page 9 | $R_{ON(inv)}$ | -- | 3.3 6.5 | 4.0 7.8 | $\text{m}\Omega$ |
| Nominal inverse load current (Pins 1,5 to Tab) $V_{ON} = -0.5 \text{ V}$, $T_C = 85 \text{ }^\circ\text{C}$ ⁹⁾ | $I_{L(inv)}$ | 80 | 96 | -- | A |
| Drain-source diode voltage ($V_{out} > V_{bb}$) $I_L = - tbd (>=20) \text{ A}$, $I_{IN} = 0$, $T_j = +150 \text{ }^\circ\text{C}$ | $-V_{ON}$ | -- | tbd | -- | mV |

7) Thermal resistance R_{thCH} case to heatsink (about 0.25 K/W with silicone paste) not included!

8) Not tested, specified by design.

9) T_j is about $105 \text{ }^\circ\text{C}$ under these conditions.

10) See timing diagram on page 13.

| Parameter and Conditions | Symbol | Values | | | Unit |
|--|--------|--------|-----|-----|------|
| | | min | typ | max | |
| at $T_j = -40 \dots +150^\circ\text{C}$, $V_{bb} = 12\text{V}$ unless otherwise specified | | | | | |

Operating Parameters

| | | | | | |
|--|----------------|-----|-----|-----|---------------|
| Operating voltage ($V_{IN} = 0$) ¹¹⁾ | $V_{bb(on)}$ | 5.0 | -- | 55 | V |
| Undervoltage shutdown ¹²⁾ | $V_{bIN(u)}$ | -- | 3.5 | 4.5 | V |
| Undervoltage start of charge pump see diagram page 14 | $V_{bIN(ucp)}$ | -- | 5 | 6.5 | V |
| Overvoltage protection ¹³⁾ | $V_{bIN(z)}$ | 68 | -- | -- | V |
| $I_{bb} = 15\text{mA}$ | | 70 | 74 | -- | |
| Standby current | $I_{bb(off)}$ | -- | 15 | 25 | μA |
| $I_{IN} = 0$ | | -- | 25 | 60 | |

Protection Functions

| | | | | | |
|---|----------------|-----|-----|-----|---------------|
| Short circuit current limit (Tab to pins 1,5) $V_{ON} = 12\text{V}$, time until shutdown max. $300\mu\text{s}$ | $I_{L(SCp)}$ | -- | 370 | -- | A |
| $T_c = -40^\circ\text{C}$: | | tbd | 320 | tbd | |
| $T_c = 25^\circ\text{C}$: | | tbd | 225 | tbd | |
| $T_c = +150^\circ\text{C}$: | | tbd | | tbd | |
| Short circuit shutdown delay after input current positive slope, $V_{ON} > V_{ON(SC)}$ min. value valid only if input "off-signal" time exceeds $30\mu\text{s}$ | $t_d(SC)$ | 80 | -- | 300 | μs |
| Output clamp ¹⁴⁾ (inductive load switch off) (typ. $I_{IS} = -120\mu\text{A}$) | $-V_{OUT(CL)}$ | -- | 15 | -- | V |
| $I_L = 40\text{mA}$: | | -- | 17 | -- | |
| $I_L = 20\text{A}$: | | -- | | -- | |
| Output clamp (inductive load switch off) at $V_{OUT} = V_{bb} - V_{ON(CL)}$ (e.g. overvoltage) $I_L = 40\text{mA}$ | $V_{ON(CL)}$ | 60 | 64 | 68 | V |
| Short circuit shutdown detection voltage (pin 3 to pins 1,5) | $V_{ON(SC)}$ | -- | 6 | -- | V |

11) For all voltages $0 \dots 55\text{V}$ the device is fully protected against overtemperature and short circuit.

12) $V_{bIN} = V_{bb} - V_{IN}$ see diagram on page 7. When V_{bIN} increases from less than $V_{bIN(u)}$ up to $V_{bIN(ucp)} = 5\text{V}$ (typ.) the charge pump is not active and $V_{OUT} \approx V_{bb} - 3\text{V}$.

13) See also $V_{ON(CL)}$ in circuit diagram on page 8.

14) This output clamp can be "switched off" by using an additional diode at the IS-Pin (see page 7). If the diode is used, V_{OUT} is clamped to $V_{bb} - V_{ON(CL)}$ at inductive load switch off.

| Parameter and Conditions at $T_j = -40 \dots +150^\circ\text{C}$, $V_{bb} = 12\text{V}$ unless otherwise specified | Symbol | Values | | | Unit |
|--|-----------------|--------|-----|-----|------------------|
| | | min | typ | max | |
| Thermal overload trip temperature | T_{jt} | 150 | -- | -- | $^\circ\text{C}$ |
| Thermal hysteresis | ΔT_{jt} | -- | 10 | -- | K |

Reverse Battery

| | | | | | |
|---|----------------------|----|----------|----------|------------------|
| Reverse battery voltage ¹⁵⁾ | $-V_{bb}$ | -- | -- | 42 | V |
| On-state resistance (Pins 1,5 to pin 3) $T_j = 25^\circ\text{C}$: $V_{bb} = -12\text{V}$, $V_{IN} = 0$, $I_L = -\text{tbd}$ (≥ 20) A, $R_{IS} = 1\text{k}\Omega$ $T_j = 150^\circ\text{C}$: | $R_{ON(\text{rev})}$ | -- | 3.7 0 | tbd 0 | $\text{m}\Omega$ |
| Integrated resistor in V_{bb} line | R_{bb} | -- | tbd | -- | Ω |

Diagnostic Characteristics

| | | | | | | | |
|---|----------------|--|----------------|--|--|---|---------------|
| Current sense ratio, static on-condition, $k_{ILIS} = I_L : I_{IS}$, $V_{ON} < 1.5\text{V}^{16)}$, $V_{IS} < V_{OUT} - 5\text{V}$, $V_{bIN} > 4.5\text{V}$ | k_{ILIS} | -40 $^\circ\text{C}$: 25 $^\circ\text{C}$: 150 $^\circ\text{C}$: | -- -- -- | 26 530 25 430 23 520 | -- -- -- | | |
| see diagram on page 11 $I_{IN} = 0$, $I_{IS} = 0$ (e.g. during deenergizing of inductive loads): | | $I_L = 150\text{A}$: $I_L = 25\text{A}$: $I_L = 12\text{A}$: $I_L = 6\text{A}$: | | -40 $^\circ\text{C}$: $\pm 4.5\%$ $\pm 8.9\%$ $\pm 15\%$ $\pm 46\%$ | +25 $^\circ\text{C}$: $\pm 4.2\%$ $\pm 7.5\%$ $\pm 12\%$ $\pm 36\%$ | 150 $^\circ\text{C}$: $\pm 4.0\%$ $\pm 6.1\%$ $\pm 9.0\%$ $\pm 24\%$ | |
| Sense current saturation | $I_{IS,lim}$ | | 5.5 | -- | -- | mA | |
| Current sense leakage current | | $I_{IN} = 0$, $V_{IS} = 0$: $V_{IN} = 0$, $V_{IS} = 0$, $I_L \leq 0$: | | $I_{IS(LL)}$ $I_{IS(LH)}$ | -- -- | 0.5 -- | μA |
| Current sense settling time ¹⁷⁾ after positive input slope (90% of I_{IS} static) $I_L = 0/\text{tbd}$ (≥ 20) A: | $t_{son(IS)}$ | | -- | tbd | 500 | μs | |
| Current sense settling time ¹⁷⁾ after negative input slope (10% of I_{IS} static) $I_L = \text{tbd}$ (≥ 20) / 0 A: | $t_{soff(IS)}$ | | -- | tbd | 500 | μs | |
| Current sense settling time ¹⁷⁾ after change of load current (60% to 90%) $I_L = 15/\text{tbd}$ (≥ 20) A: | $t_{slc(IS)}$ | | -- | tbd | 500 | μs | |
| Overshoot protection $I_{bb} = 15\text{mA}$ | $V_{bIS(Z)}$ | $T_j = -40^\circ\text{C}$: $T_j = 25\dots+150^\circ\text{C}$: | 68 70 | -- 74 | -- -- | V | |

¹⁵⁾ The reverse load current through the intrinsic drain-source diode has to be limited by the connected load (as it is done with all polarity symmetric loads). Note that under off-conditions ($I_{IN} = I_{IS} = 0$) the power transistor is not activated. This results in raised power dissipation due to the higher voltage drop across the intrinsic drain-source diode. The temperature protection is not active during reverse current operation! Increasing reverse battery voltage capability is simply possible as described on page 8.

¹⁶⁾ If V_{ON} is higher, the sense current is no longer proportional to the load current due to sense current saturation, see $I_{IS,lim}$.

¹⁷⁾ Not tested, specified by design.

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| Parameter and Conditions at $T_j = -40 \dots +150^\circ\text{C}$, $V_{bb} = 12\text{V}$ unless otherwise specified | Symbol | Values | | | Unit |
|--|--------|--------|-----|-----|------|
| | | min | typ | max | |

Input

| | | | | | |
|---|---------------|----|----|----|---------------|
| Input and operating current (see diagram page 12) IN grounded ($V_{IN} = 0$) | $I_{IN(on)}$ | -- | 1 | 2 | mA |
| Input current for turn-off ¹⁸⁾ | $I_{IN(off)}$ | -- | -- | 40 | μA |

Truth Table

| | Input current level | Output level | Current Sense I_{IS} | Remark |
|-------------------------------|---------------------|-----------------------|------------------------------|---|
| Normal operation | L H | L H | 0 nominal | $=I_L / k_{IIS}$, up to $I_{IS}=I_{IS,lim}$ |
| Very high load current | H | H | $I_{IS,lim}$ | up to $V_{ON}=V_{ON(Fold\ back)}$ I_{IS} no longer proportional to I_L |
| Current-limitation | H | H | 0 | $V_{ON} > V_{ON(Fold\ back)}$ if $V_{ON} > V_{ON(SC)}$, shutdown will occur |
| Short circuit to GND | L H | L L | 0 0 | |
| Over-temperature | L H | L L | 0 0 | |
| Short circuit to V_{bb} | L H | H H | 0 <nominal ¹⁹⁾ | |
| Open load | L H | Z ²⁰⁾ H | 0 0 | |
| Negative output voltage clamp | L | L | 0 | |
| Inverse load current | L H | H H | 0 0 | |

L = "Low" Level

H = "High" Level

Overtemperature reset via input: $I_{IN}=\text{low}$ and $T_j < T_{jt}$ (see diagram on page 15)

Short circuit to GND: Shutdown remains latched until next reset via input (see diagram on page 13)

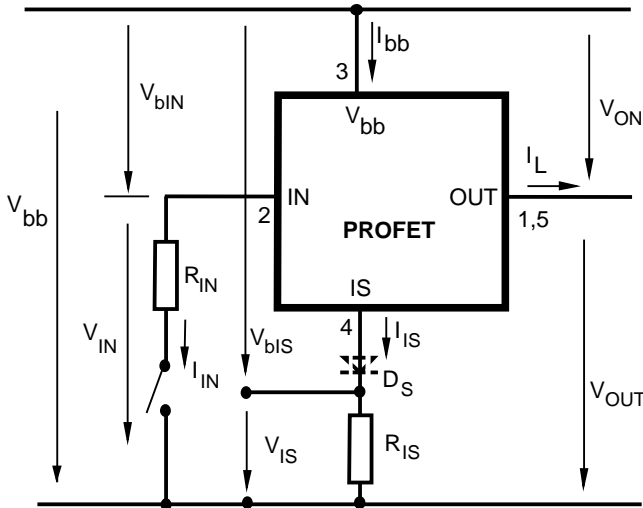
¹⁸⁾ We recommend the resistance between IN and GND to be less than $0.5\text{ k}\Omega$ for turn-on and more than $500\text{ k}\Omega$ for turn-off. Consider that when the device is switched off ($I_{IN} = 0$) the voltage between IN and GND reaches almost V_{bb} .

¹⁹⁾ Low ohmic short to V_{bb} may reduce the output current I_L and can thus be detected via the sense current I_{IS} .

²⁰⁾ Power Transistor "OFF", potential defined by external impedance.

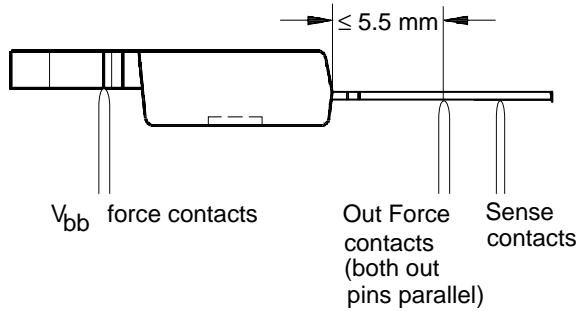
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Terms

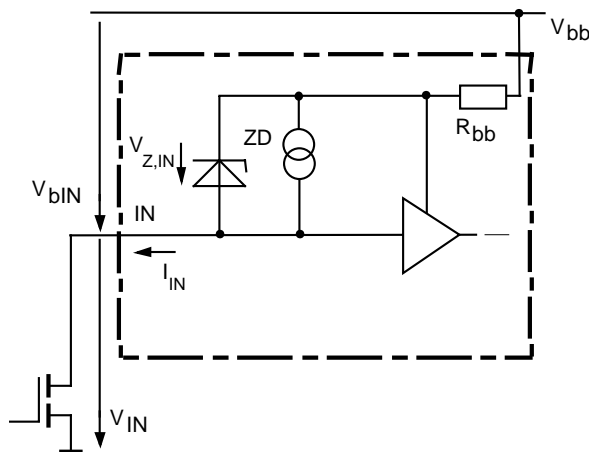


Two or more devices can easily be connected in parallel to increase load current capability.

R_{ON} measurement layout



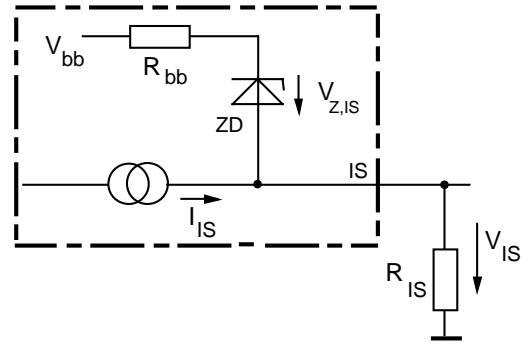
Input circuit (ESD protection)



When the device is switched off ($I_{IN} = 0$) the voltage between IN and GND reaches almost V_{bb} . Use a mechanical switch, a bipolar or MOS transistor with appropriate breakdown voltage as driver.

$V_{Z,IN} = 74\text{ V (typ.)}$.

Current sense status output

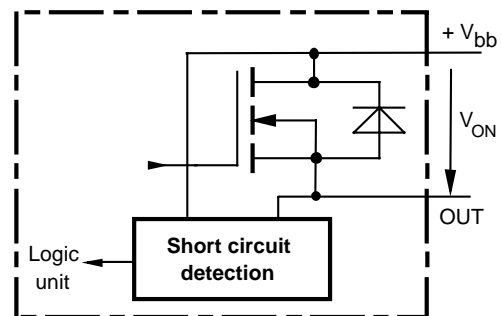


$V_{Z,IS} = 74\text{ V (typ.)}$, $R_{IS} = 1\text{ k}\Omega$ nominal (or $1\text{ k}\Omega/n$, if n devices are connected in parallel). $I_S = I_L/k_{IIS}$ can be only driven by the internal circuit as long as $V_{out} - V_{IS} > 5\text{ V}$. If you want to measure load currents up to $I_{L(M)}$, R_{IS} should be less than $\frac{V_{bb} - 5\text{ V}}{I_{L(M)} / k_{IIS}}$.

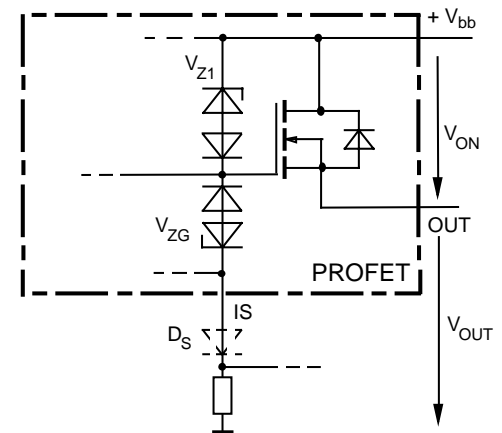
Note: For large values of R_{IS} the voltage V_{IS} can reach almost V_{bb} . See also overvoltage protection. If you don't use the current sense output in your application, you can leave it open.

Short circuit detection

Fault Condition: $V_{ON} > V_{ON(SC)}$ (6V typ.) and $t > t_{d(SC)}$ (80 ...300 μs).



Inductive and overvoltage output clamp

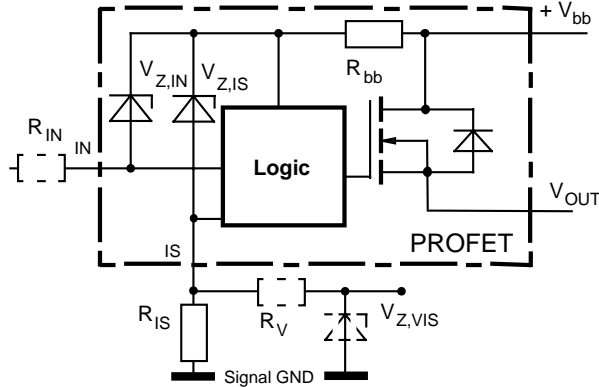


V_{ON} is clamped to $V_{ON(CL)} = 62\text{ V typ.}$ At inductive load switch-off without D_S , V_{OUT} is clamped to $V_{OUT(CL)} = -15\text{ V typ.}$ via V_{ZG} . With D_S , V_{OUT} is clamped to $V_{bb} - V_{ON(CL)}$ via V_{Z1} . Using D_S gives faster deenergizing of

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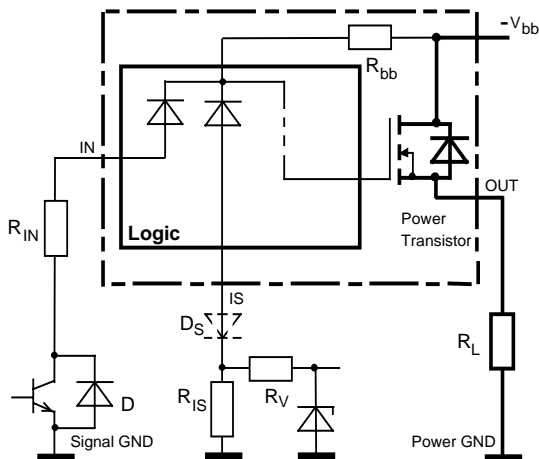
the inductive load, but higher peak power dissipation in the PROFET.

Overvoltage protection of logic part



$R_{bb} = 120\Omega$ typ., $V_{Z,IN} = V_{Z,IS} = 74\text{V}$ typ., $R_{IS} = 1\text{k}\Omega$ nominal. Note that when overvoltage exceeds 79V typ. a voltage above 5V can occur between IS and GND, if $R_V, V_{Z,VIS}$ are not used.

Reverse battery protection



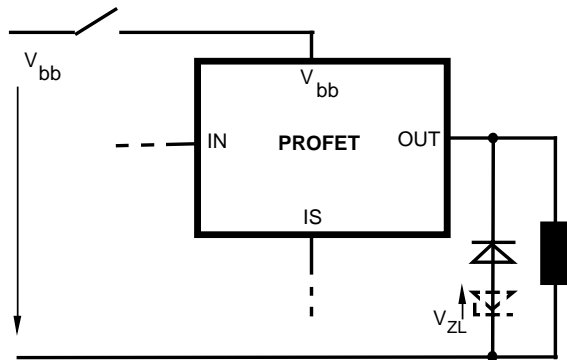
$R_V \geq 1\text{k}\Omega$, $R_{IS} = 1\text{k}\Omega$ nominal. Add R_{IN} for reverse battery protection in applications with V_{bb} above $16\text{V}^{15)}$; recommended value: $\frac{1}{R_{IN}} + \frac{1}{R_{IS}} + \frac{1}{R_V} = \frac{0.1\text{A}}{|V_{bb}| - 12\text{V}}$ if D_S is not used (or $\frac{1}{R_{IN}} = \frac{0.1\text{A}}{|V_{bb}| - 12\text{V}}$ if D_S is used).

To minimize power dissipation at reverse battery operation, the summarized current into the IN and IS pin should be about 120mA . The current can be provided by using a small signal diode D in parallel to the input switch, by using a MOSFET input switch or by proper adjusting the current through R_{IS} and R_V .

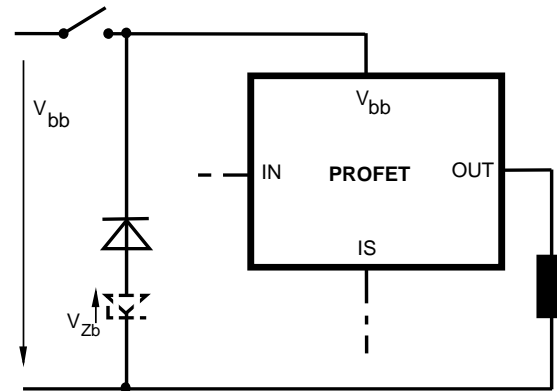
V_{bb} disconnect with energized inductive load

Provide a current path with load current capability by using a diode, a Z-diode, or a varistor. ($V_{ZL} < 70\text{V}$ or $V_{Zb} < 42\text{V}$ if $R_{IN}=0$). For higher clamp voltages currents at IN and IS have to be limited to 250mA .

Version a:

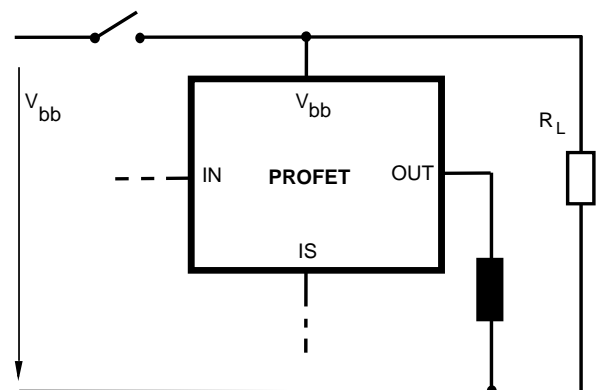


Version b:

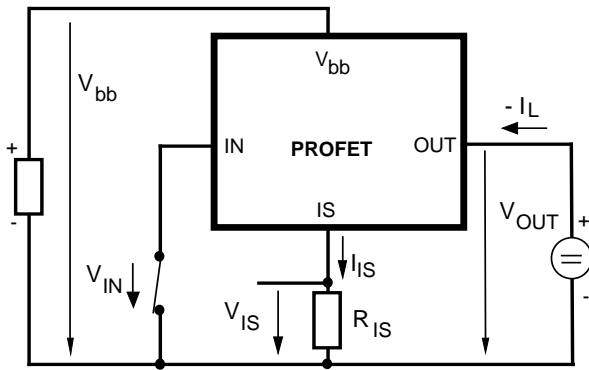


Note that there is no reverse battery protection when using a diode without additional Z-diode V_{ZL}, V_{Zb} .

Version c: Sometimes a necessary voltage clamp is given by non inductive loads R_L connected to the same switch and eliminates the need of clamping circuit:



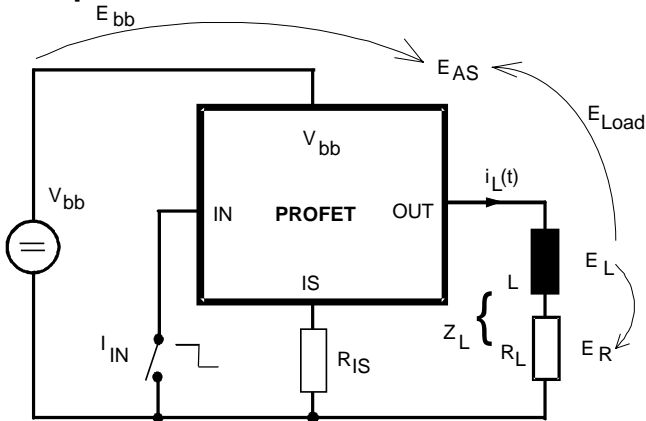
Inverse load current operation



The device is specified for inverse load current operation ($V_{OUT} > V_{bb} > 0V$). The current sense feature is not available during this kind of operation ($I_{IS} = 0$). With $I_{IN} = 0$ (e.g. input open) only the intrinsic drain source diode is conducting resulting in considerably increased power dissipation. If the device is switched on ($V_{IN} = 0$), this power dissipation is decreased to the much lower value $R_{ON(INV)} \cdot I^2$ (specifications see page 3).

Note: Temperature protection during inverse load current operation is not possible!

Inductive load switch-off energy dissipation



Energy stored in load inductance:

$$E_L = \frac{1}{2} \cdot L \cdot I_L^2$$

While demagnetizing load inductance, the energy dissipated in PROFET is

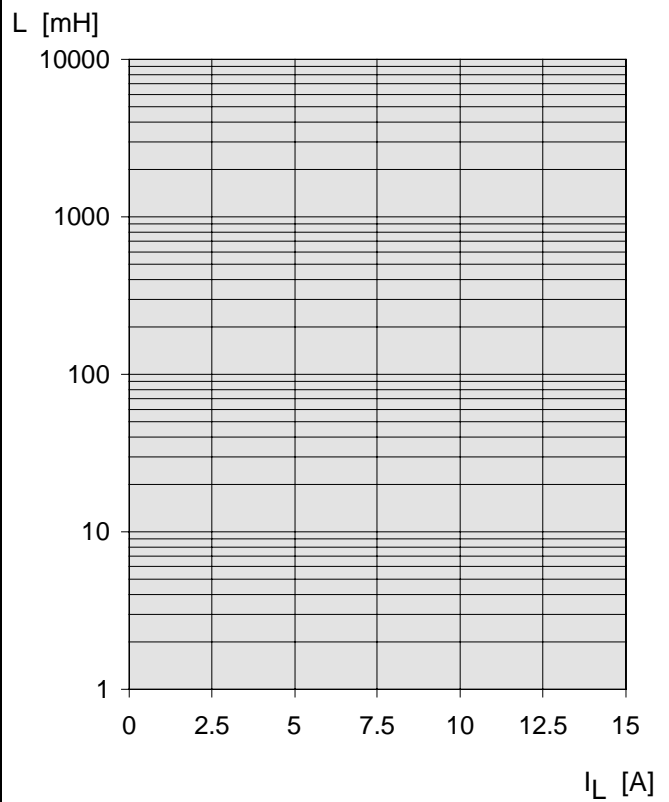
$$E_{AS} = E_{bb} + E_L - E_R = \int V_{ON(CL)} \cdot i_L(t) dt,$$

with an approximate solution for $R_L > 0 \Omega$:

$$E_{AS} = \frac{I_L \cdot L}{2 \cdot R_L} (V_{bb} + |V_{OUT(CL)}|) \ln \left(1 + \frac{I_L \cdot R_L}{|V_{OUT(CL)}|} \right)$$

Maximum allowable load inductance for a single switch off

$L = f(I_L)$; $T_{j,start} = 150^\circ C$, $V_{bb} = 12V$, $R_L = 0 \Omega$



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Options Overview

| Type | BTS | 660P | 560 |
|---|-----|-----------------------|-----------------------|
| Overtemperature protection with hysteresis $T_j > 150\text{ °C}$, latch function ²¹⁾ | | X | X |
| $T_j > 150\text{ °C}$, with auto-restart on cooling | | X | |
| Short circuit to GND protection switches off when $V_{ON} > 6\text{ V}$ typ. (when first turned on after approx. $180\text{ }\mu\text{s}$) | | X | X |
| Overvoltage shutdown | | - | - |
| Output negative voltage transient limit to $V_{bb} - V_{ON(CL)}$ to $V_{OUT} = -15\text{ V}$ typ | | X X ²²⁾ | X X ²²⁾ |

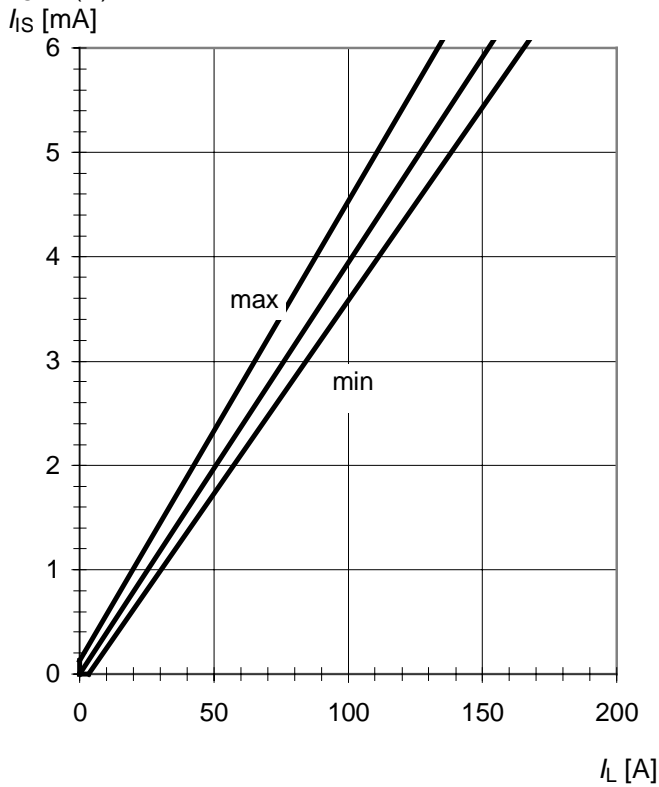
²¹⁾ Latch except when $V_{bb} - V_{OUT} < V_{ON(SC)}$ after shutdown. In most cases $V_{OUT} = 0\text{ V}$ after shutdown ($V_{OUT} \neq 0\text{ V}$ only if forced externally). So the device remains latched unless $V_{bb} < V_{ON(SC)}$ (see page 4). No latch between turn on and $t_{d(SC)}$.

²²⁾ Can be "switched off" by using a diode D_S (see page 7) or leaving open the current sense output.

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Characteristics

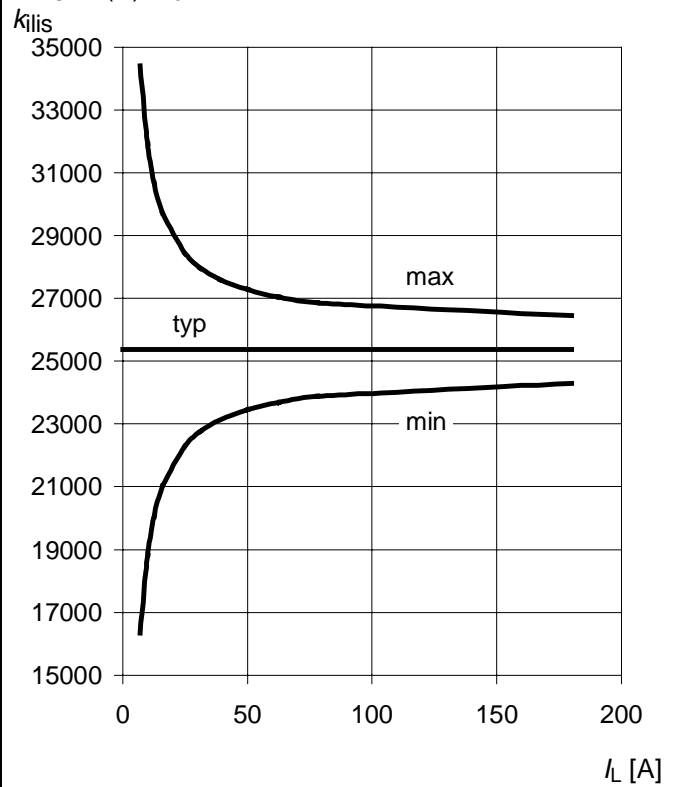
Current sense versus load current:

$$I_{IS} = f(I_L)$$



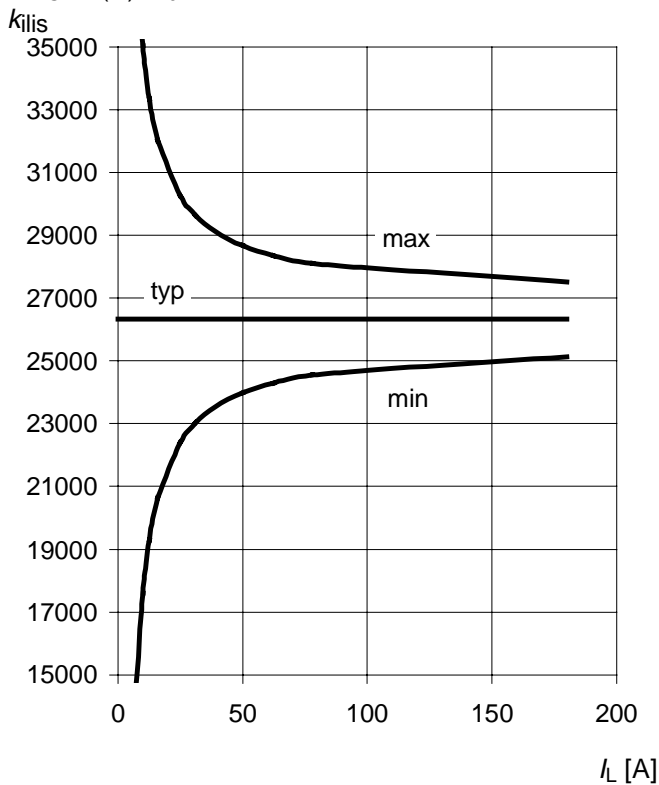
Current sense ratio:

$$K_{ILIS} = f(I_L), T_J = 25\text{ °C}$$



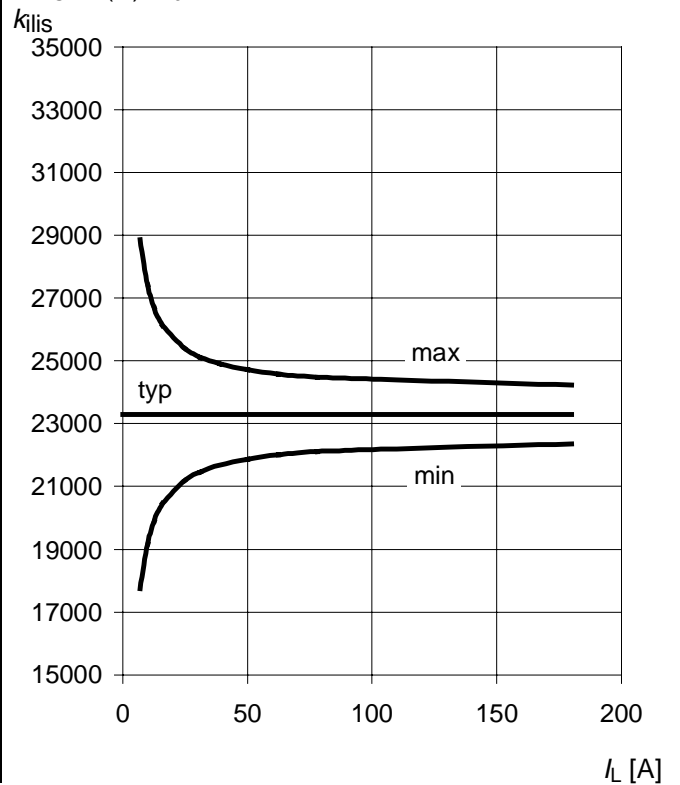
Current sense ratio:

$$K_{ILIS} = f(I_L), T_J = -40\text{ °C}$$



Current sense ratio:

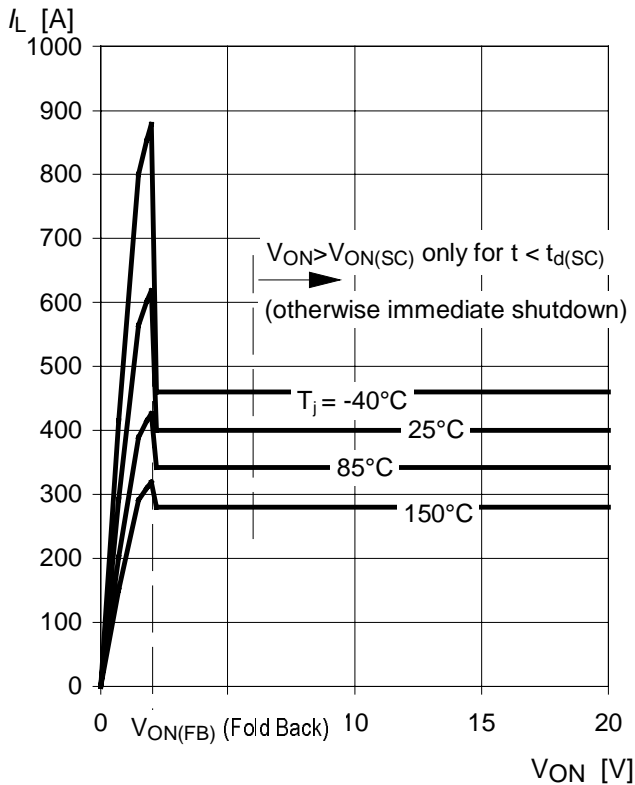
$$K_{ILIS} = f(I_L), T_J = 150\text{ °C}$$



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Typ. current limitation characteristic

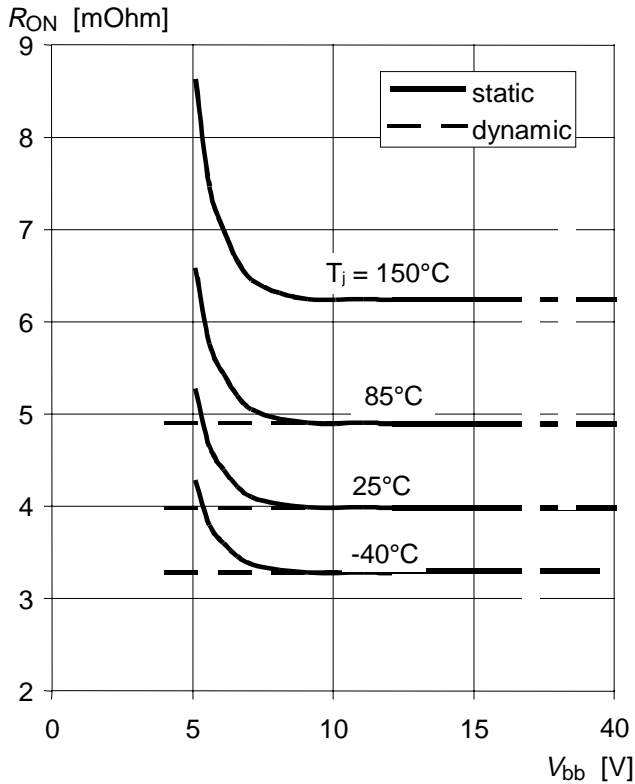
$$I_L = f(V_{ON}, T_j)$$



In case of $V_{ON} > V_{ON(SC)}$ (typ. 6 V) the device will be switched off by internal short circuit detection.

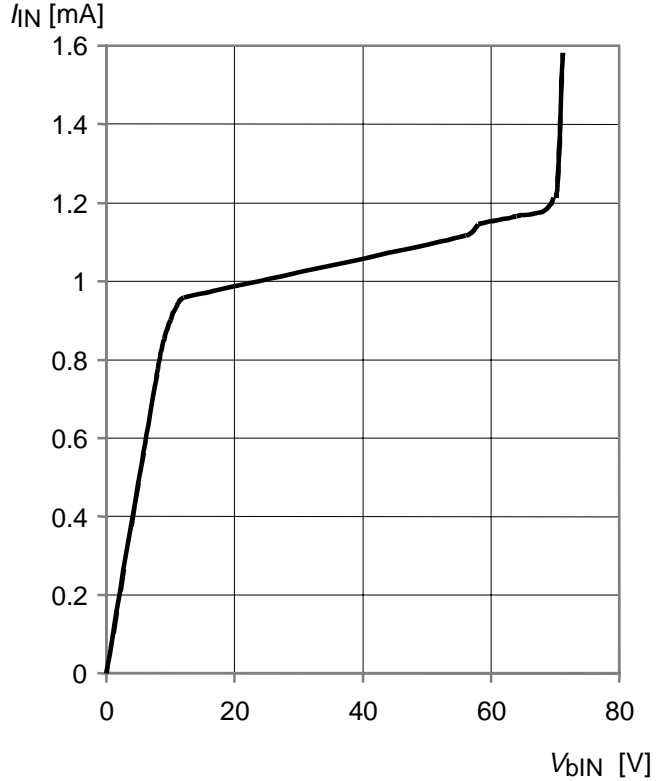
Typ. on-state resistance

$$R_{ON} = f(V_{bb}, T_j); I_L = tbd (>=20) \text{ A}; V_{IN} = 0$$



Typ. input current

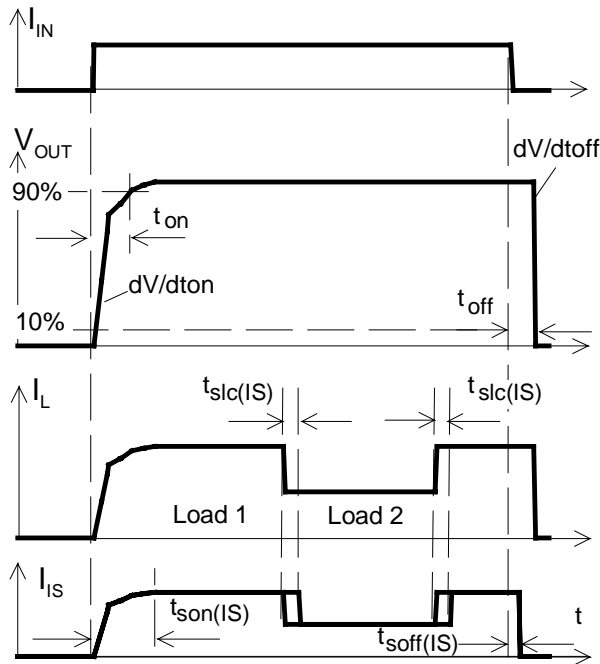
$$I_{IN} = f(V_{bIN}), V_{bIN} = V_{bb} - V_{IN}$$



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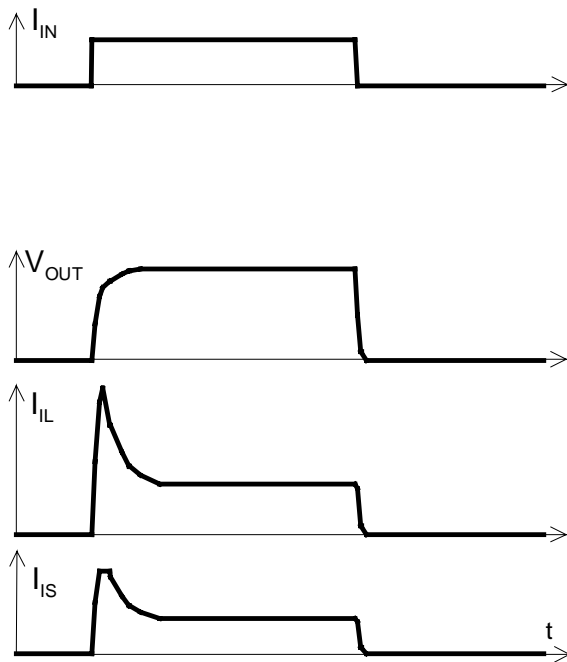
Timing diagrams

Figure 1a: Switching a resistive load, change of load current in on-condition:



The sense signal is not valid during a settling time after turn-on/off and after change of load current.

Figure 2a: Switching motors and lamps:



Sense current saturation can occur at very high inrush currents (see $I_{IS,lim}$ on page 5).

Figure 2b: Switching an inductive load:

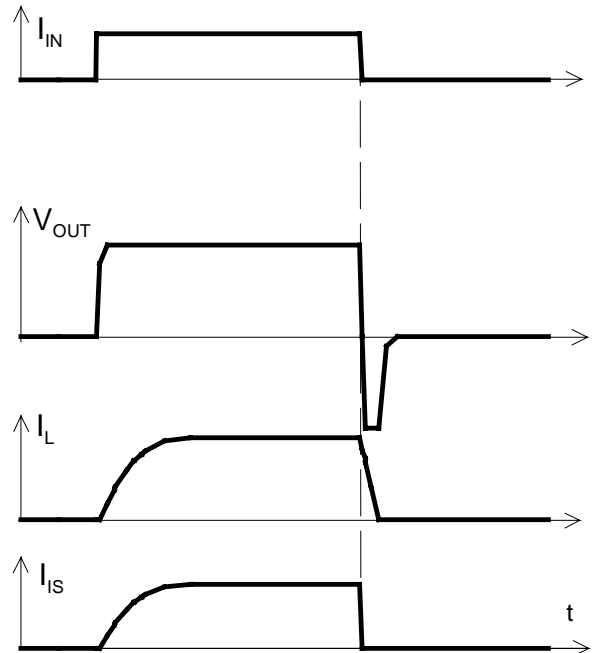
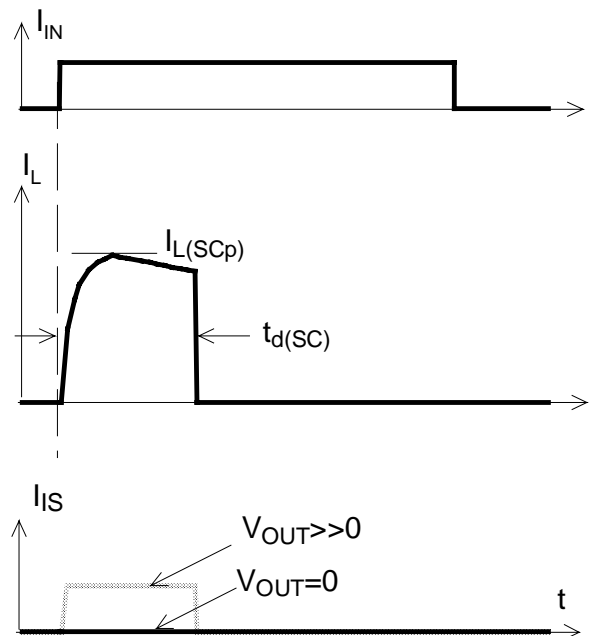


Figure 3a: Short circuit:

shut down by short circuit detection, reset by $I_{IN} = 0$.



Shut down remains latched until next reset via input.

Figure 4a: Overtemperature,
Reset if ($I_{IN}=low$) and ($T_j < T_{jt}$)

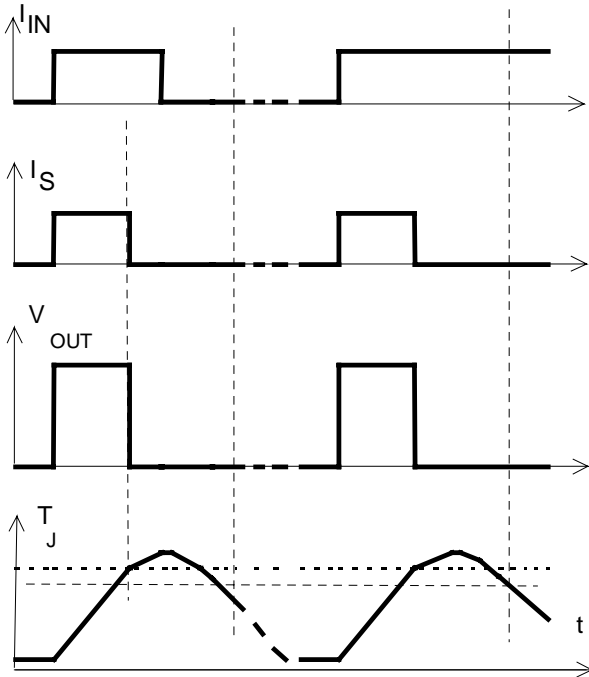
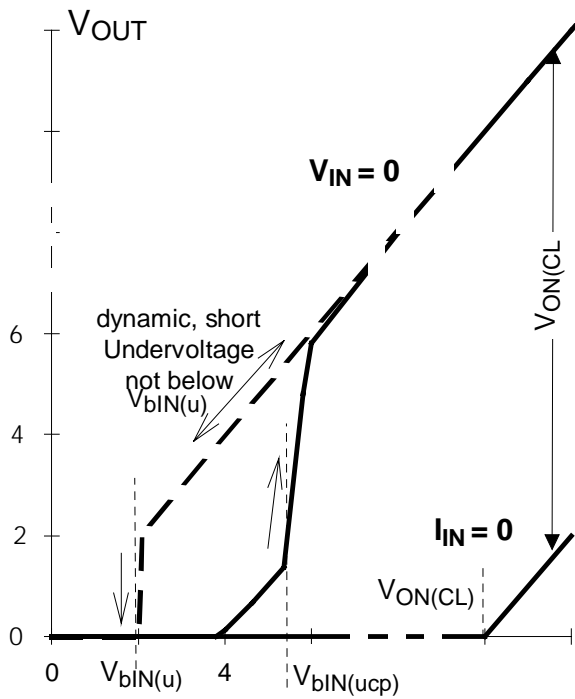


Figure 6a: Undervoltage restart of charge pump, overvoltage clamp

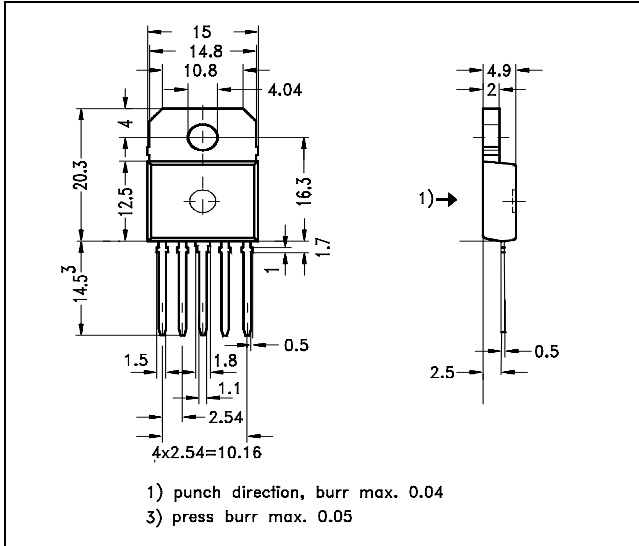


查询"BTS560"供应商 Package and Ordering Code

All dimensions in mm

TO-218AB/5 Option E3146 Ordering code

| | |
|--------------|----------------|
| BTS560 E3146 | Q67060-S6953A3 |
|--------------|----------------|



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