

HIGH VOLTAGE OPERATIONAL AMPLIFIER

0004

M.S.KENNEDY CORP

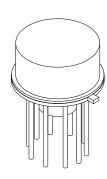
4707 Dey Road Liverpool, N.Y. 13088

(315) 701-6751

MIL-PRF-38534 QUALIFIED

FEATURES:

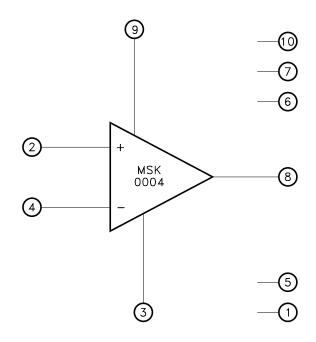
- Pin Similar Replacement for the LH0004
- Wide Supply Voltage Range: ±10V to ±50V
- Low Offset Current: 15nA
- · High Voltage Gain: 200KV/V
- Internal Compensation
- Output Overload Protection
- · Thermal Overload Protection



DESCRIPTION:

The MSK 0004 is a high voltage operational amplifier for use in high performance signal conditioning applications, as well as resolver excitation designs. These devices offer maximum reliability by providing internal output overload protection and thermal overload protection. Monolithic design and internal compensation make the MSK 0004 an excellent replacement for many general purpose operational amplifiers and specifically the LH0004. The MSK 0004 is internally compensated and can replace the LH0004 in most applications without any changes to existing circuitry. The device is packaged in an hermetically sealed 10 pin metal can.

EQUIVALENT SCHEMATIC



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TYPICAL APPLICATIONS

- Precision High Voltage Power Supply
- High Voltage Regulators
- · Signal Conditioning
- · Resolver Excitation
- Transducer Power Supply

PIN-OUT INFORMATION

1 NC 10 NC 2 +Input 9 +Vcc 3 -Vcc 8 Output 4 -Input 7 NC

5 NC 6 NC

ABSOLUTE MAXIMUM RATINGS

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V_{cc}	Supply Voltage ±50V	Тsт	Storage Temperature Range -65°C to +150°C
VIN	Differential Input Voltage ±40V	T_LD	Lead Temperature Range 300°C
Tc	Case Operating Temperature Range		(10 Seconds)
	MSK0004H/E55°C to +125°C	Tc	Junction Temperature
	MSK0004 -40° C to $+85^{\circ}$ C		

ELECTRICAL SPECIFICATIONS

Parameter	Test Conditions ①	Group A	мѕкоо		H/E	MSK0004			Units
raiametei		Subgroup	Min.	Тур.	Max.	Min.	Тур.	Max.	Units
STATIC									
Supply Voltage Range ②			±10	±40	±50	±10	±40	±45	V
Quiescent Current		1	-	±3.0	±4.5	-	±3.0	±5.0	mA
		2,3	-	-	±4.5	-	-	-	mA
INPUT									
Input Offset Voltage	AV = 10	1	-	±1.0	±6.0	-	± 1.0	±7.5	mV
		2,3	-	-	±7.0	-	-	-	mV
Input Offset Voltage Drift ②		-	-	±15	-	-	± 15	-	μV/°C
Input Bias Current ②	Vcm = 0V	1	-	±12	±30	-	±12	±50	nA
		2,3	-	-	±50	-	-	-	nA
Input Offset Current ②	Vcm = 0V	1	-	±15	±30	-	±15	±40	nA
Common Mode Rejection Ratio ②	$V_{CM} = \pm 20 V_{DC}$	-	74	100	-	74	100	-	dB
Input Impedence ②	DC	-	40	250	-	40	250	-	ΜΩ
ОИТРИТ									
Output Voltage Swing	f = 1KHz	4	±35	±37	-	±35	±37	-	V
Power Bandwidth ②	V OUT = $\pm 35V$ PK	-	-	23	-	-	23	-	KHz
Output Resistance ②	No Load	-	-	500	-	-	500	-	Ω
Capacitive Load ②	$R_L = 1 K\Omega$	-	-	50	-	-	50	-	pF
TRANSFER CHARACTERISTICS									
Slew Rate	$V_{OUT} = \pm 30 V_{PK}$	4	2.5	5.0	-	2.5	5.0	-	V/μS
Open Loop Voltage Gain ②	$Vout = \pm 30VPK$ $f = 10KHz$	4	100K	200K	-	100K	200K	-	V/V
Thermal Resistance	Junction to Case @ 125°C	-	-	16	19	-	16	22	°C/W

NOTES:

① Unless otherwise specified, Vcc = ±40Vpc and Vin = 0V.
② Guaranteed by design but not tested. Typical parameters are representative of actual device performance but are for reference only.
③ Industrial grade and "E" suffix devices shall be tested to subgroups 1 and 4 unless otherwise requested.

⁴ Military grade devices ("H" suffix) shall be 100% tested to subgroups 1,2,3 and 4.

⁽a) Subgroup 5 and 6 testing available upon request.
(b) Subgroup 1,4 Tc = +25°C
Subgroup 2,5 Tc = +125°C
Subgroup 3,6 Ta = -55°C

APPLICATION NOTES

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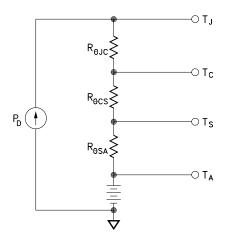
POWER SUPPLY BYPASSING

Both the negative and positive power supplies must be effectively decoupled with a high and low frequency bypass circuit to avoid power supply induced oscillation. An effective deecoupling scheme consists of a 0.1 microfarad ceramic capacitor in parallel with a 4.7 microfarad tantalum capacitor from each power supply pin to ground.

HEAT SINKING

To determine if a heat sink is necessary for your application and if so, what type, refer to the thermal model and governing equation below.

Thermal Model:



Governing Equation:

$$T_J = P_D X (R_{\theta JC} + R_{\theta CS} + R_{\theta SA}) + T_A$$

Where

TJ = Junction Temperature
PD = Total Power Dissipation

 $R_{ heta CC}$ = Junction to Case Thermal Resistance $R_{ heta CS}$ = Case to Heat Sink Thermal Resistance $R_{ heta SA}$ = Heat Sink to Ambient Thermal Resistance

TC = Case Temperature
TA = Ambient Temperature
TS = Sink Temperature

Example:

The example demonstrates a worst case analysis for the op-amp output stage. This occurs when the output voltage is 1/2 the power supply voltage. Under this condition, maximum power transfer occurs and the output is under maximum stress. Conditions:

 $Vcc = \pm 40VDC$

 $Vo = \pm 20Vp$ Sine Wave, Freq. = 1KHz

 $RL = 1K\Omega$

For a worst case analysis we treat the ± 20 Vp sine wave as an 8 VDC output voltage.

1.) Find driver power dissipation

 $P_D = (Vcc-Vo) (Vo/RL)$

 $= (40V-20V) (20V/1K\Omega)$

=400mW

- 2.) For conservative design, set $T_J = +125$ °C.
- 3.) For this example, worst case TA = +100 °C.
- 4.) $R_{\theta}JC = 16^{\circ}C/W$.
- 5.) Recs = 0.15 °C/W for most thermal greases.
- 6.) Rearrange governing equation to solve for Resa:

 $R_{\theta SA} = ((T_J - T_A) / P_D) - (R_{\theta JC}) - (R_{\theta CS})$

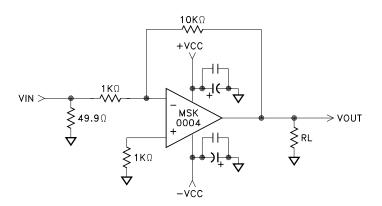
 $= (125 \,^{\circ}\text{C} - 100 \,^{\circ}\text{C})/0.4\text{W} - 16 \,^{\circ}\text{C/W} - 0.15 \,^{\circ}\text{C/W}$

= 62.5 - 16.15

 $=46.4 \, {}^{\circ}\text{C/W}$

The heat sink in this example must have a thermal resistance of no more than $46.4\,^{\circ}$ C/W to maintain a junction temperature of less than $+125\,^{\circ}$ C.

TYPICAL APPLICATION CIRCUIT

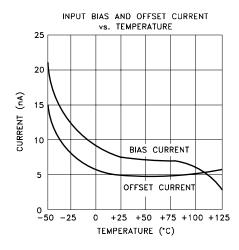


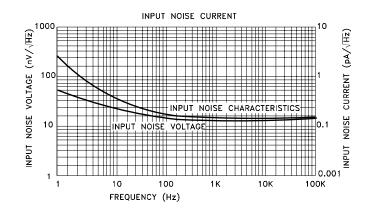
REPLACING THE LH0004

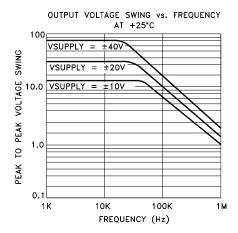
The MSK 0004 is not an exact copy of the LM0004 but it is only slightly different. The MSK 0004 is internally compensated and is lower cost. Pins 1,5,6,7 and 10 are not connected internally in the MSK0004.

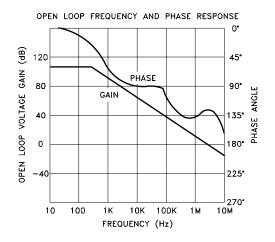
TYPICAL PERFORMANCE CURVES

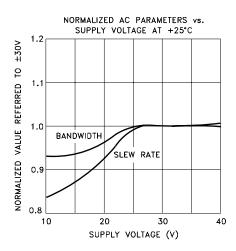
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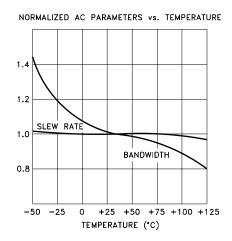




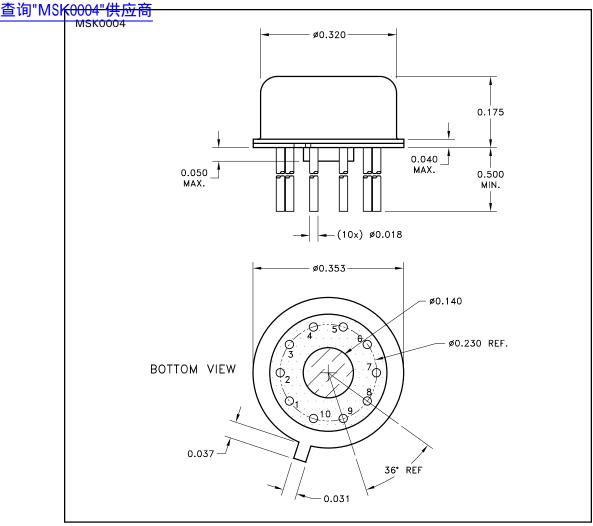






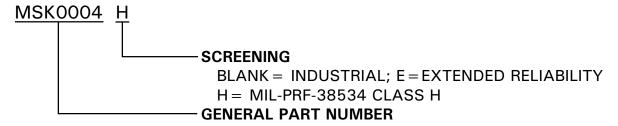


MECHANICAL SPECIFICATIONS



ALL DIMENSIONS ARE ± 0.010 INCHES UNLESS OTHERWISE LABELED.

ORDERING INFORMATION



The above example is a Military grade hybrid.

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